### Shear and Moment Relationships

$$w = -\frac{dV}{dx}$$

Slope of the shear diagram = - Value of applied loading

$$V = \frac{dM}{dx}$$

### Slope of the moment curve = Shear Force

Both equations not applicable at the point of loading because of discontinuity produced by the abrupt change in shear.

$$w = -\frac{dV}{dx}$$
 Degree of *V* in *x* is one higher than that of *w*  
$$V = \frac{dM}{dx}$$
 Degree of *M* in *x* is one higher than that of *V*

 $\rightarrow$  Degree of *M* in *x* is two higher than that of *w* 

Combining the two equations 
$$\Rightarrow \frac{d^2 M}{dx^2} = -w$$

→ M :: obtained by integrating this equation twice
→ Method is usable only if w is a continuous function of x (other cases not part of this course)

### Shear and Moment Relationships Expressing V in terms of w by integrating $w = -\frac{dV}{dx}$

 $\int_{V_0}^{V} dV = -\int_{x_0}^{x} w dx$  OR  $V = V_0 + ($ the negative of the area under the loading curve from  $x_0$  to x)

 $V_0$  is the shear force at  $x_0$  and V is the shear force at x

Expressing *M* in terms of *V* by integrating  $V = \frac{dM}{dx}$ 

 $\int_{M_0}^{M} dM = \int_{x_0}^{x} V dx \quad \text{OR} \quad M = M_0 + (\text{area under the shear diagram} \\ \text{from } x_0 \text{ to } x)$ 

 $M_0$  is the BM at  $x_0$  and M is the BM at x

 $V = V_0 + (\text{negative of area under the loading curve from } x_0 \text{ to } x)$ 

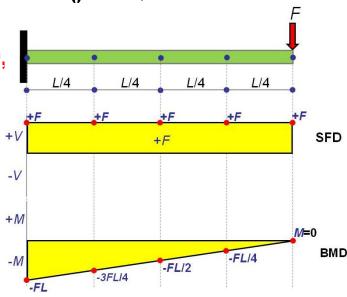
 $M = M_0 + (area under the shear diagram from x_0 to x)$ 

If there is no externally applied moment  $M_0$  at  $x_0 = 0$ , total moment at any section equals the area under the shear diagram up to that section

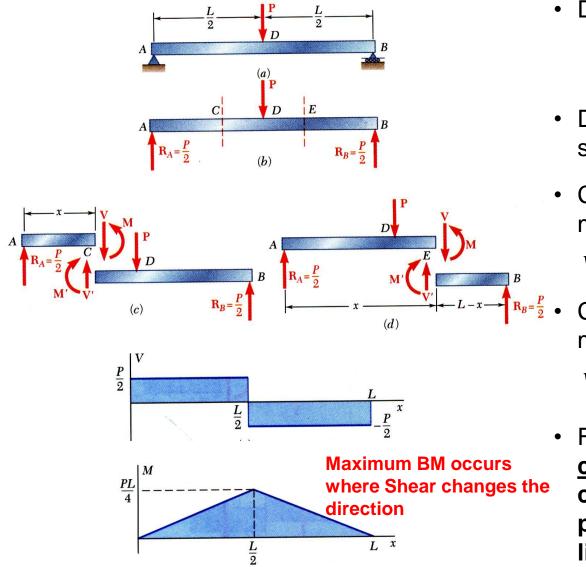
When **V** passes through zero and is a continuous function of x with  $dV/dx \neq 0$  (i.e., nonzero loading)  $\frac{dM}{dx} = 0$ 

→ BM will be a maximum or minimum at this point

# Critical values of BM also occur when SF crosses the zero axis discontinuously (e.g., Beams under concentrated loads)



# Beams – SFD and BMD: Example (1)



• Draw the SFD and BMD.

- Determine reactions at supports.
- Cut beam at *C* and consider member *AC*,

 $V = +P/2 \quad M = +Px/2$ 

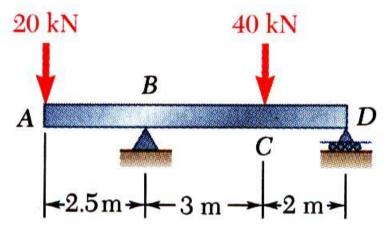
• Cut beam at *E* and consider member *EB*,

V = -P/2 M = +P(L-x)/2

 For a beam subjected to <u>concentrated loads</u>, shear is constant between loading points and moment varies linearly

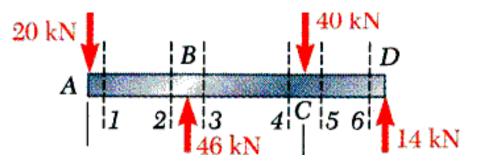
# Beams – SFD and BMD: Example (2)

Draw the shear and bending moment diagrams for the beam and loading shown.

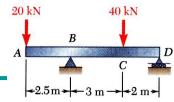


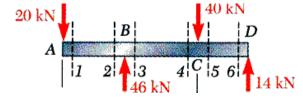
Solution: Draw FBD and find out the

support reactions using equilibrium equations

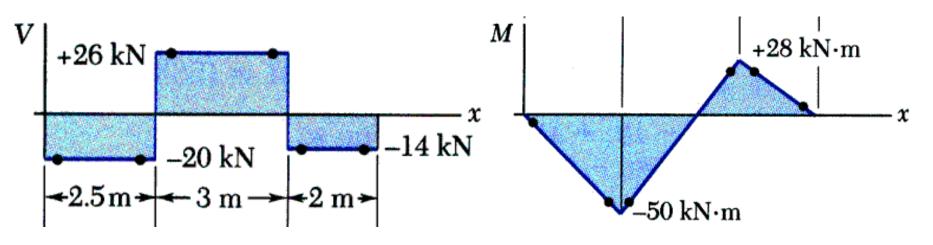


## SFD and BMD: Example (2)





Use equilibrium conditions at all sections to get the unknown SF and BM  $\sum F_y = 0: -20 \text{ kN} - V_1 = 0 \qquad V_1 = -20 \text{ kN}$   $\sum M_1 = 0: (20 \text{ kN})(0 \text{ m}) + M_1 = 0 \qquad M_1 = 0$   $V_2 = -20 \text{ kN}; M_2 = -20x \text{ kNm}$   $V_3 = +26 \text{ kN}; M_3 = -20x + 46 \times 0 = -20x \Rightarrow M_B = -50 \text{ kNm}$   $V_4 = +26 \text{ kN}; M_4 = -20x + 46 \times (x - 2.5) \Rightarrow M_C = +28 \text{ kNm}$   $V_5 = -14 \text{ kN}; M_5 = -20x + 46 \times (x - 2.5) - 40 \times 0 \Rightarrow M_C = +28 \text{ kNm}$   $V_6 = -14 \text{ kN}; M_6 = -20x + 46 \times (x - 2.5) - 40 \times (x - 5.5)$   $\Rightarrow M_D = 0 \text{ kNm}$ 

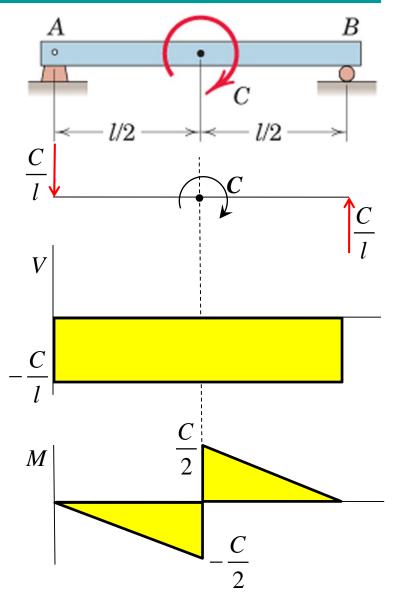


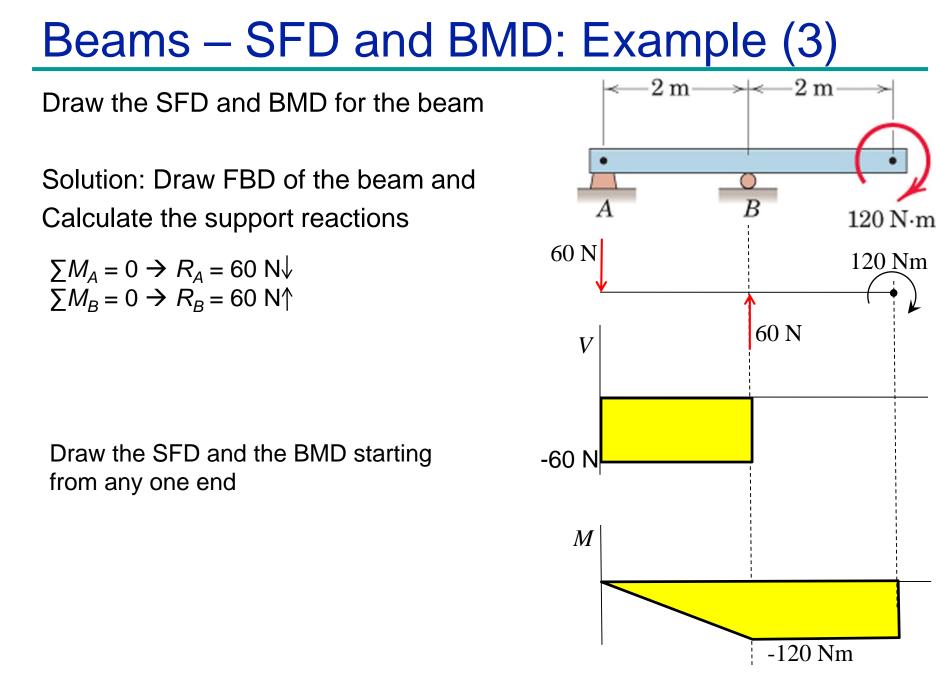
### Beams – SFD and BMD: Example (3)

Draw the SFD and BMD for the beam acted upon by a clockwise couple at mid point

Solution: Draw FBD of the beam and Calculate the support reactions

Draw the SFD and the BMD starting From any one end





### Beams – SFD and BMD: Example (4)

w

Draw the SFD and BMD for the beam

Solution:

Draw FBD of the entire beam and calculate support reactions using equilibrium equations

Reactions at supports:  $R_A = R_B = \frac{wL}{2}$ 

Develop the relations between loading, shear force, and bending moment and plot the SFD and BMD

### Beams – SFD and BMD: Example (4)

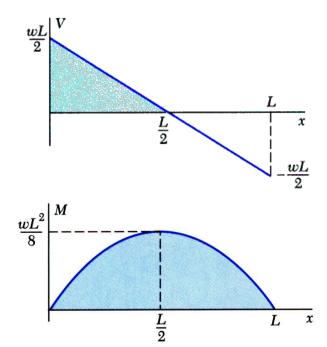
Shear Force at any section: 
$$V = \frac{wL}{2} - wx = w\left(\frac{L}{2} - x\right)$$

B

 $\mathbf{R}_B = \frac{wL}{2}$ 

Alternatively,  $V - V_A = -\int_0^x w \, dx = -wx$ 

$$V = V_A - wx = \frac{wL}{2} - wx = w\left(\frac{L}{2} - x\right)$$



BM at any section: 
$$M = \frac{wL}{2}x - wx\frac{x}{2} = \frac{w}{2}(Lx - x^2)$$

Alternatively, 
$$M - M_A = \int_0^x V dx$$

$$M = \int_{0}^{x} w \left(\frac{L}{2} - x\right) dx = \frac{w}{2} \left(Lx - x^{2}\right)$$

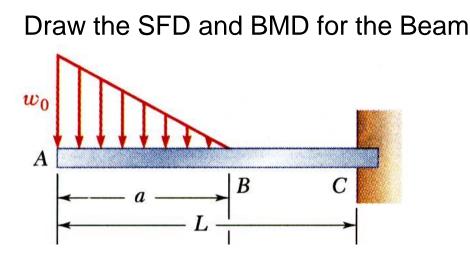
$$M_{\text{max}} = \frac{wL^2}{8} \quad \because \left(M \text{ at } \frac{dM}{dx} = V = 0\right)$$

A

 $\mathbf{R}_A = \frac{wL}{2}$ 

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# Beams – SFD and BMD: Example (5)

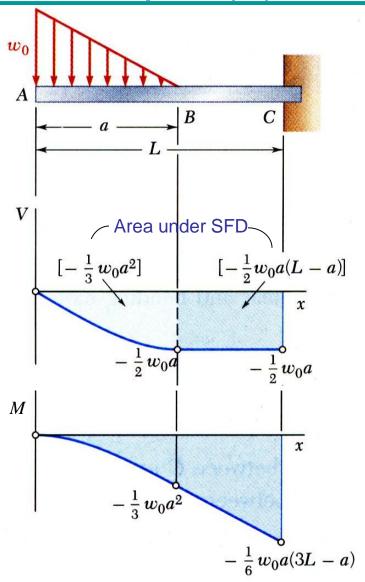


#### Solution:

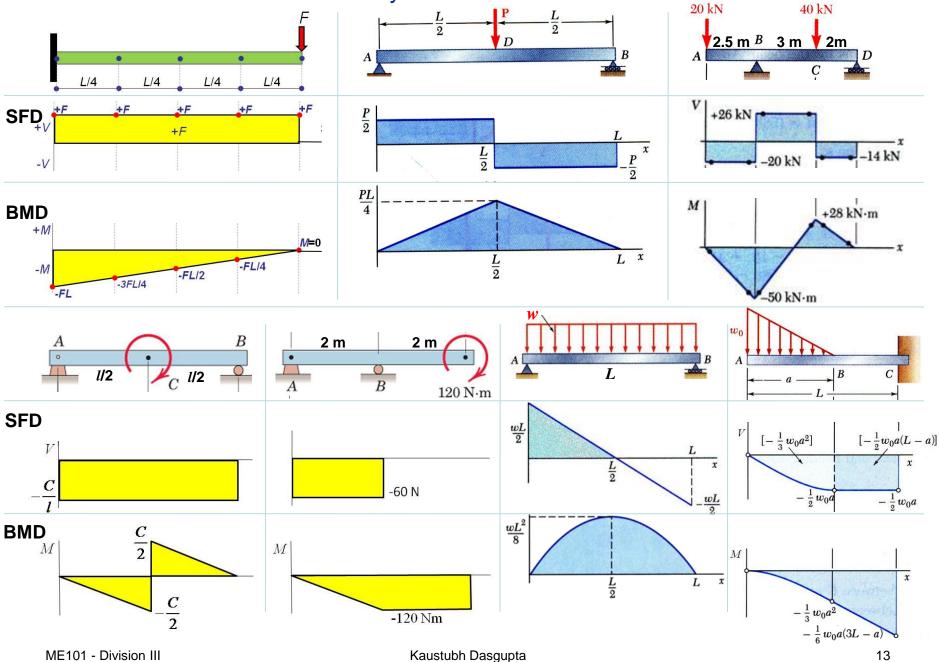
SFD and BMD can be plotted without determining support reactions since it is a cantilever beam.

However, values of SF and BM can be verified at the support if support reactions are known.

$$R_{C} = \frac{w_{0}a}{2}\uparrow; \quad M_{C} = \frac{w_{0}a}{2}\left(L - \frac{a}{3}\right) = \frac{w_{0}a}{6}\left(3L - a\right)$$



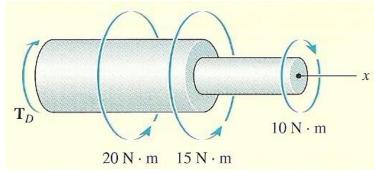
#### Beams – SFD and BMD: Summary

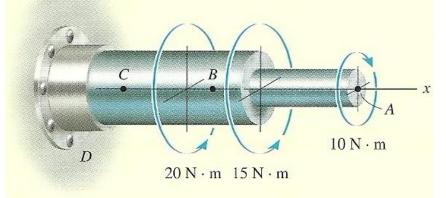


## **Beams – Internal Effects**

Example: Find the internal torques at points B and C of the circular shaft subjected to three concentrated torques

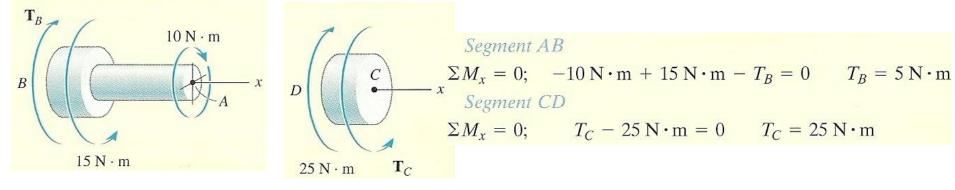
Solution: FBD of entire shaft





$$\Sigma M_x = 0; \quad -10 \operatorname{N} \cdot \operatorname{m} + 15 \operatorname{N} \cdot \operatorname{m} + 20 \operatorname{N} \cdot \operatorname{m} - T_D = 0$$
$$T_D = 25 \operatorname{N} \cdot \operatorname{m}$$

#### Sections at B and C and FBDs of shaft segments AB and CD



### Flexible and Inextensible Cables



Important Design Parameters

Tension Span Sag Length

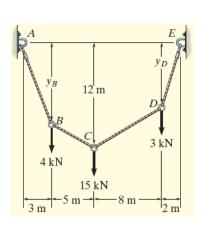


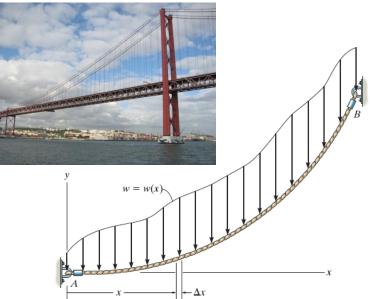




- Relations involving Tension, Span, Sag, and Length are reqd
  - Obtained by examining the cable as a body in equilibrium
- It is assumed that any resistance offered to bending is negligible → Force in cable is always along the direction of the cable.
- Flexible cables may be subjected to concentrated loads or distributed loads







- In some cases, weight of the cable is negligible compared with the loads it supports.
- In other cases, weight of the cable may be significant or may be the only load acting → weight cannot be neglected.



Three primary cases of analysis: Cables subjected to

- 1. concentrated load, 2. distributed load, 3. self weight
- → Requirements for equilibrium are formulated in identical way provided Loading is coplanar with the cable

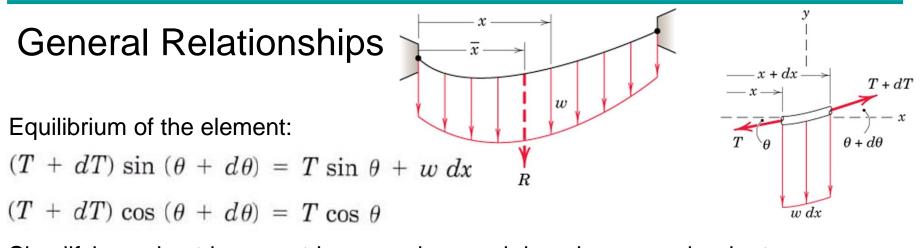
Primary Assumption in Analysis: The cable is perfectly Flexible and Inextensible

Flexible  $\rightarrow$  cable offers no resistance to bending

→ tensile force acting in the cable is always tangent to the cable at points along its length

Inextensible  $\rightarrow$  cable has a constant length both before and after the load is applied

- → once the load is applied, geometry of the cable remains fixed
- → cable or a segment of it can be treated as a rigid body



Simplifying using trigonometric expansions and dropping second order terms  $T \cos \theta \, d\theta + dT \sin \theta = w \, dx$  Further simplifying:  $\rightarrow d(T \sin \theta) = w \, dx$  $-T \sin \theta \, d\theta + dT \cos \theta = 0$   $\rightarrow d(T \cos \theta) = 0$ 

Finally: 
$$\frac{d^2y}{dx^2} = \frac{w}{T_0}$$

where  $T_0 = T \cos \theta$ 

→Equilibrium Equation
→Differential Equation for the Flexible Cable

-Defines the shape of the cable

-Can be used to solve two limiting cases of cable loading

## Cables: Parabolic Cable

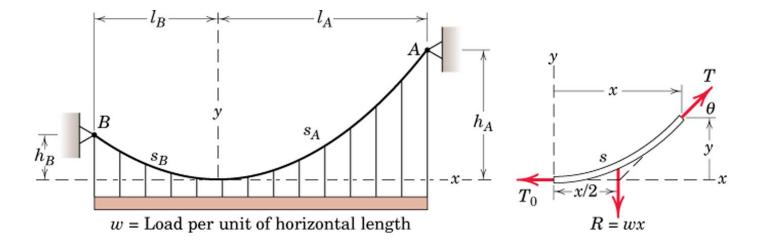
### Parabolic Cable

Intensity of vertical loading is constant

→ It can be proved that the cable hangs in a Parabolic Arc

 $\rightarrow$  Differential Equation can be used to analyse



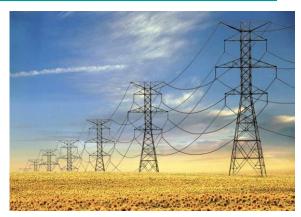


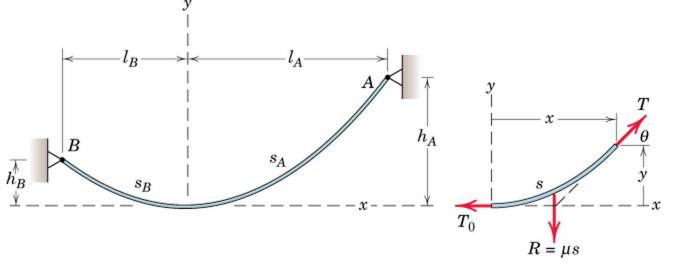
# Cables: Catenary Cable

### **Catenary Cable**

Hanging under the action of its own weight

- → It can be proved that the cable hangs in a curved shape called Catenary
- $\rightarrow$  Differential Equation can be used to analyse





 $\mu$  is the self weight per unit length