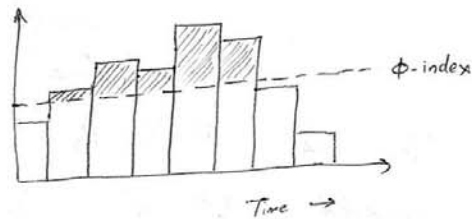
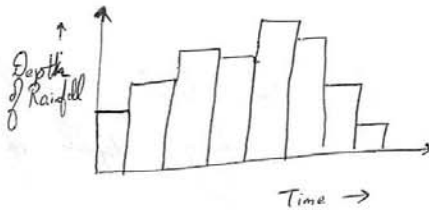


Excess Rainfall

In the last class we discussed on excess rainfall.

- What is meant by excess rainfall
- From a given rainfall data - how to find the excess rainfall, etc.

The method we discussed in the last class was the ϕ -index method.



$$\text{Depth of excess rainfall} = \text{Depth of direct runoff}$$

$$\text{ie. } R_d = \sum_{i=1}^M (R_i - \phi \Delta t)$$

where M is the number of intervals of rainfall that actually contribute to direct runoff.

→ So now you know that in the actual rainfall depths (R) you need to deduct some quantities to obtain the depth of rainfall (R_d).

→ One can easily say $R_d = f(R_i)$.

Runoff Coefficients

One particular method of relating R_d with rainfall depths is the use of runoff coefficients.

(2)

i.e. $R_d = C R$

where $R_d \rightarrow$ depth of runoff
 $R \rightarrow$ depth of rainfall
 $C \rightarrow$ runoff coefficient

Runoff coefficient $\rightarrow$ is the ratio of peak rate of direct runoff to the average intensity of rainfall in a storm.

$\rightarrow$ It is also defined as ratio of runoff to rainfall over a given time period.

e.g. If $R_1, R_2, R_3, \dots, R_m$ are the total rainfall recorded and if R_d is the corresponding depth of runoff, then

$$C = \frac{R_d}{\sum_{m=1}^M R_m}$$

SCS Method

Soil Conservation Service (1972) developed a method for computing abstractions from storm rainfall.

$\rightarrow$ When you consider a storm

- * You can think of depth of excess rainfall or depth of direct runoff (P_e).
- * You can see that this $P_e \leq P$ (the depth of rainfall).
- * Whatever rainfall occurs there will be some abstractions.

(3)

- * We can suggest a depth of water that gets retained in the watershed or abstracted (F_a).
- * This depth $F_a \leq S$, the depth of potential maximum retention possible.
- * There can be some amount of rainfall I_a (initial abstraction) before ponding for which no runoff occurs. ~~the~~
- * Now you can see that the potential maximum depth of runoff possible is $= P - I_a$.
- * SCS method suggests that the ratio of two potential quantities is equal to the ratio of their actuals.

i.e. $\frac{S}{P - I_a} = \frac{F_a}{P_e}$

→ From the continuity principle, you can see in this case that the total water available here is P .

$$P = P_e + I_a + F_a$$

$$\frac{P_e}{(P_e + I_a + F_a) - I_a} = \frac{F_a}{S}$$

Rearranging, we get

$$P_e = \frac{(P - I_a)^2}{P - I_a + S}$$

(4)

→ From studies on various small experimental watersheds, an empirical relation was observed

$$I_a = 0.2 S$$

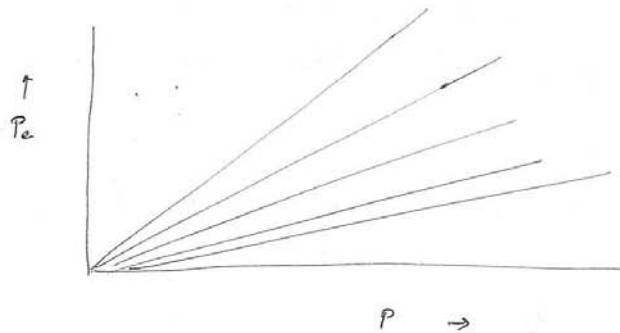
$$\therefore \text{Now } P_e = \frac{(P - 0.2 S)^2}{P + 0.8 S}$$

The soil conservation service plotted data for P and P_e for many watersheds. From these plots they obtained some curves (called SCS curves or Curve Numbers).

* Curve number is a dimensionless number

$$P_e = \frac{(P - 0.2 S)^2}{P + 0.8 S}$$

graphically plot this equation



$$CN = \frac{1000}{10 + S}$$

The elevations and depths here are in inches.
When you solve for your own problem appropriate

(5)

conversions need to be employed.

$$S = \frac{1000}{CN} - 10$$

$S \rightarrow$ in inches.

$$\therefore CN = \frac{1000}{10 + S}$$

$\rightarrow$ The curve number obtained here is for normal antecedent moisture conditions (AMC II).

$\rightarrow$ For dry conditions (AMC I)

$$CN(I) = \frac{4.2 \cdot CN(II)}{10 - 0.058 \cdot CN(II)}$$

For wet conditions (AMC III)

$$CN(III) = \frac{23 \cdot CN(II)}{10 + 0.13 \cdot CN(II)}$$

AMC	Total 5-day antecedent rainfall (in)	
	Dormant Season	Growing Season
I	< 0.5	< 1.4
II	0.5 to 1.1	1.4 to 2.1
III	> 1.1	> 2.1

We can define four soil groups based on SCS curve numbers:

- Group A : Deep sand, Deep loess
 Group B : Sandy loam, Shallow loess
 Group C : Clay loams, soils low in organic content, etc.
 Group D : Heavy plastic clay, swelling clays, etc.

⑥

Example:

Compute runoff from 5-inches rainfall on a 1000 acre watershed. The hydrologic soil group is - 50% Group B and 50% Group C.

Assume $AMC(II)$. The land use has:

- 40% residential area having 30% imperviousness
- 12% residential area having 65% imperviousness.
- 18% paved roads with curbs and storm sewers
- 16% open land with 50% grass cover, 50% good grass cover.
- 14% parking lots, plazas, schools, etc. (Impervious)

Solution

Total Area = 1000 Acres.

∴ Residential area → 20% Similarly others

We need to compute weighted soil curve number for the given watershed.

Land Use	Soil Group B			Soil Group C		
	%	B CN	(% x CN)	%	C CN	
Residential (30% Imp.)	20	72	1440	20	81	1620
" (65% Imp.)	6	85	510	6	90	540
Roads	9	98	882	9	98	882
Open Land						
grass cover	4	69	276	4	79	316
good grass cover	4	61	244	4	74	296
Parking Lot	7	98	686	7	98	686
	<u>50</u>		<u>4038</u>	<u>50</u>		<u>4340</u>

(7)

$$\therefore \text{Weighted CN} = \frac{4038 + 4340}{50 + 50} = 83.8$$

See
For $AMC(II)$, $S = \frac{1000}{CN} - 10$

$$= \frac{1000}{83.8} - 10 = 1.93 \text{ in}$$

$$\therefore P_e = \frac{(P - 0.2S)^2}{P + 0.8S}$$

$$= \underline{\underline{3.25 \text{ inches}}}$$

So you can see from 5-inch rainfall you have 3.25 inch runoff.

Urbanisation Effects



Infiltration before urbanisation
Infiltration after urbanisation

→ Due to urbanisation soil permeability is reduced. Less water is infiltrated. Therefore there will be more surface runoff.

