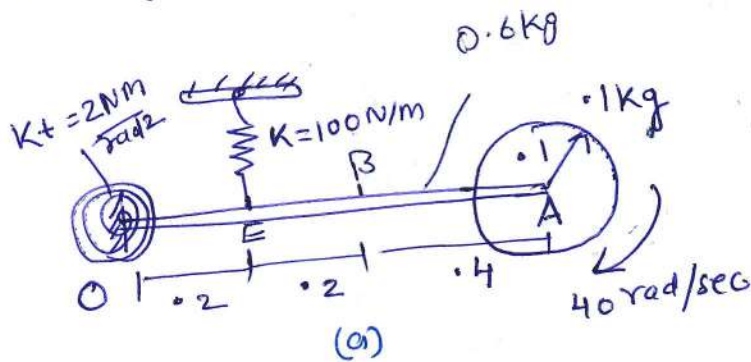


Example 3.16

(1)

A rod OA of mass 0.6 kg is hinged at O to a support and hinged to a thin disc of mass 0.1 kg at A. In a given position, the rod is held stationary, the disc rotates at 40 rad/s, the spring has a compression of 40 mm and the rotational spring is unstretched.

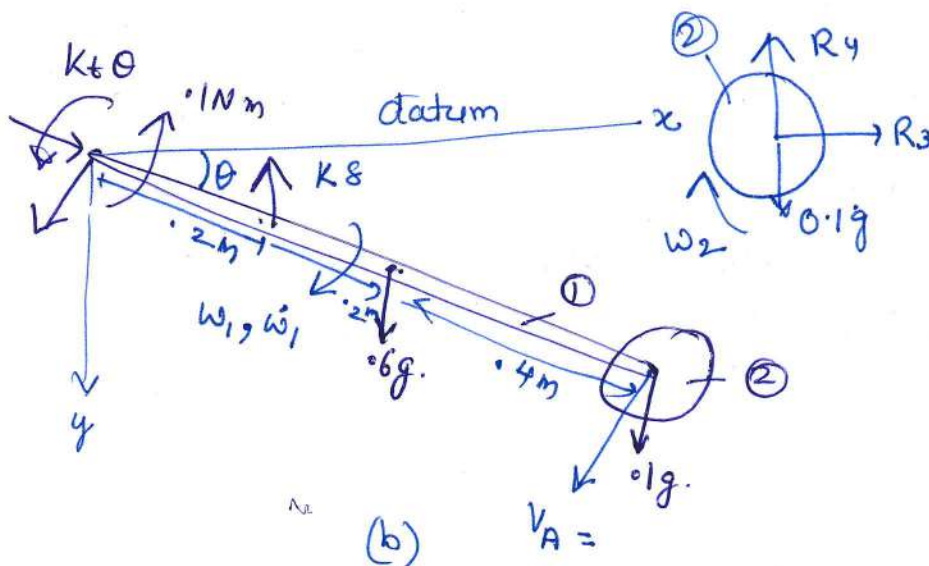


The hinge at A is frictionless and there is constant frictional torque of 0.1 Nm on the rod from hinge at O.

$$M_I = \frac{K \theta^2}{2}$$

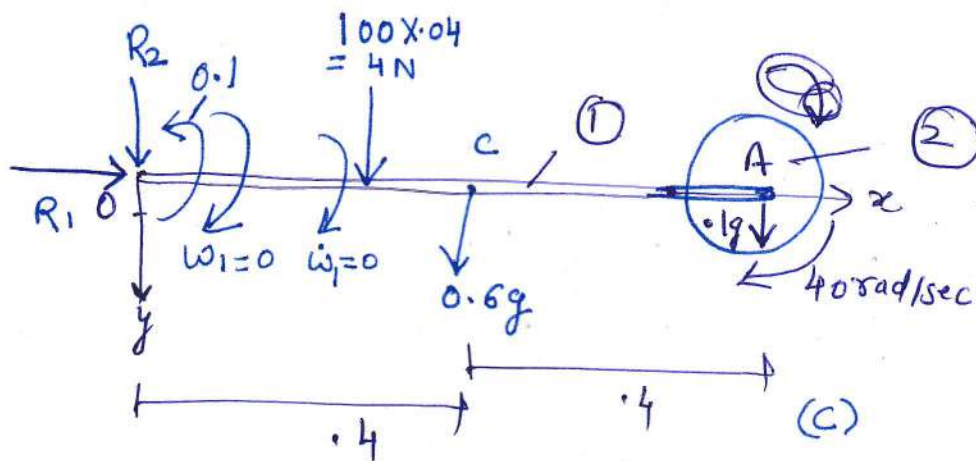
$$\frac{Nm}{rad^2}$$

- The rod is released. Find (a) the angular acceleration of the rod and the reaction from O just after release.
- The angular velocity of the rod, angular acceleration of the rod and the reaction from O when the rod has rotated by 30°
- The normal force, shear force and bending moment in the rod at B when rod has rotated by 30° .



Solution

FBD



For rod 1,

$$m_1 = 0.6 \text{ kg}$$

$$I_{zz}^O = \frac{ml^2}{3} = \frac{0.6 \times 0.8^2}{3} = 0.128 \text{ kg.m}^2$$

For disc $m_2 = 0.1 \text{ kg}$, $I_{zz}^A = \frac{mr^2}{2} = \frac{0.1(0.1)^2}{2} = 0.0005 \text{ kg.m}^2$

Let ω_1 = angular velocity of rod
 ω_2 = angular velocity of disc

For the general position of the centre of mass A of disc 2

$$\bar{M}_A = 0, \quad I_{zz}^A \dot{\omega}_2 \Rightarrow 0, \quad \dot{\omega}_2 = 0 \Rightarrow \omega_2 = \text{Constant}$$

$$\omega_2 = 40 \text{ rad/s}$$

The extension of the spring is $\delta = 0.2 \sin \theta - 0.04 \text{ m}$

$$v_A = 0.8 \omega_1 \bar{e}_\theta$$

For rod + disc, Horiz, Kinetic Energy, Potential Energy V.
 for general position θ .

$$H_{O_2} = I_{zz}^O \omega_1 + (I_{zz}^A \omega_2 + 0.8 m_2 v_A)$$

(3)

$$= .128 \omega_1 + 0.0005 \times 40 + 0.8 \times .1 \times 0.8 \omega_1 \Rightarrow 0.192 \omega_1 + 0.02 \quad \text{--- (1)}$$

$$T = \frac{1}{2} I_{zz}^O \omega_1^2 + \left[\frac{1}{2} [m_2 v_A^2] + \frac{1}{2} I_{zz}^A \omega_2^2 \right]$$

$$= \frac{1}{2} \times .128 \omega_1^2 + \frac{1}{2} \left[\frac{0.128}{2} \omega_1^2 \right] + \frac{1}{2} \times .1 \times (.8) \omega_1^2 + 0.0005 \times 40^2$$

$$\Rightarrow 0.096 \omega_1^2 + 0.41 \quad \text{--- (2)}$$

$$V = \frac{1}{2} k \theta^2 + \frac{1}{2} k (0.2 \sin \theta - 0.04)^2 - m_1 g (0.4 \sin \theta) - m_2 g (0.8 \sin \theta)$$

$$= \theta^2 + 50 (0.2 \sin \theta - 0.04)^2 - 0.32 g \sin \theta$$

(Q) FBD of rod+disc is shown in Fig.

Using equation (1). $\dot{H}_{O_2} = \dot{M}_{O_2} = 0.192 \dot{\omega}_1$

$$\dot{H}_{O_2} = 0.192 \dot{\omega}_1 = \underbrace{-0.1}_{\substack{\downarrow \\ \text{Friction} \\ \text{Torque}}} + \underbrace{4 \times 0.2}_{\substack{\downarrow \\ \text{Spring}}} + \underbrace{0.6g \times 0.4}_{\substack{\downarrow \\ \text{Rod weight}}} + \underbrace{0.1g (0.8)}_{\substack{\downarrow \\ \text{disk}}}$$

$$\Rightarrow \dot{\omega}_1 = 20.00 \text{ rad/s}^2$$

Applying Newton's Law, R_1, R_2 can be calculated, 1

$$\vec{F} = m \vec{a}_c$$

~~Initial there is not a~~

For the present state $\omega_1 = 0$, R_1, R_2 can be obtained

$$\vec{a}_c = \gamma \alpha + \omega \times (\omega \times r) = \dot{\omega}_1 \hat{k} \times 0.4 \hat{i} + \omega_1^2 (-) \hat{i} \Rightarrow 8 \hat{j} \text{ m/s}^2$$

$$\vec{a}_A = \omega_1^2 (.8) \hat{i} + \dot{\omega}_1 (.8) \hat{j} = 16 \hat{j} \text{ m/s}^2$$

$$\begin{aligned} \omega_1 &= 0 \\ \dot{\omega}_1 &= \dot{\omega}_1 \\ \dot{\omega}_1 &= \dot{\omega}_1 \\ \omega &= \frac{d\theta}{dt} \\ \frac{d\theta}{dt} &= \omega \\ \theta &= \int \omega dt \\ \theta &= C(t) \\ \frac{d\theta}{dt} &= 0 \end{aligned}$$

$$\bar{F} = \sum m_i \bar{a}_i$$

$$\Rightarrow R_1 \hat{i} + R_2 \hat{j} + (4 + 0.06g + 0.1g) \hat{j} \\ = 0.6 \times 8 \hat{j} + 0.1 \times 16 \hat{j}$$

$$R_1 = 0, \quad R_2 = -4.467 \text{ N.}$$

(b) Work-energy relation from the configuration 1 for $\theta = 0$ to configuration 2 for $\theta = 30^\circ = \pi/6$

yields ω_1 .

Using eq (1), yield ω_1 . R_1, R_2 are obtained using

$\bar{F} = \sum m_i \bar{a}_i$ and kinematic.

The pull on the spring for $\theta = 30^\circ$

$$100 (0.2 \sin 30 - 0.04) = 6 \text{ N}$$

$$(T_2 + V_2) - (T_1 + V_1) = W_{nc1-2}$$

Using eq. (2) and (3)

$$\begin{aligned} & [0.096 \omega_1^2 + 0.4] + \left\{ \left(\frac{\pi}{6} \right)^2 + 50 (0.2 \sin 30 - 0.04)^2 \right. \\ & \left. - 0.32g \sin 30 \right\} - [0.4 + 50 (-0.04)^2] = \underbrace{-0.1 \frac{\pi}{6}}_{\parallel} \end{aligned}$$

$$\Rightarrow \omega_1 = 3.451 \text{ rad/sec.}$$

$$\dot{H}_O z = M_O z.$$

Work done
by frictional Torque

$$0.192 \dot{\omega}_1 = -0.1 - 100 (0.2 \sin 30 - 0.04) (0.2 \cos 30) \\ + 0.6g (0.4 \cos 30) + 0.1g (0.8 \cos 30) - 2 \left(\frac{\pi}{6} \right)$$

$$\dot{\omega}_1 = 2.772 \text{ rad/s}^2$$

(5)

$$\begin{aligned}\bar{a}_C &= -\omega_1^2 (0.4) \bar{e}_r + \dot{\omega}_1 (0.4) \bar{e}_\phi \\ &= -4.7638 \bar{e}_r + 1.1088 \bar{e}_\phi \text{ m/s}^2\end{aligned}$$

$$\begin{aligned}\bar{a}_A &= -\omega_1^2 (0.8) \bar{e}_r + \dot{\omega}_1 (0.8) \bar{e}_\phi \\ &\Rightarrow -9.5275 \bar{e}_r + 2.2176 \bar{e}_\phi \text{ m/s}^2\end{aligned}$$

$$\bar{F} = \sum M_i \bar{a}_{ci}$$

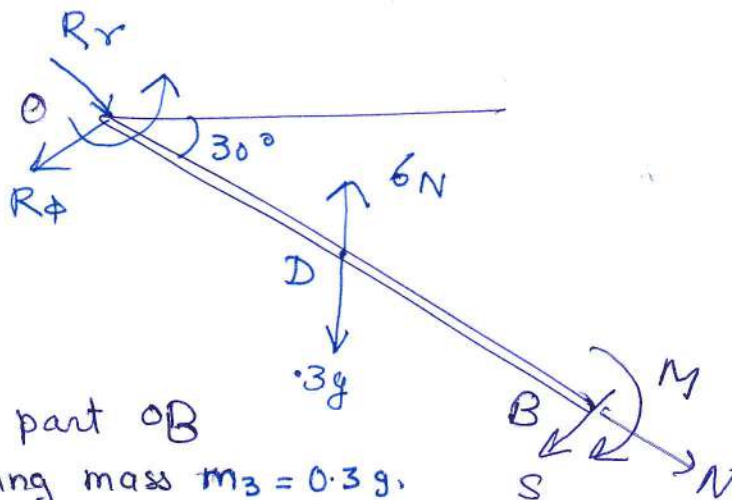
$$\bar{e}_r : R_r + (0.6g + 0.1g - 6) \sin 30^\circ = 0.6 \times -4.7638 + 0.1(-9.5275)$$

$$\Rightarrow R_r = -4.245 \text{ N}$$

$$\bar{e}_\phi : R_\phi + (0.6g + 0.1g - 6) \cos 30^\circ = 0.6(1.1088) + 0.1 \times 2.2176$$

$$\Rightarrow R_\phi = 0.1362 \text{ N}$$

(c)



The FBD of part OB of the rod having mass $m_3 = 0.3 \text{ g}$.

N & M are obtained using equation of motion

$$F_r = m_3 a_{Dr} \Rightarrow R_r + N + (0.3g - 6) \sin 30^\circ = -m_3 \omega_1^2 (0.2) \Rightarrow N = 5.059 \text{ N}$$

$$F_\phi = m_3 a_{D\phi} \Rightarrow R_\phi + S + (0.3g - 6) \cos 30^\circ = m_3 \dot{\omega}_1 (0.2) \Rightarrow S = 2.814$$

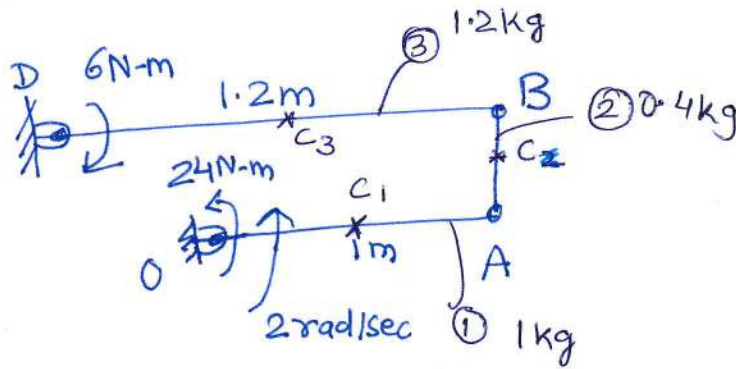
$$M_{Oz} = I_{zz}^O \dot{\omega}_1 \Rightarrow M - 0.1 - 2 \times \pi/4 + (0.3g - 6)(0.2 \cos 30^\circ) + S(0.4) = 0.3(0.4)^2/3 \dot{\omega}_1$$

$$M = 0.5954 \text{ N-m}$$

Example No 3.17 PC Dumir

①

A 4-bar Linkage moves in a vertical plane under input torque of 24 N-m on the driver link 1 and a torque of 6 N-m on the driven link 3 (see Fig). Find the support reactions at given instant



Solution:

First step: We first express $\omega_2, \omega_3, \dot{\omega}_2, \dot{\omega}_3$ in terms of ω_1 and $\dot{\omega}_1$ using kinematics of the connected linkages.

Point O, A on body 1; A, B, C on body 2 and D, B on body 3 have the same plane of motion.

$$\bar{\omega}_1 = 2\hat{k} \text{ rad/sec}, \quad \bar{\omega}_2 = \omega_2\hat{k}, \quad \bar{\omega}_3 = \omega_3\hat{k}, \quad \bar{v}_O = \bar{v}_D = 0$$

$$\bar{AB} = 0.4\hat{j} \text{ m}, \quad \bar{DB} = 1.2\hat{i}$$

$$\dot{\bar{\omega}}_1 = \dot{\omega}_1\hat{k}, \quad \dot{\bar{\omega}}_2 = \dot{\omega}_2\hat{k}, \quad \dot{\bar{\omega}}_3 = \dot{\omega}_3\hat{k}, \quad \bar{a}_O = \bar{a}_D = 0$$

$$\bar{AC} = 0.2\hat{j}, \quad \bar{OA} = 1\hat{i} \text{ m}$$

$$\boxed{\bar{v}_A = \omega_1(\bar{OA})\hat{j} = 2 \times 1\hat{j} = 2\hat{j}}, \quad \bar{v}_B = v_A + \omega_2\hat{k} \times \bar{AB} = \omega_3(\bar{DB})\hat{j}$$

$$\text{Now } 2\hat{j} + \omega_2\hat{k} \times 0.4\hat{j} = \omega_3(1.2)\hat{j} \Rightarrow 2\hat{j} - 0.4\omega_2\hat{i} = 1.2\omega_3\hat{j}$$

$$\text{Equation coefficient } \Rightarrow 2\hat{j} - 0.4\omega_2\hat{i} = 0, \quad 2 = 1.2\omega_3$$

$$\Rightarrow \omega_2 = 0, \quad \omega_3 = 1.667 \text{ rad/s.}$$

$$\bar{a}_A = -\omega_1^2 (OA) \hat{i} + \dot{\omega}_1 (OA) \hat{j} \Rightarrow -4 \hat{i} + \dot{\omega}_1 \hat{j}$$

$$\bar{a}_B = a_A - \omega_2^2 \bar{AB} + \dot{\omega}_2 \hat{k} \times \bar{AB} = -\omega_3^2 (DB) \hat{i} + \dot{\omega}_3 (DB) \hat{j}$$

$$\Rightarrow -4 \hat{i} + \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{k} \times 0.4 \hat{j} = -1.667^2 (1.2) \hat{i} + \dot{\omega}_3 (1.2) \hat{j}$$

Equating i & j component.

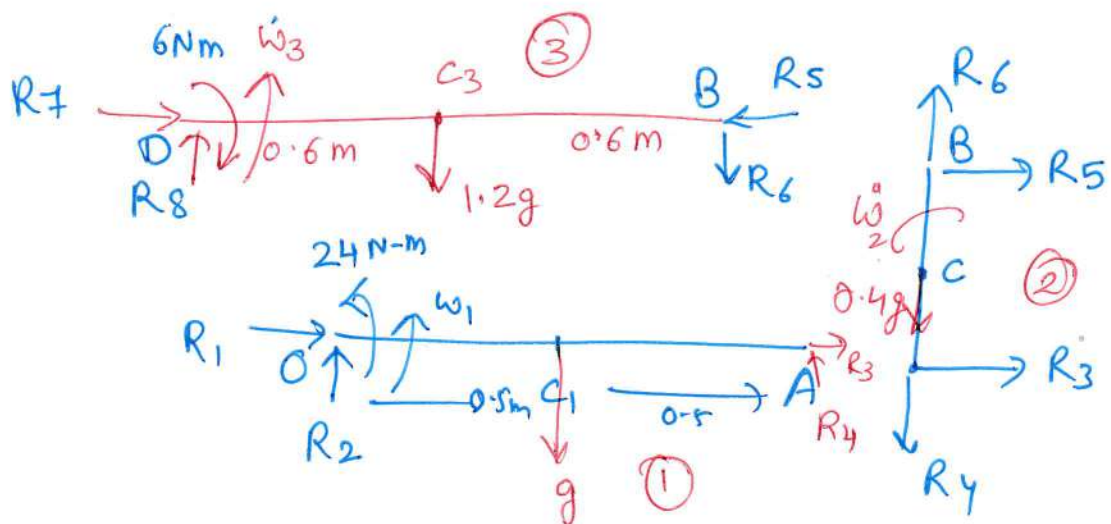
$$-4 - 0.4 \dot{\omega}_2 = -3.333 \Rightarrow \dot{\omega}_2 = -1.667 \text{ rad/sec}^2$$

$$\dot{\omega}_1 = 1.2 \dot{\omega}_3 \Rightarrow \dot{\omega}_3 \Rightarrow 0.8333 \dot{\omega}_1$$

$$\bar{a}_C = \bar{a}_A - \omega_2^2 \bar{AC} + \dot{\omega}_2 \hat{k} \times \bar{AC} = -4 \hat{i} + \dot{\omega}_1 \hat{j} + \dot{\omega}_2 \hat{k} \times 0.2 \hat{j}$$

$$\Rightarrow -3.6667 \hat{i} + \dot{\omega}_1 \hat{j}$$

FBD



For Link 1

$$M_{O2} = I_{O2} \dot{\omega}_1 \Rightarrow 24 - 0.5g + R_4 = \left(\frac{1 \times 1^2}{3}\right) \dot{\omega}_1$$

$$\Rightarrow R_4 = -19.095 + 0.333 \dot{\omega}_1$$

For Link 3.

$$M_{D2} = I_{D2} \dot{\omega}_3 = -6 - 1.2g(0.6) - 1.2R_6 = \frac{1.2(1.2)^2}{3} \dot{\omega}_3$$

$$\Rightarrow R_6 = -10.866 - 0.4 \dot{\omega}_1$$

(3)

For link 2

$$F_y = m_2 a_{cy} = R_6 - R_4 - 0.4g = 0.4\dot{\omega}_1$$

Now substitute the value of R_6 & R_4 in the above equation.

$$\dot{\omega}_1 = 3.781 \text{ rad/s}^2$$

For link 2

$$M_{C_2} = I_{C_2} \dot{\omega}_2 = -0.2(R_5 + R_3) = \left(\frac{0.4(0.4)^2}{12} \right) (-1.667)$$

$$R_5 + R_3 = 0.0444 \quad \text{--- (a)}$$

$$F_x = m_2 a_{cx} = R_5 - R_3 = 0.4(-3.667) = -1.4667 \quad \text{(b)}$$

From (a) & (b)

$$R_5 = -0.711 \text{ N}, \quad R_3 = +7.55 \text{ N}$$

Link 1

$$F_x = m_1 a_{c1x} \Rightarrow R_1 + R_3 = 1(-\dot{\omega}_1^2(0.5)) = R_1 = -2.756 \text{ N}$$

$$F_y = m_1 a_{c1y} \Rightarrow R_2 + R_4 - g = 1[\dot{\omega}_1(0.5)]$$

$$\Rightarrow R_2 = 29.53 \text{ N}$$

Link 3

$$F_x = m_3 a_{c3x} \Rightarrow R_7 - R_5 = 1.2(-\dot{\omega}_3^2(0.5))$$

$$R_7 = -2.711 \text{ N}$$

$$F_y = m_3 a_{c3y} \Rightarrow R_8 - R_6 - 1.2g = 1.2(\dot{\omega}_3(0.4))$$

$$\Rightarrow R_8 = 1.641 \text{ N}$$