

CONSERVATION EQUATIONS

We have seen yesterday in a multi-specie moving fluid continuum, the Eulerian approach to write the conservation of any extensive property G_α is given as:

$$\int_V \frac{\partial g_\alpha}{\partial t} dV + \int_S g_\alpha (\vec{V}_{G\alpha} \cdot \hat{n}) dS = \int_V I_\alpha dV$$

or for any arbitrary volume V

$$\frac{\partial g_\alpha}{\partial t} + \nabla \cdot (g_\alpha \vec{V}_{G\alpha}) = I_\alpha \rightarrow \textcircled{1}$$

where $g_\alpha \rightarrow$ the density of the extensive property G_α
 $\vec{V}_{G\alpha} \rightarrow$ the velocity of propagation of the extensive property G_α (i.e. property G for a α -specie)

$I_\alpha \rightarrow$ Production of the property G_α per unit volume per unit time.

① This general conservation principle can be applied for developing conservation equations for

- \rightarrow Mass
 - \rightarrow Momentum
 - \rightarrow Energy
- } \rightarrow The various extensive properties

(2)

1) Mass conservation of a specie α

Yesterday again we discussed on this aspect and formed the equation:

$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha) = I_\alpha \rightarrow (2)$$

Again using $\rho_\alpha = \rho_\alpha$ and $\vec{V}_{\alpha\alpha} = \vec{V}^*$ in equation (1) we can form the another material derivative for ρ_α such that

$$\frac{D^* \rho_\alpha}{Dt} = \frac{\partial \rho_\alpha}{\partial t} + (\vec{V}^* \cdot \nabla) \rho_\alpha$$

$$\text{or } \frac{D^* \rho_\alpha}{Dt} = \frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) - \rho_\alpha (\nabla \cdot \vec{V}^*) \rightarrow (3)$$

2) We also know diffusive velocity for specie α

$$\vec{V}_\alpha^{\hat{}} = \vec{V}_\alpha - \vec{V}^*$$

and diffusive mass flux

$$\vec{J}_\alpha^* = \rho_\alpha \vec{V}_\alpha^{\hat{}} = \rho_\alpha (\vec{V}_\alpha - \vec{V}^*) \rightarrow (a)$$

(found based on mass average velocity)

Utilising the information in (3) and (a) in (2) we will get:

(3)

$$\frac{\partial \rho_\alpha}{\partial t} + \underbrace{\nabla \cdot (\rho_\alpha \vec{V}^*)}_{\text{Advection or convective component of mass flux of } \alpha\text{-species}} + \underbrace{\nabla \cdot \vec{J}_\alpha^*}_{\text{Diffusive or conductive mass flux of } \alpha\text{-species}} = I_\alpha \rightarrow (4)$$

$\rho_\alpha \vec{V}^*$ = Advection or convective component of mass flux of α -species

\vec{J}_α^* = Diffusive or conductive mass flux of α -species

2) Mass conservation of the entire fluid

In equation (1) put $\rho_{G\alpha} = \rho$ and $g_\alpha = \rho$ (the density of entire fluid system)

We will now get

$$\boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{V}^*) = 0} \rightarrow (5)$$

Q: Why $I_\alpha = 0$ in equation (5)?

When talking about the entire fluid and considering the mass average velocity \vec{V}^* , new mass cannot be created or destroyed in the system. The mass of some species may transform to some other species, etc, but new mass cannot be created. $\therefore I_\alpha = 0$.

Hence equation (5) may also be represented as

$$\underline{\underline{\frac{D\rho}{Dt} + \rho (\nabla \cdot \vec{V}^*) = 0}}$$

(4)

For homogeneous incompressible fluid, the average density ρ will not vary w.r.t space and time.

Then the equation for continuity will be

$$\boxed{\nabla \cdot \vec{V}^* = 0} \quad \rightarrow \quad (6)$$

3) Conservation of Linear Momentum of a specie α

In a fluid continuum that is developed on mass (i.e. fluid consist of mass particles), the average mass density is ρ , average mass velocity is \vec{V}^* .

\rightarrow The linear momentum is an extensive property of mass and can now be given as

$$\int_V \rho \vec{V}^* dV$$

\rightarrow Based on this, let us now consider: $G_\alpha \rightarrow$ linear momentum and density of extensive property $g_\alpha =$ linear momentum of specie α per unit volume of multi-specie fluid.

i.e. $g_\alpha = \rho_\alpha \vec{V}_\alpha$

Also let $\vec{V}_{g_\alpha} =$ velocity of propagation of property for α -specie
 $=$ velocity of ~~momentum~~ α -specie momentum particles.
 $= \vec{V}_{m_\alpha}$

(5)

$I_\alpha = I_{m\alpha} \rightarrow$ Rate of production of linear momentum of α -species per unit volume per unit time.

\therefore Equation (1) the conservation equation becomes:

$$\frac{\partial (\rho_\alpha \vec{V}_\alpha)}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha \vec{V}_{m\alpha}) = I_{m\alpha} \rightarrow (7)$$

Now the product $\vec{V}_\alpha \vec{V}_{m\alpha}$ is a dyadic product

(Recall from vector mechanics - if there are two vectors $\vec{u} = u_1 \hat{i}_1 + u_2 \hat{i}_2 + u_3 \hat{i}_3$ and $\vec{v} = v_1 \hat{i}_1 + v_2 \hat{i}_2 + v_3 \hat{i}_3$)

then you can have dyadic product

$$\vec{u} \vec{v} = \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} \{v_1 \ v_2 \ v_3\} = \begin{pmatrix} u_1 v_1 & u_1 v_2 & u_1 v_3 \\ u_2 v_1 & u_2 v_2 & u_2 v_3 \\ u_3 v_1 & u_3 v_2 & u_3 v_3 \end{pmatrix}$$

This dyadic product of two vectors give a second rank tensor.

Now let us define this dyadic product as:

$$\begin{aligned} \vec{J}_{m\alpha} &\rightarrow \text{Flux of momentum of species } \alpha \text{ with respect to a fixed frame of reference.} \\ &= \rho_\alpha \vec{V}_\alpha \vec{V}_{m\alpha} \quad (\text{Please Note that this will be a second-rank tensor}) \end{aligned}$$

Again with mass average velocity \vec{V}^* , if we can define a diffusive momentum velocity ~~and~~

$$\vec{V}_{m\alpha}^* = \vec{V}_{m\alpha} - \vec{V}^*$$

then:

(6)

we can also suggest a diffusive momentum flux

$$\overline{\overline{J}}_{m\alpha}^* = \rho_\alpha \vec{V}_\alpha \vec{V}_{m\alpha} = \rho_\alpha \vec{V}_\alpha (\vec{V}_{m\alpha} - \vec{V}^*)$$

$$\begin{aligned} \text{Now } \overline{\overline{J}}_{m\alpha} &= \rho_\alpha \vec{V}_\alpha \vec{V}_{m\alpha} \\ &= \rho_\alpha \vec{V}_\alpha \vec{V}^* + \overline{\overline{J}}_{m\alpha}^* \end{aligned}$$

∴ Equation (7) becomes:

$$\frac{\partial (\rho_\alpha \vec{V}_\alpha)}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha \vec{V}^*) + \nabla \cdot \overline{\overline{J}}_{m\alpha}^* = I_{m\alpha}$$

↳ (8)

Again you may see advective and diffusive components in the conservation equation.

4) Conservation of Linear Momentum for entire liquid

For the entire fluid,

$$\text{Mass average velocity} = \vec{V}^*$$

$$\text{Mass density} = \rho$$

$$\text{Linear momentum density} \cdot g_\alpha = \rho \vec{V}^*$$

$$\text{Now } G_\alpha = \text{linear momentum for entire fluid}$$

$$= \int \rho \vec{V}^* dV$$

$$\vec{V}_{G\alpha} = \text{velocity of propagation of linear momentum in entire fluid}$$

$$= \vec{V}_m$$

(7)

I_α \rightarrow The rate of production of linear momentum in entire fluid per unit volume per unit time
= Resultant of all external forces acting on the volume.

$\rho \vec{F}_\alpha$ = external force per unit mass of species α acting on this α -species particles

$$\text{Then } I_\alpha = \sum_{\alpha=1}^N \rho_\alpha \vec{F}_\alpha$$

\therefore The general conservation equation becomes

$$\frac{\partial (\rho \vec{V}^*)}{\partial t} + \nabla \cdot (\rho \vec{V}^* \vec{V}_m) = \sum_{\alpha=1}^N \rho_\alpha \vec{F}_\alpha \rightarrow (9)$$

Note: $\vec{V}^* \vec{V}_m \rightarrow$ dyadic product

\therefore let us define

$$\begin{aligned} \overline{\overline{J}}_m &= \text{Momentum flux w.r.t fixed frame of reference} \\ &= \rho \vec{V}^* \vec{V}_m \end{aligned}$$

$$\begin{aligned} \overline{\overline{J}}_m^* &= \text{diffusive momentum flux w.r.t mass average velocity} \\ &= \rho \vec{V}^* (\vec{V}_m - \vec{V}^*) \end{aligned}$$

$$\text{Then } \overline{\overline{J}}_m = \overline{\overline{J}}_m^* + \rho \vec{V}^* \vec{V}^*$$

\therefore Equation (9) becomes:

(8)

$$\frac{\partial (\rho \vec{V}^*)}{\partial t} + \nabla \cdot (\rho \vec{V}^* \vec{V}^*) + \nabla \cdot \bar{\bar{J}}_m^* = \sum_{\alpha=1}^3 \rho_{\alpha} \vec{F}_{\alpha}$$

↳ (10)

Again you can see in equation (10) that while evaluating ~~the~~ linear momentum conservation ~~of~~ there are advective momentum fluxes and conductive momentum fluxes.

Q: What is this conductive or diffusive momentum flux?

$$\bar{\bar{J}}_m^*$$

→ This is actually nothing but the negative of the stress tensor

Recall in index notation, stress tensor was given as:

$$\sigma_{ij} = -p \delta_{ij} + \tau_{ij}$$

$$\therefore \bar{\bar{J}}_m^* = -\bar{\bar{\sigma}}$$

$$\text{or } (\bar{\bar{J}}_m^*)_{ij} = -\sigma_{ij}$$

∴ The momentum flux tensor $\bar{\bar{J}}_m = \rho \vec{V}^* \vec{V}_m$

will now become

$$\bar{\bar{J}}_m = \rho \vec{V}^* \vec{V}^* + p \bar{\bar{\delta}} - \bar{\bar{\tau}}$$

$$\text{or } \left((\bar{\bar{J}}_m)_{ij} = \rho V_i^* V_j^* + p \delta_{ij} - \tau_{ij} \quad ; \quad \begin{matrix} i = 1, 2, 3 \\ j = 1, 2, 3 \end{matrix} \right)$$