

The Reynold's Transport Theorem

We can also arrive at the Reynold's Transport theorem by utilising the material derivatives for volumes.

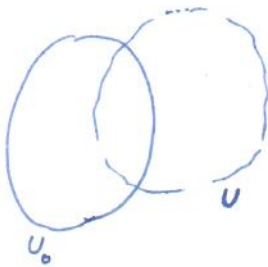
Recall that any extensive property G_α for an α -species in a fluid continuum can also be expressed in terms of its density g_α as:

$$G_\alpha(t) = \int_{[U(t)]} g_\alpha(\vec{x}, t) dU$$

where $G_\alpha(t) \rightarrow$ The amount of G_α instantaneously present in the volume $U(t)$

See that volume of continuum is moving and therefore it deforms (fluid).

i.e. Volume is function of time t . $g_\alpha(\vec{x}, t)$ is density of the extensive property at any spatial location in the continuum.



Again, for a fluid mass particle - if its initial volume is given as dU_0 and represented by position material coordinates $\vec{X} = x_1 \hat{I}_1 + x_2 \hat{I}_2 + x_3 \hat{I}_3$.

When the fluid moves particle moves, we represent it through spatial coordinates \vec{x} .

where now $\vec{x} = \vec{x}(\vec{x}^*)$ function of material coordinates.

In the 3-dimensional orthogonal Cartesian coordinate system

$$\text{let } dU_0 = dx_1 dx_2 dx_3$$

This volume deforms to $dU = dx_1 dx_2 dx_3$

$$\text{Aris (1962) suggested: } dU = J dU_0$$

$$J \rightarrow \text{jacobian} \rightarrow \frac{\partial x_i}{\partial x_j^*}$$

From fluid mechanics we have seen that
Material derivative for this particle volume

$$\frac{D}{Dt}(dU) = \frac{D}{Dt}(J dU_0) = \frac{D J}{Dt} dU_0$$

($\because dU_0$ will not change with time)

$$\frac{D J}{Dt} = J (\nabla \cdot \vec{v}^*) \quad \left(\text{That is divergence of velocity vector} \right)$$

$$\therefore \frac{D}{Dt}(dU) = \frac{D J}{Dt} dU_0 = (\nabla \cdot \vec{v}^*) dU_0 J$$

11b Now for the multi-species component

$$\frac{D g}{Dt} = (\nabla \cdot \vec{v}_{G\alpha}) g$$

$\Rightarrow \therefore$ If we want to take material derivative of G_α

$$\text{where } G_\alpha(t) = \int_{U(t)} g_\alpha(\vec{x}, t) dU,$$

then we need to express $g_\alpha(\vec{x}, t)$ and dU
in terms of material coordinates.

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i.e. We know for the fluid continuum initially the volume is U_0 and represented by material coordinate \vec{x}_α

i.e. Our spatial coordinate at any instant ~~is~~ will

$$\text{be.} \quad \vec{x} = \vec{x}(\vec{x}_\alpha, t)$$

$$\begin{aligned} \therefore \frac{D G_\alpha}{Dt} &= \frac{D}{Dt} \left[\int_{U_\alpha} g_\alpha(\vec{x}, t) dU \right] \\ &= \int_{U_0} \frac{D g_\alpha}{Dt} f dU_0 + \int_{U_0} g_\alpha \frac{D f}{Dt} dU_0 \\ &= \int_{U_0} \left[\frac{\partial g_\alpha}{\partial t} + (\vec{V}_{c\alpha} \cdot \nabla) g_\alpha \right] f dU_0 + \int_{U_0} g_\alpha (\nabla \cdot \vec{V}_{c\alpha}) f dU_0 \\ &= \int_{U_0} \left[\frac{\partial g_\alpha}{\partial t} + \nabla \cdot (g_\alpha \vec{V}_{c\alpha}) \right] f dU_0 \\ &= \int_U \left[\frac{\partial g_\alpha}{\partial t} + \nabla \cdot (g_\alpha \vec{V}_{c\alpha}) \right] dU \end{aligned}$$

$$\text{Now} \quad \int_U \nabla \cdot (g_\alpha \vec{V}_{c\alpha}) dU = \int_S g_\alpha (\vec{V}_{c\alpha} \cdot \hat{n}) dS$$

(Using Gauss divergence theorem).

$$\therefore \frac{D G_\alpha}{Dt} = \int_U \frac{\partial g_\alpha}{\partial t} dU + \int_S g_\alpha (\vec{V}_{c\alpha} \cdot \hat{n}) dS$$

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Cases

If in a volume U , there are ~~no~~ production of property G_α within the volume at a rate

say I_α per unit volume per unit time.
(e.g. due to chemical, internal processes, etc.)

Then

$$\frac{DG_\alpha}{Dt} = \int_U I_\alpha dU$$

$$\therefore \int_U I_\alpha dU = \int_U \frac{\partial g_\alpha}{\partial t} dU + \int_S g_\alpha (\vec{V}_{\alpha\alpha} \cdot \hat{n}) dS$$

The Eulerian point of view is represented.

That is the rate of increase of G_α within the volume U is equal to the sum of the rate at which this property G_α crosses into (or out) through the surface and the rate at which this property is produced within U .

$$\therefore \int_U \frac{\partial g_\alpha}{\partial t} dU + \int_S g_\alpha (\vec{V}_{\alpha\alpha} \cdot \hat{n}) dS = \int_U I_\alpha dU$$

$$\text{i.e.} \int_U \left[\frac{\partial g_\alpha}{\partial t} + \nabla \cdot (g_\alpha \vec{V}_{\alpha\alpha}) - I_\alpha \right] dU = 0$$

As this volume U is arbitrary we need to have then

$$\boxed{\frac{\partial g_\alpha}{\partial t} + \nabla \cdot (g_\alpha \vec{V}_{\alpha\alpha}) = I_\alpha}$$

(5)

This equation is the general conservation principle of a property G of the specie α .

Equation of Mass

1) Mass conservation of α -specie

In the general conservation principle

$$\frac{\partial g}{\partial t} + \nabla \cdot (g \vec{V}_{G\alpha}) = I_\alpha$$

put $g = \rho_\alpha$, $\vec{V}_{G\alpha} = \vec{V}_\alpha$

$$\therefore \frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha) = I_\alpha$$

where I_α will be now $[M L^{-3} T^{-1}]$

→ the rate at which mass of α -specie is produced per unit volume of the system (Maybe by chemical reactions, etc.).

∴ Equation of continuity is:

$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha) = I_\alpha$$

Note that, when the material derivative was

discussed

$$\left\{ \begin{aligned} \frac{D B_\alpha}{Dt} &= \frac{\partial B_\alpha}{\partial t} + (\vec{V}_{G\alpha} \cdot \nabla) B_\alpha \\ &= \frac{\partial B_\alpha}{\partial t} + \nabla \cdot (\vec{V}_{G\alpha} B_\alpha) - B_\alpha (\nabla \cdot \vec{V}_{G\alpha}) \end{aligned} \right\}$$

Using that, we have for

$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}_\alpha) = I_\alpha$$

can be written as:

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$$\frac{D \rho_\alpha}{Dt} + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) = I_\alpha \rightarrow (1)$$

Again if we wish to evaluate in:

$$\frac{D R_\alpha}{Dt} = \frac{\partial R_\alpha}{\partial t} + (\vec{V}_{\alpha\alpha} \cdot \nabla) R_\alpha$$

Put $R_\alpha = \rho_\alpha$, $\vec{V}_{\alpha\alpha} = \vec{V}^*$ (Mean Average velocity)

$$\text{Then } \frac{D^* \rho_\alpha}{Dt} = \frac{\partial \rho_\alpha}{\partial t} + (\vec{V}^* \cdot \nabla) \rho_\alpha \rightarrow (2)$$

We also have $\frac{D \rho_\alpha}{Dt} + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) = I_\alpha \rightarrow (1)$
(Obtained earlier).

From (1) and (2), we can now write:

$$\frac{D^* \rho_\alpha}{Dt} - (\vec{V}^* \cdot \nabla) \rho_\alpha + (\vec{V}_\alpha \cdot \nabla) \rho_\alpha + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) = I_\alpha$$

$$\text{i.e. } \frac{D^* \rho_\alpha}{Dt} + \left[(\vec{V}_\alpha - \vec{V}^*) \cdot \nabla \right] \rho_\alpha + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) = I_\alpha \rightarrow (3)$$

~~$$= \frac{\partial \rho_\alpha}{\partial t} + (\vec{V}^* \cdot \nabla) \rho_\alpha + (\vec{V}_\alpha \cdot \nabla) \rho_\alpha + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) = I_\alpha$$~~

Also note that

$$\frac{D^* \rho_\alpha}{Dt} = \frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) - \rho_\alpha (\nabla \cdot \vec{V}^*)$$

and $\hat{\vec{V}}_\alpha^* = \vec{V}_\alpha - \vec{V}^*$

and we have:

$$\therefore \text{In equation (3),}$$

$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) - \rho_\alpha (\nabla \cdot \vec{V}^*) + \rho_\alpha (\nabla \cdot \hat{\vec{V}}_\alpha^*) = I_\alpha$$

②

ie.
$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) + \rho_\alpha [\nabla \cdot (\vec{V}_\alpha - \vec{V}^*)] + (\vec{V}_\alpha \cdot \nabla) \rho_\alpha = I_\alpha$$

ie.
$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) + \rho_\alpha (\nabla \cdot \vec{V}_\alpha) + (\vec{V}_\alpha \cdot \nabla) \rho_\alpha = I_\alpha$$

or
$$\frac{\partial \rho_\alpha}{\partial t} + \nabla \cdot (\rho_\alpha \vec{V}^*) + \nabla \cdot (\rho_\alpha \vec{J}_\alpha^*) = I_\alpha \rightarrow (4)$$

$\rho_\alpha \vec{V}^*$ → Convective component of the mass flux of the α -species based on mass average velocity \vec{V}^*

\vec{J}_α^* → Diffusive component of the mass flux of the α -species

From the above equation, we can now identify that there can be

↳ Advective flux } for the α -species
 ↳ Diffusive flux }

while considering the mass average velocity \vec{V}^* .

2) Mass conservation for entire fluid

For entire fluid, you have mass density = ρ .
 Mass average velocity = \vec{V}^* .

(8)

Then the conservation equation will be:

$$\frac{\partial \rho}{\partial t}$$

$$\rho_{, \alpha} = \rho$$

$$\vec{v}_{\alpha \alpha} = \vec{v}^*$$

$$I_{\alpha} = 0$$

(\because Because mass cannot be produced in the system)

$$\therefore \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}^*) = 0$$

Case (i)

For incompressible, liquid ^{homogeneous} you have

$$\boxed{\nabla \cdot \vec{v}^* = 0}$$