

CONTINUITY OF COMPRESSIBLE HOMOGENEOUS FLUID IN HOMOGENEOUS ISOTROPIC POROUS MEDIA

Yesterday we derived or formulated the continuity equation of a compressible homogeneous fluid in an homogeneous isotropic porous media. The fluid density was related to the pressure and the continuity equation was described in terms of fluid pressure.

$$\frac{k}{\mu} \nabla^2 p + \frac{k\beta}{\mu} (\nabla p)^2 + \frac{2k\beta g}{\mu} \frac{\partial p}{\partial z} = n\beta \frac{\partial p}{\partial t} \quad \rightarrow \textcircled{1}$$

or  
in index notation

$$\frac{k}{\mu} \left[ \frac{\partial}{\partial x_i} \left( \frac{\partial p}{\partial x_i} \right) + \beta \frac{\partial p}{\partial x_i} \frac{\partial p}{\partial x_i} + 2\beta g \frac{\partial p}{\partial z} \right] = n\beta \frac{\partial p}{\partial t}$$

⇒ To express continuity equation in terms of piezometric head  $\phi^*$

Recall

$$\frac{\partial p}{\partial x} = \rho g \frac{\partial \phi^*}{\partial x} \quad ; \quad \frac{\partial p}{\partial y} = \rho g \frac{\partial \phi^*}{\partial y}$$

$$\text{and} \quad g \frac{\partial \phi^*}{\partial z} = g + \frac{1}{\rho} \frac{\partial p}{\partial z}$$

$$\text{and} \quad \frac{\partial p}{\partial t} = \rho g \frac{\partial \phi^*}{\partial t}$$

(2)

Substituting these expressions in the equation

$$k \left[ \frac{\partial}{\partial x} \left( \frac{\rho}{\mu} \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\rho}{\mu} \frac{\partial p}{\partial y} \right) + \frac{\partial}{\partial z} \left( \frac{\rho}{\mu} \left( \frac{\partial p}{\partial z} + \rho g \right) \right) \right] = n \frac{\partial \rho}{\partial t} \rightarrow \textcircled{2}$$

We will get:

$$k \left[ \frac{\partial}{\partial x} \left( \frac{\rho^2 g}{\mu} \frac{\partial \phi^*}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\rho^2 g}{\mu} \frac{\partial \phi^*}{\partial y} \right) + \frac{\partial}{\partial z} \left( \frac{\rho^2 g}{\mu} \frac{\partial \phi^*}{\partial z} \right) \right] = n \frac{\partial \rho}{\partial t}$$

However, recall  $\rho = \rho(p)$  (i.e.  $\rho = \rho_0 \exp[\beta(p-p_0)]$ )

Also recall, the continuity equation form for this case is eqn. ①.

Substitute the relation between  $\frac{\partial p}{\partial x}$  and  $\frac{\partial \phi^*}{\partial x}$ , etc. in eqn. ①

We will get for eqn. ①

$$\frac{k}{\mu} \left( \frac{\partial^2 p}{\partial x^2} + \frac{\partial^2 p}{\partial y^2} + \frac{\partial^2 p}{\partial z^2} \right) + \frac{\beta k}{\mu} \left( \left( \frac{\partial p}{\partial x} \right)^2 + \left( \frac{\partial p}{\partial y} \right)^2 + \left( \frac{\partial p}{\partial z} \right)^2 \right) + \frac{2k\rho g\beta}{\mu} \frac{\partial p}{\partial z} = n\beta \frac{\partial p}{\partial t} \rightarrow \textcircled{1}$$

$$\begin{aligned} \frac{\partial^2 p}{\partial x^2} &= \frac{\partial}{\partial x} \left( \frac{\partial p}{\partial x} \right) = \frac{\partial}{\partial x} \left( \rho g \frac{\partial \phi^*}{\partial x} \right) = \rho g \frac{\partial^2 \phi^*}{\partial x^2} + g \frac{\partial \rho}{\partial x} \frac{\partial \phi^*}{\partial x} \\ &= \rho g \frac{\partial^2 \phi^*}{\partial x^2} + g \beta \rho \frac{\partial p}{\partial x} \frac{\partial \phi^*}{\partial x} \\ &= \rho g \frac{\partial^2 \phi^*}{\partial x^2} + \rho^2 g^2 \beta \left( \frac{\partial \phi^*}{\partial x} \right)^2 \end{aligned}$$

$$\text{||} \frac{\partial^2 p}{\partial y^2} = \rho g \frac{\partial^2 \phi^*}{\partial y^2} + \rho^2 g^2 \beta \left( \frac{\partial \phi^*}{\partial y} \right)^2$$

(3)

$$\begin{aligned}\frac{\partial^2 p}{\partial z^2} &= \frac{\partial}{\partial z} \left( \frac{\partial p}{\partial z} \right) = \frac{\partial}{\partial z} \left( \rho g \left( \frac{\partial \phi^*}{\partial z} - 1 \right) \right) \\ &= \frac{\partial}{\partial z} \left( \rho g \frac{\partial \phi^*}{\partial z} \right) - \frac{\partial (\rho g)}{\partial z} \\ &= \rho g \frac{\partial^2 \phi^*}{\partial z^2} + \beta \rho s^2 g^2 \left( \frac{\partial \phi^*}{\partial z} \right)^2 - g \beta \rho s^2 g \frac{\partial \phi^*}{\partial z} + \beta \rho s^2 g^2\end{aligned}$$

$$\begin{aligned}\text{Again } \left( \frac{\partial p}{\partial x} \right)^2 &= \rho^2 g^2 \left( \frac{\partial \phi^*}{\partial x} \right)^2 \\ \left( \frac{\partial p}{\partial y} \right)^2 &= \rho^2 g^2 \left( \frac{\partial \phi^*}{\partial y} \right)^2 \\ \left( \frac{\partial p}{\partial z} \right)^2 &= \rho^2 g^2 \left( \frac{\partial \phi^*}{\partial z} - 1 \right)^2 \\ \text{and } \frac{\partial p}{\partial t} &= \rho g \frac{\partial \phi^*}{\partial t}\end{aligned}$$

∴ We have equation (1) as:

$$\begin{aligned}\frac{k}{\mu} \rho g \left( \frac{\partial^2 \phi^*}{\partial x^2} + \frac{\partial^2 \phi^*}{\partial y^2} + \frac{\partial^2 \phi^*}{\partial z^2} \right) + \frac{k \beta \rho s^2 g^2}{\mu} \left( \left( \frac{\partial \phi^*}{\partial x} \right)^2 + \left( \frac{\partial \phi^*}{\partial y} \right)^2 + \left( \frac{\partial \phi^*}{\partial z} \right)^2 \right) \\ - \frac{k \beta \rho s^2 g^2}{\mu} \frac{\partial \phi^*}{\partial z} + \frac{k \beta \rho s^2 g^2}{\mu} + \frac{k \beta \rho s^2 g^2}{\mu} \left( \left( \frac{\partial \phi^*}{\partial x} \right)^2 + \left( \frac{\partial \phi^*}{\partial y} \right)^2 + \left( \frac{\partial \phi^*}{\partial z} - 1 \right)^2 \right) \\ + \frac{2 k g \rho \beta}{\mu} \rho g \left( \frac{\partial \phi^*}{\partial z} - 1 \right) = \rho \beta \rho g \frac{\partial \phi^*}{\partial t} \quad \rightarrow (3)\end{aligned}$$

Cancel or eliminate  $\rho g$  throughout equation (3) we get:

$$\begin{aligned}\frac{k}{\mu} \left( \frac{\partial^2 \phi^*}{\partial x^2} + \frac{\partial^2 \phi^*}{\partial y^2} + \frac{\partial^2 \phi^*}{\partial z^2} \right) + \frac{k \beta \rho s^2 g^2}{\mu} \left[ \left( \frac{\partial \phi^*}{\partial x} \right)^2 + \left( \frac{\partial \phi^*}{\partial y} \right)^2 + \left( \frac{\partial \phi^*}{\partial z} \right)^2 \right] \\ - \frac{k \beta \rho s^2 g^2}{\mu} \frac{\partial \phi^*}{\partial z} + \frac{k \beta \rho s^2 g^2}{\mu} + \frac{k \beta \rho s^2 g^2}{\mu} \left[ \left( \frac{\partial \phi^*}{\partial x} \right)^2 + \left( \frac{\partial \phi^*}{\partial y} \right)^2 + \left( \frac{\partial \phi^*}{\partial z} \right)^2 \right] - \frac{2 k \beta \rho s^2 g^2}{\mu} \frac{\partial \phi^*}{\partial z} \\ + \frac{k \beta \rho s^2 g^2}{\mu} + \frac{2 k \beta \rho s^2 g^2}{\mu} \frac{\partial \phi^*}{\partial z} - \frac{2 k \beta \rho s^2 g^2}{\mu} = \rho \beta \frac{\partial \phi^*}{\partial t}\end{aligned}$$

(4)

i.e.

$$\frac{k}{\mu} \nabla^2 \phi^* + \frac{2k\beta s g}{\mu} [(\nabla \phi^*)^2] - \frac{k\beta s g}{\mu} \frac{\partial \phi^*}{\partial z} = n\beta \frac{\partial \phi^*}{\partial t}$$

↳ (4)

If we define hydraulic conductivity  $K = \frac{k s g}{\mu} = \text{a constant}$

Then

$$K \nabla^2 \phi^* + 2K\beta s g (\nabla \phi^*)^2 - K\beta s g \frac{\partial \phi^*}{\partial z} = n\beta s g \frac{\partial \phi^*}{\partial t}$$

↳ (5)

If we neglect higher degree differential terms, then equation (5) reduces to:

$$K \nabla^2 \phi^* - K\beta s g \frac{\partial \phi^*}{\partial z} = n\beta s g \frac{\partial \phi^*}{\partial t}$$

## Mass Conservation of Homogeneous Compressible

### Fluid in a Deforming Porous Media

Earlier we were discussing about continuity equation in a non-deforming porous media.

Recall the general continuity equation for a homogeneous fluid:

$$\nabla \cdot (s \vec{q}) + \frac{\partial (n s)}{\partial t} = 0$$

⑤

i.e.

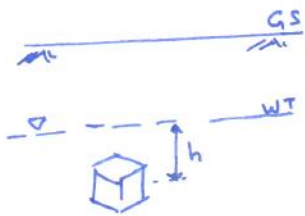
$$\frac{\partial}{\partial x} (\rho q_x) + \frac{\partial}{\partial y} (\rho q_y) + \frac{\partial}{\partial z} (\rho q_z) + n \frac{\partial p}{\partial t} + S \frac{\partial n}{\partial t} = 0$$

Now here:  $S \frac{\partial n}{\partial t} \neq 0$  because of consolidation or deformation of porous media.

⇒ In confined aquifers when the water is pumped, there are chances of consolidation

Matrix & Medium Compressibilities

A porous medium volume at some depth below ground surface is subjected to - hydrostatic pressure (p) and extend stress (σ) exerted by the porous formation above it. Consolidation of the porous medium can occur.



Coefficient of bulk compressibility -  $\alpha'_b$  w.r.t. extend stress σ  
 → In a saturated porous medium, Bulk volume of the porous medium fractional change in with unit change in σ.

$$\alpha'_b = - \frac{1}{U_b} \frac{dU_b}{d\sigma} \Big|_{p = \text{constant}}$$

$U_b$  → volume of fixed mass of the porous medium.  
 Most of the time σ remains approximately same throughout.

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We can define coefficient of bulk compressibility ( $\alpha_b$ ) with respect to liquid pressure (p).

$$\alpha_b = - \frac{1}{U_b} \frac{dU_b}{dp} \Big|_{T = \text{constant}}$$

As the volume of porous medium  $U_b = U_s + U_p$

$U_s \rightarrow$  volume of rock matrix

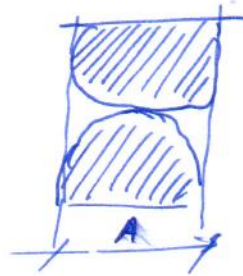
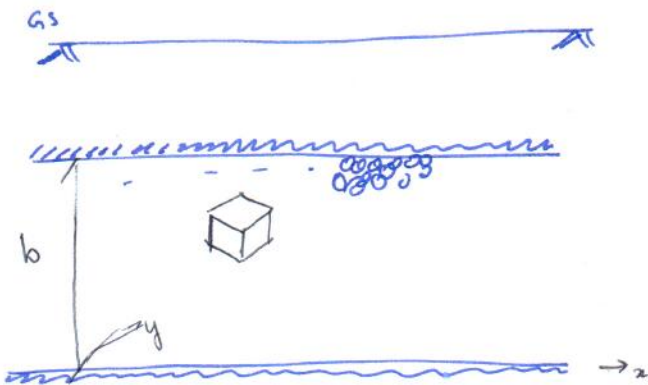
$U_p \rightarrow$  volume of pores

We can also define rock compressibility  $\alpha_s$

$$\alpha_s = - \frac{1}{U_s} \frac{dU_s}{dp} \Big|_{T = \text{constant}}$$

or Pore compressibility,  $\alpha_p = - \frac{1}{U_p} \frac{dU_p}{dp} \Big|_{T = \text{constant}}$

Now consider a confined sizer as shown in fig. below.



$\rightarrow$  In the confined sizer - let us neglect molecular and inter-particle forces among individual grains.

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→ Moreover we assume individual grains are not compressible.

→ From the expanded cross-sectional area  $A$

$$\text{Solid-solid contact area} = mA$$

$$\text{Water solid contact area} = (1-m)A$$

→ If  $p$  is pressure in water

$\sigma_s$  → stress in solid

Then total ~~stress~~ <sup>force balance,</sup>  $\sigma A = p(1-m)A + \sigma_s mA$

∴ Total stress,  $\sigma = p(1-m) + \sigma_s m$

Mathly  $m \ll 1.0$

The quantity  $m\sigma_s$  = defined as effective stress  $\sigma'$

$$\therefore \sigma = \sigma' + (1-m)p$$

Also  $(1-m)p \approx p$

$$\therefore \boxed{\sigma = \sigma' + p}$$

Effective stress concept.

Now changes in porosity will be due to

→ Variations in effective stress,  $\sigma'$

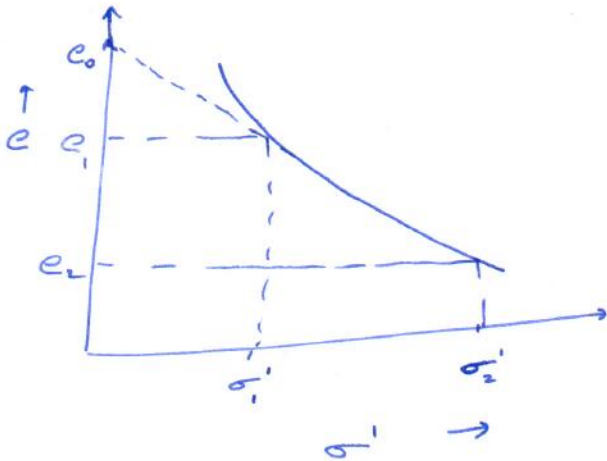
→ Variations in water pressure,  $p$

$$d\sigma = d\sigma' + dp$$

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$$\text{Void ratio } e = \frac{n}{1-n}$$

In one-dimensional analysis, the relation between void ratio and effective stress can be plotted:



$$e = e_0 - \alpha^* \sigma'$$

where  $\alpha^* \rightarrow$  slope of the straight line in the graph.

$\alpha^* \rightarrow$  compressibility coefficient of soil

$$e = e_0 - \alpha^* \sigma'$$

$$\therefore \frac{\partial e}{\partial \sigma'} = -\alpha^*$$

$$\text{i.e. } \frac{\partial}{\partial \sigma'} \left( \frac{n}{1-n} \right) = \frac{1}{1-n} \frac{\partial n}{\partial \sigma'} + \frac{n}{(1-n)^2} \frac{\partial n}{\partial \sigma'}$$

$$= \frac{1}{(1-n)^2} \frac{\partial n}{\partial \sigma'}$$

$$\text{i.e. } \frac{1}{(1-n)^2} \frac{\partial n}{\partial \sigma'} = -\alpha^* \frac{\partial \sigma'}{\partial \sigma'}$$
$$= -\alpha^* \left( \frac{\partial \sigma}{\partial \sigma} - \frac{\partial p}{\partial \sigma} \right)$$