

STREAM FUNCTION

Last classes, we described about the differential equations that can be used to represent:

- \* the conservation of mass
- \* the linear momentum principle
- \* the energy principle

⇒ We also saw that we need to apply appropriate conditions to solve these differential equations in the respective fluid flow domain.

⇒ For some of the fluid problems, where the flow field varies predominantly in  $x$ -,  $y$ - directions only and no variations in  $z$ - direction, then the derivatives in the direction of  $z$ - can be neglected.

e.g: The continuity equation for incompressible fluid can be given as:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad \rightarrow (1)$$

⇒ To utilise the mathematical property, we can define a <sup>scalar</sup> function  $\psi$ , such that the above continuity equation (1) is satisfied.

(2)

That is, (1) can be written as:

$$\frac{\partial}{\partial x} \left( \frac{\partial \psi}{\partial y} \right) + \frac{\partial}{\partial y} \left( -\frac{\partial \psi}{\partial x} \right) = 0$$

where  $\psi(x, y)$  is a function called stream function.

$\Rightarrow$  Now it is clear,

$$u = \frac{\partial \psi}{\partial y}, \quad \text{and} \quad v = -\frac{\partial \psi}{\partial x}$$

$\Rightarrow$  Utilising  $\psi$  will help us to reduce the number of unknowns to one (i.e.  $\psi$ ) and utilise it directly in linear momentum equation to solve for fluid flow in the domain.

$$\text{i.e.} \quad \vec{v} = \frac{\partial \psi}{\partial y} \hat{i} - \frac{\partial \psi}{\partial x} \hat{j}$$

Therefore, in the momentum equation

$$\rho \left[ \frac{\partial \vec{v}}{\partial t} + u \frac{\partial \vec{v}}{\partial x} + v \frac{\partial \vec{v}}{\partial y} + \omega \frac{\partial \vec{v}}{\partial z} \right] = \rho \vec{g} - \vec{\nabla} p + \mu \nabla^2 \vec{v}$$

As the flow is in  $x, y$ -directions and also steady,

we can write:

$$u \frac{\partial \vec{v}}{\partial x} + v \frac{\partial \vec{v}}{\partial y} = \vec{g} - \frac{1}{\rho} \vec{\nabla} p + \frac{\mu}{\rho} \left( \frac{\partial^2 \vec{v}}{\partial x^2} + \frac{\partial^2 \vec{v}}{\partial y^2} \right) \rightarrow (2)$$

If we take curl of equation (2), we get:

$$\text{i.e.} \quad \vec{\nabla} \times [ \quad ] = \vec{\nabla} \times [ \quad ]$$

(3)

$$\vec{\omega} = \left[ u \frac{\partial^2 v}{\partial x^2} - u \frac{\partial^2 u}{\partial x \partial y} + v \frac{\partial^2 u}{\partial y^2} - v \frac{\partial^2 v}{\partial x \partial y} \right] \hat{k}$$

$$= \frac{\mu}{\rho} \left[ \vec{\nabla} \times \frac{\partial^2 \vec{v}}{\partial x^2} + \vec{\nabla} \times \frac{\partial^2 \vec{v}}{\partial y^2} \right]$$

i.e. Considering  $u = \frac{\partial \psi}{\partial y}$  and  $v = -\frac{\partial \psi}{\partial x}$ .

We get

We can define vorticity  $\omega = \vec{\nabla} \times \vec{v}$  (curl of velocity vector)

i.e. Your momentum equation has only one dependent variable  $\psi$ .

It will be a fourth-order differentiated equation.

→ So you require four boundary conditions.

Note: For irrotational flow of inviscid fluids:

$$\vec{\nabla} \times \vec{v} = 0$$

$$\text{i.e.} \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial \psi}{\partial y} & -\frac{\partial \psi}{\partial x} & 0 \end{vmatrix} = \hat{i} \left( -\frac{\partial^2 \psi}{\partial x \partial y} \right) - \hat{j} \left( -\frac{\partial^2 \psi}{\partial y \partial x} \right) + \hat{k} \left( -\frac{\partial^2 \psi}{\partial x^2} - \frac{\partial^2 \psi}{\partial y^2} \right) = 0$$

$$\text{i.e.} \quad \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0$$

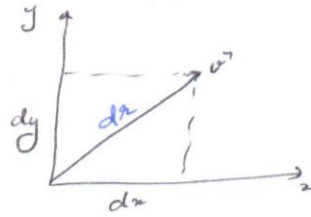
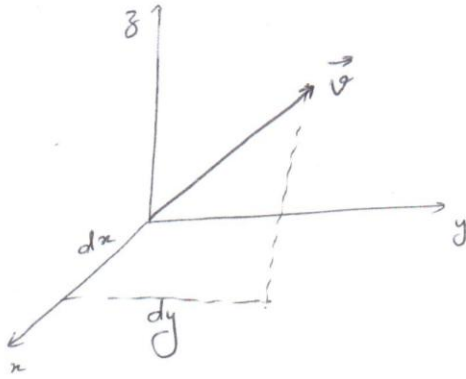
This is Laplace equation.

Q: What is the geometric interpretation of stream function  $\psi$ ?

Recall the definition of streamlines.  
A streamline is a line, which is tangent to velocity.

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vector  $\vec{v}$  everywhere at a given instant



$\Rightarrow$  Any elemental arc length  $dr$  of a streamline should be parallel to  $\vec{v}$ .

Therefore, their components should also match

The components should be such that:

$$\frac{dx}{u} = \frac{dy}{v} = \frac{dr}{|\vec{v}|}$$

$$u = \frac{\partial \psi}{\partial y}, \quad v = -\frac{\partial \psi}{\partial x}$$

$$\frac{dx}{u} = \frac{dy}{v}$$

$$v dx - u dy = 0$$

$$\text{i.e. } -\frac{\partial \psi}{\partial x} dx - \frac{\partial \psi}{\partial y} dy = 0$$

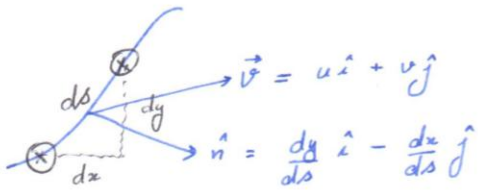
$$\text{or } \frac{\partial \psi}{\partial x} dx + \frac{\partial \psi}{\partial y} dy = 0 = d\psi = \text{a constant}$$

i.e.  $\psi = \text{a constant}$  along a streamline

So in a flow domain, if we solve momentum equation for  $\psi$ , we can then subsequently plot streamlines or lines of constant  $\psi$ 's.

(5)

Again consider a control surface



Now  $d\phi$  between the two points across the control surface will be

$$d\phi = (\vec{V} \cdot \vec{n}) dA$$

Let us take unit width into the paper.

$$\therefore dA = ds \times 1 = ds$$

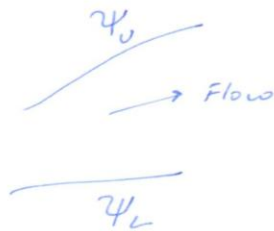
$$\begin{aligned} \text{i.e. } d\phi &= (u \hat{i} + v \hat{j}) \cdot \left( \frac{dy}{ds} \hat{i} - \frac{dx}{ds} \hat{j} \right) ds \times 1 \\ &= \left( \frac{\partial \psi}{\partial y} \hat{i} + \frac{\partial \psi}{\partial x} \hat{j} \right) \cdot \left( \frac{dy}{ds} \hat{i} - \frac{dx}{ds} \hat{j} \right) ds \\ &= \frac{\partial \psi}{\partial x} dx + \frac{\partial \psi}{\partial y} dy = d\psi \end{aligned}$$

That is change in  $\psi$  across the element surface is equal to the volume flow through the element.

Volume flow between any two streamlines ① and ② =  $\psi_2 - \psi_1$

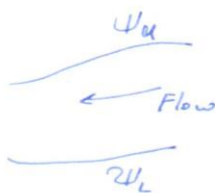
$$\therefore \int_1^2 d\phi = \int_1^2 d\psi = \psi_2 - \psi_1$$

Direction of flow, if  $\psi_u > \psi_L$



If  $\psi_u < \psi_L$

flow



Example

Find the stream function for following irrotational flow  
 $u = a(x^2 - y^2)$  ;  $v = -2axy$  ;  $w = 0$ .