

LINEAR MOMENTUM IN DIFFERENTIAL APPROACH (CONT...)

Yesterday, we started discussing about linear momentum principle through differential approach.

We have seen for an elemental volume $\Delta x \Delta y \Delta z$

$$\sum \vec{F} = \rho \Delta x \Delta y \Delta z \left[\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right]$$

$$\text{or } \sum \vec{F} = \rho \frac{d\vec{v}}{dt} \Delta x \Delta y \Delta z$$

\Rightarrow There will be - body forces and surface forces that contribute to $\sum \vec{F}$

\rightarrow For this situation, let us consider the body force is only due to gravity

$$\therefore d\vec{F}_{\text{grav}} = \rho \vec{g} \Delta x \Delta y \Delta z$$

$$\text{where } \vec{g} = 0 \hat{i} + 0 \hat{j} - g \hat{k}$$

\rightarrow The surface force will be due to pressure and viscous stresses.

\rightarrow The surface forces can be related with respect to the stresses on the sides of the rectangular element considered here.

These stresses are sum of hydrostatic pressure and viscous stress.

(2)

Viscous stress can be represented as $\bar{\tau}$ or in short form τ_{ij} . They are tensorial quantities.

eg. Velocity is a vector

$$\vec{v} = u\hat{i} + v\hat{j} + w\hat{k} \rightarrow v_i$$

i.e. It has three components.

Or in other words, we require three components to define a vector.

Similarly, a ^{second rank} tensorial quantity requires nine components to be described.

$$\bar{\tau} = \begin{pmatrix} \tau_{xx} & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & \tau_{yy} & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & \tau_{zz} \end{pmatrix} \rightarrow \tau_{ij}$$

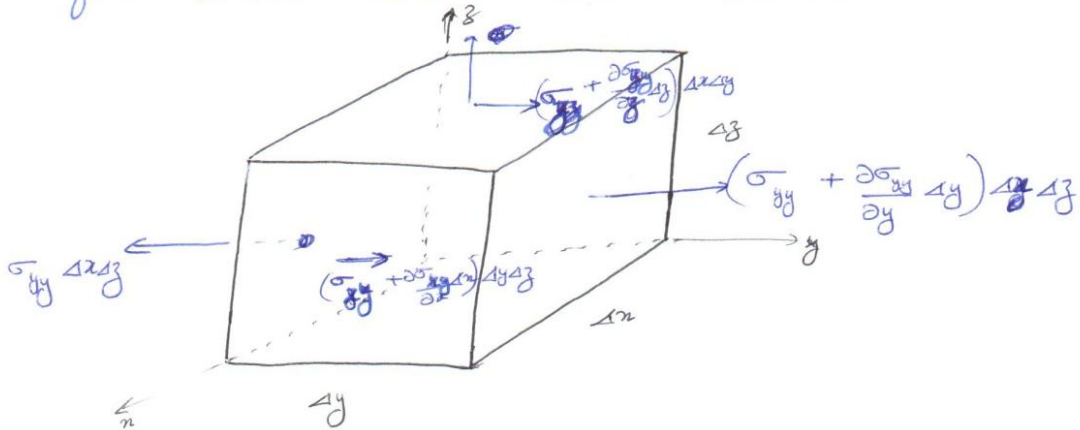
Similarly, strain rates ϵ_{ij} are also second rank tensors.

The stress, therefore, is a second rank tensor

$$\bar{\sigma} \rightarrow \sigma_{ij} = \begin{pmatrix} -p + \tau_{xx} & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & -p + \tau_{yy} & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & -p + \tau_{zz} \end{pmatrix}$$

(3)

As discussed earlier for pressure, here also, it is the gradients or differences that cause a net ~~for~~ surface force on the elemental control volume.



Consider ~~again~~ the surface force, right now, only in y-direction
 you have normal forces $\left\{ \left(\sigma_{yy} + \frac{\partial \sigma_{yy}}{\partial y} \Delta y \right) \Delta x \Delta z - \sigma_{yy} \Delta x \Delta z \right\}$

$$= \frac{\partial \sigma_{yy}}{\partial y} \Delta x \Delta y \Delta z$$

you have ^{also} tangential or shear forces in y-direction

$$\left(\sigma_{xy} + \frac{\partial \sigma_{xy}}{\partial x} \Delta x \right) \Delta y \Delta z - \sigma_{xy} \Delta y \Delta z$$

$$\text{and } \left(\sigma_{zy} + \frac{\partial \sigma_{zy}}{\partial z} \Delta z \right) \Delta x \Delta y - \sigma_{zy} \Delta x \Delta y$$

\therefore The Net ^{surface} force in x-direction

$$dF_{y, \text{surface}} = \left[\frac{\partial (\sigma_{xy})}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zy}}{\partial z} \right] \Delta x \Delta y \Delta z$$

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$$\frac{dF_{y, \text{surface}}}{dV} = -\frac{\partial p}{\partial y} + \frac{\partial(\tau_{xy})}{\partial x} + \frac{\partial(\tau_{yy})}{\partial y} + \frac{\partial(\tau_{zy})}{\partial z}$$

$$16) \frac{dF_{x, \text{surface}}}{\Delta x \Delta y \Delta z} = -\frac{\partial p}{\partial x} + \frac{\partial(\tau_{xx})}{\partial x} + \frac{\partial(\tau_{yx})}{\partial y} + \frac{\partial(\tau_{zx})}{\partial z}$$

$$\frac{dF_{z, \text{surface}}}{\Delta x \Delta y \Delta z} = -\frac{\partial p}{\partial z} + \frac{\partial(\tau_{xz})}{\partial x} + \frac{\partial(\tau_{yz})}{\partial y} + \frac{\partial(\tau_{zz})}{\partial z}$$

$$\hat{i} \frac{dF_{x, \text{surface}}}{\Delta x \Delta y \Delta z} + \hat{j} \frac{dF_{y, \text{surface}}}{\Delta x \Delta y \Delta z} + \hat{k} \frac{dF_{z, \text{surface}}}{\Delta x \Delta y \Delta z} = \vec{dF}_{\text{surface}}$$

$$\frac{\vec{dF}_{\text{surface}}}{\Delta x \Delta y \Delta z} = -\nabla p + \frac{dF_{\text{viscous}}}{\Delta x \Delta y \Delta z}$$

$$\text{Now } \frac{dF_{\text{viscous}}}{\Delta x \Delta y \Delta z} = \hat{i} \left[\frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} \right] + \hat{j} \left[\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} \right] + \hat{k} \left[\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} \right]$$

= $\nabla \cdot \underline{\underline{\tau}}$, please note $\underline{\underline{\tau}}$ is a second rank tensor

$$\underline{\underline{\tau}} = \begin{pmatrix} \tau_{xx} & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & \tau_{yy} & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & \tau_{zz} \end{pmatrix}$$

(5)

\vec{c} → Various stress tensors acting on the elemental fluid volume $\Delta x \Delta y \Delta z$:

∴ We have now from the relation:

$$\vec{\Sigma F} = \rho \frac{d\vec{v}}{dt} \Delta x \Delta y \Delta z$$

$$\text{i.e. } \frac{d\vec{F}}{dt}_{\text{grav}} + \frac{d\vec{F}}{dt}_{\text{surface}} = \rho \frac{d\vec{v}}{dt} \Delta x \Delta y \Delta z$$

$$\text{i.e. } \rho \vec{g} \Delta x \Delta y \Delta z + \left[(-\nabla p) \Delta x \Delta y \Delta z + \nabla \cdot \vec{c} \Delta x \Delta y \Delta z \right] = \rho \frac{d\vec{v}}{dt} \Delta x \Delta y \Delta z$$

As the volume is arbitrary, the equation becomes expression at any mathematical point:

$$\boxed{\rho \vec{g} - \nabla p + \nabla \cdot \vec{c} = \rho \frac{d\vec{v}}{dt}} \rightarrow \textcircled{1}$$

(6)

$$\int g_x - \frac{\partial p}{\partial x} + \frac{\partial z}{\partial x} + \frac{\partial y}{\partial x} + \frac{\partial z}{\partial x} = \int \left(\frac{\partial w}{\partial x} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + \omega \frac{\partial w}{\partial z} \right)$$

$$\int g_y - \frac{\partial p}{\partial y} + \frac{\partial z}{\partial y} + \frac{\partial y}{\partial y} + \frac{\partial z}{\partial y} = \int \left(\frac{\partial w}{\partial y} + v \frac{\partial w}{\partial x} + u \frac{\partial w}{\partial y} + \omega \frac{\partial w}{\partial z} \right)$$

$$\int g_z - \frac{\partial p}{\partial z} + \frac{\partial z}{\partial z} + \frac{\partial y}{\partial z} + \frac{\partial z}{\partial z} = \int \left(\frac{\partial w}{\partial z} + \omega \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + u \frac{\partial w}{\partial z} \right)$$