# Reference-Lines Steered Guide Assignment and Update for Pareto-based Many-Objective Particle Swarm Optimization

Deepak Sharma  $\,\cdot\,$  Devang Agarwal  $\,\cdot\,$  Santosh Kumar

Received: date / Accepted: date

Abstract The reference-lines-framework has been successfully used for developing efficient many-objective evolutionary algorithms. In this paper, the concepts and methodologies of such evolutionary algorithms are adapted in the parlance of multi-objective particle swarm optimization (MOPSO) for addressing the challenges of assigning and updating the global and local guides. The proposed algorithm, which is referred to as RMaOPSO, is developed via five modules using the framework so that a diverse set of guides can be selected to steer the search of MOPSO toward the Paretooptimal front. The modules include global guide assignment, local and global guide update, line assignment to the guides and swarm, and evolutionary search for global guides. The proposed algorithm is tested on DTLZ and WFG test instances of 3-, 5-, 8-, 10- and 15- objectives. Results obtained from RMaOPSO show its efficacy over six multi-objective evolutionary and MOPSO algorithms from the literature.

# 1 Introduction

The real-world optimization problems such as car-cab design [21], topology optimization of continuum structures [46, 50, 51], water resource management [47], bulldozer-blade parametric optimization [6] to name a few, are modeled with multiple objectives. A generic multi-objective optimization problem (MOP) can be written as

min 
$$\mathbf{f}(\mathbf{x}) = (f_1(\mathbf{x}), \dots, f_M(\mathbf{x}))^T,$$
 (1)

subject to  $\mathbf{x} \in \Omega$ , where  $\mathbf{f} \in \mathbb{R}^M$  is the vector of conflicting objectives,  $\mathbf{x} \in \mathbb{R}^N$  is the vector of design variables, and  $\Omega$  is the search space.

Evolutionary and swarm algorithms are mainly preferred for solving equation (1) because these algorithms can generate Pareto-optimal (PO) solutions in one run. Among them, particle swarm optimization (PSO) has been the choice for many researchers because it is simple in concept, easy to implement, and computationally efficient as compared to other meta-heuristic algorithms [26, 48].

PSO has been used for solving MOP, which is generally referred to as MOPSO. In the most commonly used framework of MOPSO, a swarm is initialized by assigning random values to  $\mathbf{x}_i(t)$  for each particle  $i \in \mathbb{R}^N$  at generation t = 0. The initial velocity  $(\mathbf{v}_i(t))$  of each particle *i* is either kept zero or chosen randomly. The archives of global guides  $(G_t)$  and local guides  $(L_t)$  are initialized. At the beginning, the non-dominated solutions from the swarm are copied to the global guide archive and  $\mathbf{x}_i$ 's for all particles are copied to the local guide archive. In a typical loop of generation, the global guide is chosen for each particle in the swarm. The velocity of each particle is then calculated as

$$\mathbf{v}_{i}(t+1) = w\mathbf{v}_{i}(t) + c_{1}r_{1}(G_{ti} - \mathbf{x}_{i}(t)) + c_{2}r_{2}(L_{ti} - \mathbf{x}_{i}(t)),$$
(2)

where w is the inertia weight of the particle,  $c_1$  and  $c_2$ are the coefficients for exploitation and exploration,  $r_1$ and  $r_2$  are the random numbers between [0, 1],  $L_{ti}$  is the personal best of *i*-th particle at *t*-th generation,

Department of Mechanical Engineering, Indian Institute of Technology, Guwahati, Assam-781039, India E-mail: dsharma@iitg.ac.in

and  $G_{ti}$  is the global best of *i*-th particle at *t*-th generation. The position of each particle *i* is then updated as

$$\mathbf{x}_i(t+1) = \mathbf{x}_i(t) + \mathbf{v}_i(t+1). \tag{3}$$

The new position of each particle is evaluated and the archives of the global and local guides are updated. The counter for the generation (t) is then increased by one. PSO finally terminates when (t > T), where T is the maximum number of allowed generations.

It can be observed from the framework that a set of challenges needs to be addressed for developing MOPSO [15, 24, 26, 63, 64]. The first challenge is updating the archive of global guides. While solving MOP, the number of non-dominated solutions can be more than the size of the archive. In this situation, only a diverse set of non-dominated solutions needs to be selected for which an efficient selection operator is needed. Once the archive is updated, the another challenge is to select an appropriate global guide for a particle. It is crucial because the selection of guide can change the flight direction of a particle that can affect the convergence and diversity of MOPSO. Another challenge is diversity loss among the particles of a swarm due to the fast convergence characteristic of PSO.

The above challenges have been addressed by keeping an external archive of non-dominated solutions and the global guides are updated for every particle in a swarm. For example, MOPSOs are developed using an adaptive grid procedure [13, 14],  $\epsilon$ -dominance method [54], distance-based ranking method [38], nondominated sorting and crowding distance [40, 63], parallel coordinate system method [26], global margin ranking method [32], multi-objective gradient method [24], and circular crowding distance measure [12] for pruning the size of the archive and for selecting global guides. Decomposition-based MOPSOs use Tchebycheff function [43], PBI function [5], and crowding distance [34] for the same purpose.

In addition to the above challenges, MOPSOs encounter another big challenge when solving manyobjective optimization problems (MaOPs), when  $M \geq$ 3 in equation (1). It is because many of the above MOP-SOs can fail due to the reduction of selection pressure when almost all particles become non-dominated [44] along with the global guides in the archive. In this situation, the Pareto-ranking cannot differentiate particles/guides and selection procedure depends only on diversity preserving operator.

Efforts have been made in the literature for developing MOPSO for MaOPs. For example, MOPSOs are developed using the gradual Pareto-dominance [31],

the weighted average ranking and distance-based ranking [39], Tchebycheff function and augmented scalarizing function (ASF) [55], ideal point and NWSUM method [7], reference points with k-means clustering [11], Tchebycheff function and crowding distance measure [25], non-dominated sorting and minimum angle approach [15]. The idea of association and niching of structured reference lines of NSGA-III [18] is also explored and the global guides are selected [23]. In another attempt, association and PBI distance are used for storing non-dominated solutions in an external archive [42]. Parallel cell coordinate system [27], scalar projection approach [59], balanceable fitness estimator [35], cooperative hybrid strategy [61] are few recent attempts of developing MOPSOs for MaOPs.

In this paper, the challenges described earlier for developing MOPSO are addressed using the referencelines-based framework of NSGA-III in order to select a diverse set of solutions using the reference lines. The proposed algorithm, which is referred to as RMaOPSO, is developed by adapting the concepts and methodologies of NSGA-III in the parlance of MOPSO for improving its performance. Therefore, RMaOPSO is developed using the five modules with the following contributions.

- The first contribution of RMaOPSO is the development Global\_Guide\_Assignment module in which a global guide is assigned to each particle through an evenly distributed reference lines. These lines are drawn through the origin and the reference points generated on a unit hyperplane using Das and Dennis approach [16]. The first challenge is addressed by assigning the nearest non-dominated solution from the archive of global guides  $(G_t)$  to each reference line. The same solution becomes the global guide for all particles in a swarm that are associated with the same reference line.
- Another contribution is the update of global guides using the Global\_Guide\_Update module, which is developed using the concept of niching of NSGA-III. At this point, other challenges are addressed in which guides are assigned and updated using the structured reference lines that can help in maintaining diversity among the guides and can steer the search toward the PO front along these reference lines.
- Since the reference-lines-based framework is used, the local guide for each particle is updated using the Local\_Guide\_Update module. In this module, the update of local guide is performed by comparing the rank followed by the distance between the particle and local guide with their respective reference lines.
  Since the guides and particles are updated in each
- Since the guides and particles are updated in each generation, they are ranked and associated together

with the reference lines using the Line\_Assignment module.

- Evolutionary\_Search is also coupled with the global guides of RMaOPSO so that these guides do not stuck in the local optima and can further improve the search of the algorithm. It is performed by using the simulated binary crossover and polynomial mutation operators [17].

RMaOPSO is tested using DTLZ and WFG test problems. Since both the sets of test problems are scalable, the objective instances of  $M = \{3, 5, 8, 10, 15\}$  are used and the results are compared using the inverse generalized distance (IGD) and hypervolume (HV) indicators, and using the Wilcoxon test. The outcome of RMaOPSO is compared with six multi-objective evolutionary and MOPSO algorithms from the literature.

The paper is organized into five sections. Section 2 presents the approaches of Pareto-based MOPSO for MaOP. Section 3 presents the proposed RMaOPSO algorithm in which the framework and all modules are described. Section 4 presents the results obtained by RMaOPSO on DTLZ and WFG test problems, and the outcome of RMaOPSO is compared with six exiting algorithms. Section 5 concludes the paper with a future work.

# 2 Overview of Pareto-based Many-Objective PSO

A many-objective optimization problem is referred to as MaOP defined in equation (1), when M > 3 objectives. In the parlance of PSO, various many objective PSO algorithms have been developed. For example, MOPSO using gradual Pareto-dominance [31] for MaOPs is proposed in which ranking is given to each solution by calculating the degree of being dominated. The global guides for particles are selected through the fuzzy Pareto-dominance concept. MOPSOs are also developed using weighted average ranking and distancebased ranking [39] in which the global guides are selected using fitness proportionate selection and tournament selection. In another attempt, a distance-metric using Tchebycheff function and augmented scalarizing function [55] are used with MOPSO. The archive is maintained using these functions, and both global and local guides are updated.

Speed-constrained Multi-objective PSO (SMPSO) has also been extended for MaOP. An ideal point is used for pruning the size of the archive in which the non-dominated solution farthest from the ideal point is removed [7]. The global guide for each particle is selected through NWSum method [41]. Later, a set

of reference points is used for pruning the size of the archive [9]. A multi-grid archiver approach is also coupled with SMPSO [11], which stores a diverse set of non-dominated solutions. The clusters are then made using k-means algorithm in the variable space of non-dominated solutions for generating new solutions.

An objective space decomposition approach is attempted that uses two-step search with MOPSO [25]. First, a swarm is divided into M + 1 groups, where M is the number of objective functions. The best solution from each group is selected as a global guide using Tchebycheff function. In step-2, these global guides are used for diversity. The archive size is controlled using crowding distance measure. In another approach, the objective space is decomposed using weight vectors and the clusters are made for every weight vector. The non-dominated solution, which makes the smallest angle to each weight vector, is selected for the archive [15]. In the recent attempt, MOPSO is modified using the decomposition-based approach for different ideal points for MaOP [45].

A reference-lines-based framework similar to NSGA-III [18] is used for MOPSO in which the archive size is controlled through the niche count of each reference line [23]. The non-dominated solutions closer to the reference lines are selected as the global guides for the swarm. On a similar framework, an external archive is maintained through the association of non-dominated solutions using PBI distance [42]. The non-dominated solution, which makes the maximum cosine angle, becomes the global guide for the particle. A bottleneck learning strategy for convergence and multiple swarm strategy for diversity is coupled with NSGA-III framework for updating the archive [36]. An evolutionary state estimation is used [57] for selecting two types of global guides for convergence and diversity. The reference-lines-based framework is used for updating the archive. The unary epsilon indicator for selecting the local guides, and the reference-vector framework for global guides and the archive are proposed by [37]. Using the referencelines-based framework, a diversity preference approach is developed [53] for MOPSO in which diversity is preserved first by making clusters of solutions and then one solution from each cluster is selected using PBI method. The approach is used for updating the archives of global and local guides.

Some other recent approaches include an immunebased evolutionary strategy [64] for an archive update and pruning of the same is done using crowding distance measure. The global guide for a particle is selected randomly from the archive. Parallel cell coordinate system [27] is also used for MaOP in which two archives of global guides are kept separately for convergence and diversity. A scalar projection approach [59] is used for selecting the global guides from the swarm which is updated through fitness summation and L2 norm. A balanceable fitness estimator [35] consisting of convergence and diversity distances is proposed for updating the archive. The convergence distance is calculated with respect to the ideal point and the diversity distance is found using shift-based density estimation. Intuitionistic fuzzy dominance [60] is used with double search strategy for updating particle's position. The archive is updated using reference points with PBI distance metric. A concept of dominant different [33] is used for comparing solutions, selection of global and local guides, and for updating the archive.

Meanwhile, some comparative studies are also performed for ranking the solutions, guides assignment, and archive update. The study [30] presents comparison among the guide selection methods, such as random, crowding distance, WSum, NWSum, Sigmamethod, and opposite method, which are coupled with SMPSO. It is found that NWSum and Sigma method evolve better results. Another study [8] presents comparison of various archiving methods, such as adaptive grid, crowding distance, dominating archive, adaptive  $\epsilon$ -approx archiving, adaptive  $\epsilon$ -Pareto archiving, multi-level grid archiving, random archiver, and unbounded archive. The unbounded archiver and  $\epsilon$ -Pareto archiving are found to be the best. The study [56] presents comparison of the methods that can differentiate non-dominated solutions for MaOP. Methods like favour relation, k-optimality, CDAS, crowding distance and average ranking, and sum ratios are considered. It is found that CDAS-based archiving method [10] is the most efficient among others.

In the literature, there is a considerable effort toward developing MOPSO for solving MaOP. Still, the performance of MOPSOs is not comparable with other multi-objective evolutionary algorithms for solving MaOPs. In this paper, an efficient MOPSO is developed using the reference-lines-framework through modules for better convergence and diversity. The proposed algorithm is described in the following section.

# 3 RMaOPSO: Proposed Many-objective MOPSO

The reference-lines-based framework is used to develop MOPSO, which is presented in Algo. 1. It is referred to as RMaOPSO that begins by initializing random swarm  $(P_t)$  of size N. At the same time, the archives to store local guides  $(L_t)$  and global guides  $(G_t)$  are

kept empty. In order to assign  $L_t$  and  $G_t$  in subsequent generations, RMaOPSO adopts various features of reference lines-based-framework similar to NSGA-III [18] in which swarm  $P_t$  is evaluated, ranked, normalized and associated with a set of structured reference lines in Step 2 using Line\_Assignment module of Algo. 1, which is discussed later. Initially,  $L_t$  and  $G_t$ archives are filled with the same swarm of  $P_t$ . An extreme vector ( $\mathbf{e} \in \mathbb{R}^M$ ) [49, 52] is also initialized with the Nadir point, which is evaluated from the set of the non-dominated solutions from  $P_t$ . The vector  $\mathbf{e}$  will be used later for normalization.

RMaOPSO enters into the standard loop of generation in Step 5. Since PSO is used for multi-objective optimization, there are always multiple global guides to steer the search of particles in the swarm. Generally, the non-dominated solutions are considered as global guides for which various algorithms have been adopted in the literature as discussed in Section 2. RMaOPSO proposes Global\_Guide\_Assignment module for assigning the global guides to particles in the swarm using the reference-lines-based framework. Once the guides are assigned, particle's velocity and position are updated in Steps 7 and 8. Thereafter, the Line\_Assignment module is used on the combined population of the current swarm at t-th generation and the archives of global and local guides  $(M_t = P_t \cup G_t \cup L_t)$  to rank, normalize and associate them together with the set of structured reference lines. In Step 10, the Local\_Guide\_Update module is developed to update the local guides using the rank and association obtained in Step 9. Thereafter, the Global\_Guide\_Update module is developed to update the global guides in Step 11 from the combined population  $(M_t)$ . The niching concept of NSGA-III is adopted to develop this module. At the last, the Evolutionary\_Search module is applied to the archive of the global guides in Step 12 in which crossover and mutation operators are used to update  $G_t$ . The modules under the generation-loop are repeated until t reaches to the maximum allowed generations (T). The archive of the global guides is then reported as the set of nondominated solutions for the given optimization problem. In the following subsections, the reference-linesbased framework and the modules of Algo. 1 are discussed in detail.

## 3.1 Reference-Lines-based Framework

In this framework, a set of structured reference points is generated on a unit hyperplane using [16] approach in the objective space. In this approach, each objective axis is divided into p equal divisions that create Algorithm 1 Reference-Lines-based Framework for MOPSO (RMaOPSO)

**Input:** t = 1, M : objectives, N : swarm size, H : reference points

- **Output:** A set of non-dominated solutions  $(G_t)$
- 1: Initialize random swarm  $(P_t)$ , and initialize the archive of global guides  $(G_t = \emptyset)$  and local guides  $(L_t = \emptyset)$ ;
- 2: Line\_Assignment $(P_t)$ ;
- 3: Assign global guides  $(G_t = P_t)$  and local guides  $(L_t = P_t)$ ;
- 4: Compute extreme point:  $\mathbf{e} = (e_1, e_2, \dots, e_M)^T$  such that  $e_j = \max_{\mathbf{x} \in P_t} f_j(\mathbf{x})$  and  $\mathbf{x}$  is a non-dominated solution
- 5: while  $\tilde{t} \leq T$  do
- 6: Global\_Guide\_Assignment( $G_t$ );
- 7:  $W_t = \text{Velocity\_Update}(P_t);$
- 8:  $P_t = \text{Position_Update}(W_t);$
- 9: Line\_Assignment $(M_t = P_t \cup G_t \cup L_t);$
- 10:  $L_t = \text{Local_Guide_Update}(P_t, L_t);$
- 11:  $G_t = \text{Global_Guide_Update}(M_t);$
- 12: Evolutionary\_Search $(G_t)$ ;
- 13: t = t + 1
- 14: end while

|H| number of reference points on a unit hyperplane as given in (4).

$$|H| = \binom{M+p-1}{p}.$$
(4)

The set of structured reference points for M = 3 objective case is shown in Fig. 1. The figure on the top shows 21 reference points when p = 5 is taken. The two-layered approach [18] is shown at the bottom of the figure in which p = 2 for the outer layer and p = 1for the inner layer are used. Although the two-layered approach is shown for 3-objective case, but it is mainly used for the instances of more than five objectives. It is because the number of reference points becomes very high for higher number of objectives as given by equation (4). The reference lines are then drawn, which pass from these reference points and the origin. These reference lines are used to associate each particle in the swarm. For example, a particle  $(\mathbf{s})$  is associated to that reference line  $(\mathbf{w})$  which is closest to it. The Euclidean distance, referred to as  $dist(\mathbf{s}, \mathbf{w})$ , between  $(\mathbf{s})$  and  $(\mathbf{w})$ is calculated using (5).

$$dist(\mathbf{s}, \mathbf{w}) = ||(\mathbf{s} - \mathbf{w}^T \mathbf{s} \mathbf{w} / ||\mathbf{w}||^2)||.$$
(5)

In the reference-lines-based framework, the convergence of a swarm is maintained through the nondominated sorting [19] in which particles are sorted in different fronts based on their ranks. The diversity is maintained by associating particles with the reference lines. In the ideal condition when the global guides are assigned to each reference line and particles are associated with their closest reference lines, particles are



Fig. 1 A set of structured reference lines are drawn using Das and Dennis approach [16].

expected to converge along those reference lines onto the PO front. Thus, the framework can evolve a well converge and diverse set of non-dominated solutions, which is maintained through the distribution of those structured reference lines.

# 3.2 Line\_Assignment Module: Steps 2 and 9 of Algo. 1

Line\_assignment module is developed to quantify the solution based on its rank and association. Algo. 2 for this module presents three major steps in which solutions of  $R_t$  are ranked, normalized and associated with their nearest reference lines. For ranking, solutions of  $R_t$  are sorted in different fronts based on their ranks using the non-dominated sorting [19]. Thereafter in Step 2,  $R_t$  is normalized using Algo. 3 in which the ideal point ( $\mathbf{z}^{\mathbf{I}}$ ) of  $R_t$  is calculated in Step 1 using (6).

$$\mathbf{z}^{\mathbf{I}} = (z_1^I, z_2^I, \dots, z_M^I)^T : z_j^I = \min_{\mathbf{s} \in R_t} f_j(\mathbf{s})$$
(6)

Algorithm 2 Line_Assignment( $R$	(2t)
1: $(F_1, F_2,) =$ Non-dominated sort	ting $(R_t)$ ;
2: $\bar{R}_t =$ Normalize $(R_t)$ ;	%Using Algo. 3
3: Associate $(\bar{R}_t)$ ;	%Using Algo. 4

In this case, the minimum of each objective is stored to translate  $R_t$  in Step 2 using (7).

$$\mathbf{f}'(\mathbf{s}) = (f_1'(\mathbf{s}), f_2'(\mathbf{s}), \dots, f_M'(\mathbf{s}))^T : f_j'(\mathbf{s}) = f_j(\mathbf{s}) - z_j^I, \ \forall \mathbf{s} \in (7)$$

The ideal point of  $R_t$  is now translated to the origin. For normalizing  $R_t$ , the extreme vectors (Z) in each objective are calculated in Step 3 of Algo. 3 by minimizing the achievement scalarizing function given in (8).

$$Z = (\mathbf{z}_{1}^{\mathbf{e}}, \mathbf{z}_{2}^{\mathbf{e}}, \dots, \mathbf{z}_{\mathbf{M}}^{\mathbf{e}}) : \mathbf{z}_{j}^{e} = \mathbf{f}'(\mathbf{s}), \mathbf{s} : \min_{\mathbf{s} \in R_{t}} \left( \max_{i=1}^{M} f_{i}'(\mathbf{s})/w_{i} \right).$$
(8)

Here,  $w_i$  is set to 1.0 when i = j for  $\mathbf{z}_j^e$  and  $10^{-6}$  for rest of the objectives. These vectors in Z construct the M-dimensional hyperplane. This plane intersects each objective axis at  $a_j$  that is used for normalizing  $R_t$  as given in (9).

$$\bar{f}_j(\mathbf{s}) = \frac{f'_j(\mathbf{s})}{a_j}, \ \forall j \in \{1, \dots, M\}.$$
(9)

However, it has been found that the extreme vectors in Z can have duplicates that results in a degenerate case. In Step 6, the Nadir point  $(\mathbf{Z}^{\mathbf{N}})$  is computed from the set of non-dominated solutions of  $R_t$ if there is any duplicate in Z. Otherwise, the intercept  $\mathbf{a} = (a_1, a_2, \dots, a_M)^T$  on each objective axis is found in Step 8. At this stage, any intercept can become negative after solving a system of linear equations. In order to deal with this degenerate case, the Nadir point  $(\mathbf{Z}^{\mathbf{N}})$  is again computed in Step 10. If negative intercept is not found, the extreme vector  $\mathbf{e}$  is updated in Step 13. Otherwise, the component of the extreme vector is compared with its corresponding Nadir point component and is updated accordingly in Step 18 [49]. The normalization of  $R_t$  is performed with the updated **e** vector in Step 21.

The last step in Algo. 2 is association, which is presented in Algo. 4. First, the reference lines  $(\mathbf{w})$  are created using the structured reference points generated on the hyperplane, which pass through these points and the origin in Step 2 of Algo. 4. Thereafter, an Euclidean distance  $(dist(\mathbf{s}, \mathbf{w}))$  is calculated for each solution  $(\mathbf{s} \in R_t)$  to all reference lines  $(\mathbf{w})$  using (5). The solution is then associated with the nearest reference line in Step 8 and its distance is stored in  $d(\mathbf{s})$ . This association will help RMaOPSO in assignment and updating the global guides.

A	lgorit	hm 3	Norma	lize( <i>I</i>	$(t_t)$	[49]
---	--------	------	-------	----------------	---------	------

- 1: Compute ideal point using (6);
- 2: Translate objectives using (7);
- 3: Compute extreme points using (8);
- $R_{t}$ : Compute number of duplicate points (D) in Z;
- 5: if D > 0 then
- 6: Compute Nadir point,  $\mathbf{z}^{\mathbf{N}} = (z_1^N, z_2^N, \dots, z_M^N)^T$  from the set of the non-dominated solutions of  $R_t$ ;

```
7: else
```

- 8: Compute intercept  $\mathbf{a} = (a_1, a_2, \dots, a_M)^T$  from (Z)and assign flag= 0;
- 9: **if**  $a_i < 0$  **then**
- 10: Compute Nadir point,  $\mathbf{z}^{\mathbf{N}} = (z_1^N, z_2^N, \dots, z_M^N)^T$ from the set of the non-dominated solutions of  $R_t$ ;

```
11: flag = 1;
12: else
```

```
13: update \mathbf{e} = \mathbf{a};
```

14: end if

- 15: end if
- 16: if D > 0 or flag= 1 then
- 17: **if**  $z_j^N < e_j$ , where  $j \in \{1, \ldots, M\}$  **then**
- 18:  $e_j = z_j^N$
- 19: end if
- 20: end if
- 21:  $\overline{f}_j(\mathbf{s}) = f'_j(\mathbf{s})/e_j, \forall \mathbf{s} \in R_t, \forall j \in \{1, \dots, M\}$

Algorithm	<b>4</b>	Associate	$(R_t)$	) [	18	
-----------	----------	-----------	---------	-----	----	--

1:	for all $\mathbf{r} \in H$ do	
2:	Compute reference line $\mathbf{w}$ and $W = W \cup \mathbf{w}$ ; %No	te
	that $ W  = H$ .	
3:	end for	
4:	for all $\mathbf{s} \in \bar{R}_t$ do	
5:	for all $\mathbf{w} \in W$ do	
6:	Compute $dist(\mathbf{s}, \mathbf{w})$ using (5);	
7:	end for	
8:	$\pi(\mathbf{s}) = \mathbf{w} : \operatorname{argmin} dist(\mathbf{s}, \mathbf{w});$ %Associates <b>s</b> to line	ne
	$\pi(\mathbf{s})$	
9:	$d(\mathbf{s}) = dist(\mathbf{s}, \pi(\mathbf{s}));$ %Stores minimum distance of $\mathbf{s}$	to
	$d(\mathbf{s})$	
10:	end for	

# 3.3 Global\_Guide\_Assignment Module: Step 6 of Algo. 1

Using Algo. 2, all particles in the swarm and global guides in  $G_t$  are associated with their respective nearest reference lines. In this module, first the global guide is found for each reference line (**w**) and the same global guide is then assigned to all particles, which are associated with the same reference line **w**. This module is developed using Algo. 5 in which a set of non-dominated global guides associated with the reference line **w** is stored in  $T_{\mathbf{w}}$  in Step 2. If  $T_{\mathbf{w}} \neq \emptyset$ , the nearest solution **s** from  $T_{\mathbf{w}}$  is assigned as the global guide for the line **w** in Step 4. In case  $T_{\mathbf{w}} = \emptyset$ , the non-dominated solution **s** from  $G_t$ , which is closest to the line **w**, is selected as the global guide for the line **w** in Step 6. It is noted that Step 6 shows a different approach than NSGA-III in which the line is deleted if any solution is not asso-

ciated with it. However, since particles of the current swarm  $(P_t)$  can be associated with the line for which  $T_{\mathbf{w}} = \emptyset$ , Step 6 helps RMaOPSO to find the nearest non-dominate global guide.

Algorithm 5 Global_Guide_Assignment	$(G_t$	)
-------------------------------------	--------	---

1: for all  $\mathbf{w} \in W$  do  $T_{\mathbf{w}} = \mathbf{s} : \pi(\mathbf{s}) = \mathbf{w}, \ \mathbf{s} \in G_t \text{ and } \mathbf{s} \text{ is non-dominated}$ 2:

- solution; 3:
- if  $T_{\mathbf{w}} \neq \emptyset$  then 4:
- $GB_{\mathbf{w}} = GB_{\mathbf{w}} \cup \{\mathbf{s} : \operatorname{argmin}_{\mathbf{s} \in T_{\mathbf{w}}} d(\mathbf{s})\};$  $\% GB_{w}$ refers to the global best solution for line w
- 5: else
- $GB_{\mathbf{w}} = GB_{\mathbf{w}} \cup \{\mathbf{s} : \operatorname{argmin} d(\mathbf{s}), \ \mathbf{s} \in G_t \text{ and } \mathbf{s} \text{ is }$ 6:non-dominated solution}; 7:
- end if 8: end for

3.4 Velocity and Position Update

The velocity and the position of a particle are updated using equations (2) and (3). The most commonly used approach for setting  $w, c_1$ , and  $c_2$  parameters is to sample them randomly in their respective ranges. Since this approach did not work well with RMaOPSO, an adaptive approach is used in which the parameters are changed as given in equation (10).

$$w = 0.9 \times (1 - t/T),$$
  

$$c_1 = 2.5 \times (1 - t/T),$$
  

$$c_2 = 2.5 \times (1 - t/T),$$
  
(10)

where t is the current generation, and T is the maximum allowed generations.

#### 3.5 Local\_Guide\_Update Module: Step 10 of Algo. 1

Once particles updated their positions in Step 8 and associated with reference lines in Step 9 of Algo. 1, the archive of the local guides is updated. Algo. 6 presents the local guide update rules, which depend on the rank and distance of a particle to the associated line. If the rank of a particle is better than its local guide, the local guide is updated in Step 3. If rank is the same, the local guide is updated based on the smaller Euclidean distance of a particle from the associated reference line in Step 6.

#### 3.6 Global\_Guide\_Update Module: Step 11 of Algo. 1

The global\_guide\_update module is developed by adopting the niching mechanism of NSGA-III so that

# **Algorithm 6** Local\_Guide\_Update $(P_t, L_t)$

- 1: for all  $i \in N$  do
- if (rank of  $P_t^i < \text{rank of } L_t^i$ ) then 2
- Update  $L_t^i = P_t^i; \mathscr{P}_t^i$  and  $L_t^i$  are *i*-th swarm of  $P_t$ 3: and  $L_t$
- 4: else if (rank is same) then
- if  $(d(P_t^i) < d(L_t^i))$  then 5:
- 6: Update  $L_t^i = P_t^i;$ %Based on distance found in Step 8 of Algo. 4
- 7: end if
- 8: end if
- 9: end for

#### **Algorithm 7** Global\_Guide\_Update $(R_t)$

- Classify solutions in different fronts based on the ranks obtained earlier by Line\_Assignment module;
- 2: Initialize  $S_t = \emptyset$  and i = 1;
- 3: while  $|S_t| \leq N$  do
- 4:  $S_t = S_t \cup F_i$  and i = i + 1;
- 5: end while
- 6: if  $(|S_t| = N)$  then
- $G_t = S_t$ , Stop; 7: 8: else
- $G_t = \bigcup_{i=1}^{l-1} F_i$ ; %Inclusion of fronts till last but one. 9: Compute niche count of each reference line  $(\mathbf{w})$  such 10:that  $\rho_{\mathbf{w}} = \sum_{\mathbf{s} \in S_t/F_l} ((\pi(\mathbf{s}) = j) ? 1 : 0);$
- while  $(|G_t| \le H)$  do 11:
- 12:Find a line which has the least niche count. In case of multiple lines having minimum niche count, choose one of them  $(\mathbf{w})$  at random;
- 13: $I_{\mathbf{w}} = \{\mathbf{s} : \pi(\mathbf{s}) = \mathbf{w}, \mathbf{s} \in F_l\}; \ \% F_l \text{ is the last front}$ to be used for filling  $G_t$
- if  $(I_{\mathbf{w}} \neq \emptyset)$  then 14:
- if  $(\rho_w = 0)$  then 15:16:
  - $G_t = G_t \cup (\mathbf{s} : \operatorname{argmin}_{\mathbf{s} \in I_{\mathbf{w}}} d(\mathbf{s}));$ %Copy the solution closest to the line  $\mathbf{w}$
  - else  $G_t = G_t \cup \operatorname{random}(I_{\mathbf{w}});$
  - end if
  - $\rho_{\mathbf{w}} = \rho_{\mathbf{w}} + 1, \ F_l = F_l \setminus \mathbf{s};$
- $21 \cdot$ else

17:

18:

19:

20:

- 22:Remove line  $\mathbf{w}$ end if
- 23: 24:end while
- 25: end if

a set of good solutions can be stored in the archive of global guides. Algo. 7 presents the global guide update for Step 11 of Algo. 1 in which the combined population  $(M_t)$  is sent and for Step 4 of Algo. 8 in which  $(G_t \cup G_t)$ is sent. Since ranking and association have already been done by Line\_Assignment module, solutions of  $R_t$  are classified into different fronts based on their ranks in Step 1 of Algo. 7. Solutions of  $R_t$  are then copied frontwise into  $S_t$  till its size is more than N in Step 4. If the size of  $S_t$  is the same as N, all solutions of  $S_t$  are copied into  $G_t$  in Step 7 and the module is terminated. Otherwise, solutions in the fronts are copied to  $G_t$ , excluding the last front  $(F_l)$  solutions in Step 9. Thereafter, the niche count of each reference line is computed in Step 10. This count signifies the number of solutions associated with a line. If the niche count of a line is relatively lower than other lines, it signifies that the region around this line is less crowded. It means that a solution can be chosen to update the archive of global guides. The same procedure is followed in Step 12 to find the line which has the minimum niche count. If the line has no associated solution from  $S_t/F_l$ , its niche becomes zero. For this line, a solution from  $F_l$ , which is nearest to it, is copied to  $G_t$  in Step 16. In case, the niche count of the line is non-zero, any random solution from  $F_l$ , which is associated with it, is copied to  $G_t$  in Step 18. When a solution from  $F_l$  is copied to  $G_t$ , the niche count is updated and the selected solution is removed from  $F_l$  so that a distinct solution can be copied. If a line has no associated solution from  $S_t/F_l$  and also from  $F_l$ , this line is then removed for further consideration in Step 22. This update for the archive of the global guides ensures selection of a diverse set of the best-ranked solutions into  $G_t$ , which is useful for velocity update of particles and also to report the non-dominated solutions.

#### 3.7 Evolutionary\_Search Module: Step 12 of Algo. 1

An evolutionary search is performed on the archive of the global guides  $(G_t)$  in every generation so that the global guides do not stuck to any local optima and can improve further to steer the search of the swarm toward the PO front. Algo. 8 presents the four major steps in which crossover is performed using SBX operator and mutation is performed using polynomial mutation operator [17]. The new set of global guides  $(\hat{G}_t)$  along with the current global guides  $(G_t)$  are then ranked, normalized and associated together with the lines using Line\_Assignment $(G_t \cup \hat{G}_t)$  module in Step 3 of Algo. 8. Thereafter, the global guides are selected through Global\_Guide\_Update $(G_t \cup \hat{G}_t)$  module in Step 4.

<b>Algorithm 8</b> Evolutionary Search $(G_t)$									
1: $\bar{G}_t =$	$\operatorname{crossover}(G_t); \%$	by using SBX crossover operator							
2: $\hat{G}_t =$	$\operatorname{mutate}(\bar{G}_t);$	% by using Polynomial mutation							

operator 3: Line\_Assignment  $(G_t \cup \hat{G}_t)$  using Algo. 2;

4: Global\_Guide\_Update( $G_t \cup \hat{G}_t$ ) using Algo. 7;

## 3.8 Computational Complexity

The computational complexity of RMaOPSO is similar to NSGA-III since it involves all the key operations, such as non-dominated ranking, normalization, association, and niching. However, the non-dominated ranking and association are performed thrice in one generation. Therefore, the worst-case computational complexity of one generation of RMaOPSO is either the nondominated ranking  $(O(3 \times N^2 \log^{M-2} N))$  or association  $(O(3 \times N^2 M))$ , whichever is larger.

# 4 Results and Discussion

In this section, RMaOPSO is tested on DTLZ [20] and WFG [28] problem instances having M = $\{3, 5, 8, 10, 15\}$  objectives. The number of variables for DTLZ problems is n = M + k - 1, where k = 5 is kept fixed for DTLZ1, and k = 10 is kept the same for DTLZ2-4 problems. Similarly, n = k + l is used for WFG1-9 problems in which  $k = 2 \times (M - 1)$  is the position-related variable and l = 20 is kept fixed for the distance-related variable. These test problems are chosen because they have different characteristics, such as DTLZ1 is linear and multi-modal; DTLZ2 is concave; DTLZ3 is concave and multi-modal; DTLZ4 is concave and biased; WFG1 is mixed and biased; WFG2 is convex, disconnected, multi-modal and non-separable; WFG3 is linear, degenerate and non-separable; WFG4 is concave and multi-modal; WFG5 is concave and deceptive; WFG6 is concave and non-separable; WFG7 is concave and biased; WFG8 is concave, biased and non-separable; WFG9 is concave, biased, multi-modal, deceptive and non-separable. These characteristics pose challenges for algorithms to converge to the PO front.

Two statistical indicators, such as inverse generalized distance (IGD) and hypervolume (HV) are used to assess the performance of RMaOPSO with respect to the existing multi-objective evolutionary algorithms and MOPSOs. IGD indicator measures convergence and diversity of a set of the obtained non-dominated solutions (P) with respect to the PO solutions (Q<sup>\*</sup>). It is calculated using (11) in which  $d(q_i^*, p_j) = ||q_j^* - p_i||^2$  is the Euclidean distance in the objective space,  $|Q^*|$  and |P| are the cardinality of Q<sup>\*</sup> and P, respectively.

$$IGD(\mathbf{P}, \mathbf{Q}^*) = \frac{\sum_{i=1}^{|Q^*|} \min_{j=1}^{|P|} d(q_i^*, p_j)}{|Q^*|}.$$
 (11)

HV indicator measures the size of the objective space dominated by the solutions in P and bounded by  $\mathbf{z}^r$ . It is given in (12), where VOL(.) represents the Lebesgue measure, and  $\mathbf{z}^r = (z_1^r, \ldots, z_M^r)^T$  is the reference point, which is dominated by all PO solutions. Larger is the HV value, better is the quality of P for approximating the PO front. For DTLZ1,  $\mathbf{z}^r = (1, \ldots, 1)^T$  is chosen. For other DTLZ and WFG problems,  $\mathbf{z}^r = (2, \dots, 2)^T$  is considered. The HV values presented in this paper are normalized between [0,1] by dividing  $z = \prod_{i=1}^{M} z_i^r$ . Both the indicators are determined by normalizing P, except for DTLZ1.

$$HV(Q) = VOL\left(\bigcup_{s \in P} [f_1((s), z_i^r] \times \dots [f_M((s), z_M^r]]\right),$$
(12)

RMaOPSO is compared with six algorithms from the literature, that are, NSGA-III [18]<sup>1</sup>, SPEA/R [29]<sup>2</sup>, VaEA [58], dMOPSO <sup>3</sup> [62], SMPSO [40], and MaPSO [59]. NSGA-III is chosen because RMaOPSO is developed using its reference-lines-based framework. However, RMaOPSO has adopted the concepts of NSGA-III for developing procedure for the global and local guides' assignment and update. SPEA/R is chosen because it uses k-layered reference direction search method in which it emphasis first on diversity followed by convergence. VaEA is chosen because it also uses the referencelines-based framework; however, the environmental selection is performed using the maximum-vector-angle approach and worst-elimination principle. SMPSO and dMOPSO are chosen because these algorithms are established MOPSOs which have been tested successfully on many multi-objective optimization problems. MaPSO is the recently published MOPSO and its working principle was discussed in Section 2.

All the algorithms are run 20 times with different initial populations or swarms and their results are compared. The Wilcoxon signed-rank test at 5% significance level is performed to compare the outcome of RMaOPSO with the existing algorithms. The population size for all algorithms is chosen based on the number of reference points calculated using (4). The details are given in Table 1. These algorithms are terminated based on the number of generations, which are presented in Table 2.

For a fair comparison, the algorithm parameters are kept same. The SBX and polynomial mutation operators are used as evolutionary search. The probability of crossover is kept 1.0, and the probability of mutation is  $p_m = 1/n$ . The distribution index for SBX operator is  $\eta_c = 30$ , and the distribution index for polynomial mutation operator is  $\eta_m = 20$ . For all MOPSOs, the

 Table 1
 Number of reference points and corresponding population sizes for the algorithms.

No. of	divisions	No. of ref.	Population
obj. $(M)$	$p \text{ or } (p_1, p_2)$	points $( H )$	(N)
3	12	91	92
5	6	210	210
8	(3, 2)	156	156
10	(3, 2)	275	276
15	(2,1)	135	136

Table 2 Maximum number of generations for algorithms.

No. of	DTLZ1	DTLZ2	DTLZ3	DTLZ4	WFG (all)
objectives					
3	400	250	1000	600	1000
5	600	350	1000	1000	1250
8	750	500	1000	1250	1500
10	1000	750	1500	2000	2000
15	1500	1000	2000	3000	3000

parameters  $(w, c_1, c_2)$  are sampled randomly from their respective ranges, such as  $w \in [0.1, 0.5]$ , and  $c_1, c_2 \in$ [1.5, 2.5]. For SPEA/R, the archive size is set same as the population size, and the number of k-layers for 3-, 5-, 8-, 10-, and 15-objectives for all problems is k = 7, 8, 5, 6, and 3, respectively. The population size is determined as  $N = 4 \times ceil(((M \times k \times (k+3)/2)+1)/4))$ . For MaPSO, the parameters K = 3 and  $\theta_{max} = 0.5$  are kept fixed.

# 4.1 Performance on DTLZ Problems

The performance of RMaOPSO is tested on scalable DTLZ1-4 problems in this section, and its outcome is tested using the IGD and HV indicators. Table 3 presents the best, median, and worst values of IGD indicator for each objective of DTLZ problems. The gray cells represent the best IGD value for each row among the algorithms. Here, smaller IGD value is better. It can be seen that RMaOPSO shows better IGD values in 44 out of 60 rows, which is the highest in number. The outcome from the Wilcoxon test is also shown for each instance in the same table. The symbol '+' indicates that RMaOPSO is significantly better than the corresponding algorithm. Similarly, the symbols '-' and '=' indicate significantly worse and equivalent performance of RMaOPSO with respect to the corresponding algorithm, respectively. At the bottom of the table, the collective outcome (+/=/-) from the Wilcoxon test is shown. It can be seen that RMaOPSO outperforms all the algorithms on all instances of DTLZ1-4 problems.

Table 4 presents the best, median and worst HV indicator values for DTLZ problems. The gray cells again represent the best HV values for each row. Here, larger

 $<sup>^1\,</sup>$  NSGA-III code developed by [49] is used, which is available in the public domain.

 $<sup>^2\,</sup>$  The codes of SPEA/R, VaEA and MaPSO are provided by the authors.

 $<sup>^3\,</sup>$  The source codes of dMOPSO and SMPSO are obtained from the jmetal framework [22].

HV value is better. RMaOPSO shows the best HV values in 33 out of 48 rows, which is the highest in number. It can be seen again at the bottom of the table that RMaOPSO again outperforms all the algorithms based on the outcome of Wilcoxon test.

The obtained non-dominated solutions for 3- and 10-objective DTLZ3 problem are shown here because DTLZ3 is concave and multi-modal multi-objective optimization problem. The plots are generated corresponding to the run of median IGD value. Fig. 2 shows the obtained non-dominated solutions for 3-objective problem from all the algorithms. It can be seen that RMaOPSO, NSGA-III, SPEA/R, and MaPSO are able to converge to the PO front of DTLZ3. However, the evenness in the distribution of solutions can be seen with RMaOPSO and NSGA-III. SMPSO and dMOPSO generates the solutions quite close to the PO front but the distribution of solutions is not as even as RMaOPSO. VaEA is only the algorithm which fails to converge to the PO front.

Fig. 3 shows the value path of the obtained nondominated solutions for 10-objective DTLZ3 problem. It can be seen that RMaOPSO and NSGA-III generate a converged and well-distributed set of solutions, where the rest of the algorithms fail to converge to the PF. Except for the tenth objective, VaEA is also converged to the PO front.

#### 4.2 Performance on WFG Problems

Now, RMaOPSO is tested on the WFG test problems and its outcome is compared with other algorithms based on the IGD and HV values, and on Wilcoxon test outcome. Table 5 presents the best, median, and worst IGD values obtained from the algorithms for WFG1-9 problem instances. The gray cells represent the best IGD values among the algorithm for each row. Here, smaller IGD value is better. For WFG problems, a scattered distribution of gray cells can be seen in which RMaOPSO shows better IGD values in 39 rows out of 135, which is the highest in number. The table also shows the outcome of Wilcoxon test for individual instances and the cumulative outcome is presented at the bottom of the table. It can be seen that RMaOPSO outperforms all MOPSOs and shows better performance over SPEA/R and VaEA. RMaOPSO shows an equivalent performance with NSGA-III.

Table 6 presents the statistical HV indicator values for WFG1-9 problem instances. The gray cells again represent the better HV value. Here, larger HV value is better. Again, a scatter gray cells can be seen in which RMaOPSO shows better HV values in 31 out of 108 rows, which is the highest in number. The outcome of Wilcoxon test is shown for each problem instance and the cumulative performance can be seen at the bottom of the table. It can be observed that RMaOPSO outperforms dMOPSO and SMPSO. It shows better performance than SPEA/R and VaEA and an equivalent performance with MaPSO. Based on HV values, NSGA-III shows slightly better outcome of Wilcoxon test over RMaOPSO. The main reason is the frequent jumping of the particles out of the bounds which are then brought back to the bounds.

The non-dominated solutions obtained from all algorithms are shown in Fig. 4 for 3-objective WFG6 problem in the normalized objective space. The plots are generated corresponding to the run of median IGD value. It can be seen that RMaOPSO and NSGA-III are converged to the PO front and the obtained solutions are evenly spread over the PO front. The rest of the algorithms are little far from the PO front. Fig. 5 shows value path plots of algorithms for 10-objective WFG6 problem. Except for dMOPSO, all algorithms have generated the extreme solutions in each objective. However, RMaOPSO and NSGA-III show a better distribution of the obtained non-dominated solutions over the PO front.

#### 4.3 Average Performance

Since a large set of problem instances is solved in which none of the algorithms come out to be the clear winner, an average performance score of the algorithms for different objectives and problems is calculated [26, 53, 57, 60]. The score is calculated by comparing the median IGD values obtained in Table 3 and Table 4 and then, a rank is assigned to every algorithm for each instance. The smaller average performance score represents better performance. Fig. 6 shows the average performance score of all algorithms for different objectives. It can be clearly seen that RMaOPSO shows the best performance in all objective instances cumulatively. Fig. 7 shows the average performance score over different DTLZ and WFG problems. RMaOPSO shows the best performance for DTLZ2-4 problems, and WFG4-6 and WFG8 problems. RMaOPSO is the second best in DTLZ1, WFG3, WFG7, and WGF9 problems. Based on the above average performance scores, the ranking of the algorithms is calculated and shown in Fig. 8. It can be seen that RMaOPSO emerges as the best algorithm among the others. It is slightly better than NSGA-III but outperforms the others.



Fig. 2 Obtained non-dominated solutions by the algorithms for 3-objective DTLZ3 problem.



Fig. 3 The value path of the obtained non-dominated solutions by the algorithms for 10-objective DTLZ3 problem.



Fig. 4 Obtained non-dominated solutions by the algorithms for 3-objective WFG6 problem in the normalized objective space.



Fig. 5 The value path of the obtained non-dominated solutions by the algorithms for 10-objective WFG6 problem.

		11001 111	675 F 1 (5		NARDAR	a) (D a c	16 220	<b>D</b> 14 0 D 6 0
	M	NSGA-III	SPEA/R	VaEA	dMOPSO	SMPSO	MaPSO	RMaOPSO
		3.510E-04	4.447E-03	1.280E-02	2.398E-02	2.900E-02	2.135E-02	1.238E-04
	3	1 5265 02 +	2 128E 02 +	4 8005 02 +	2 826E 02 +	$2.107E_{-0.2} +$	2 221E 02+	2 127E 04
	0	1.55012-05	2.1301-02	4.0331-02	2.8201-02	0.197E-02	2.3311-02	2.12712-04
		5.787E-03	9.910E-02	4.039E-01	4.943E-02	3.485E-02	2.494E-02	3.073E-04
		4.962E-04	1.517E-02	1.898E-02	7.658E + 00	9.169E-02	6.422E-02	3.706E-04
	5	7.431E-04 <sup>+</sup>	4.038E-02 <sup>+</sup>	3.401E-02 <sup>+</sup>	$3.939E+01^+$	1.094E-01 <sup>+</sup>	$7.465 \text{E}{-}02^{+}$	4.209E-04
		1.246E-03	1.323E-01	6.372E-02	$6.338E \pm 01$	1.343E-01	1.069E-01	1.870E-03
Zl		2 175E 03	6 328E 02	1 033E 02	$2.565E \pm 01$	1 344E 01	1 178E 01	1 408E-03
E	0	2.1751-05	0.5261-02	1.5551-02	2.0000-01	1.04412-01	1.176E-01	1.4001-05
E	8	3.582E-03	1.490E-01	2.722E-02	4.972E+01	3.216E-01	1.370E-01	7.047E-02
Ц		6.645E-02	6.193E-01	4.981E-02	6.342E + 01	7.597E + 00	1.925E-01	7.767E-02
		2.279E-03	4.146E-02	2.214E-02	2.258E + 01	1.564E-01	1.249E-01	1.400E-03
	10	$2.583E-03^{=}$	1.018E-01 +	$2.939E_{-}02 =$	$4.367E \pm 01^{+}$	5 223E-01 <sup>+</sup>	$1.564E_{-}01^{+}$	9 153E-03
		0.207E 02	2.807E 01	2.000H 02	7.082E   01	$1.204E \pm 01$	1.060E 01	7 405E 02
		9.297E-02	2.897E-01	3.972E-02	$7.065E \pm 01$	$1.304E \pm 01$	1.909E-01	1.405E-02
		1.922E-03	2.409E-01	4.884E-02	2.202E+01	3.301E-01	1.730E-01	1.825E-03
	15	$2.853\mathrm{E}\text{-}03^-$	4.356E-01 -	5.362E-02 -	$4.257E+01^{+}$	5.630E-01 $^{-}$	$1.959E-01^{+}$	5.433E-02
		4.324E-03	2.969E + 00	5.938E-02	6.759E + 01	1.778E + 01	2.163E-01	2.249E-01
		1.045E-03	3.125E-03	8.292E-03	5.914E-02	7.385E-02	4.903E-02	5.017E-04
	3	$1.970 \pm 0.2 \pm$	5 074E 02 +	1 485E 02 +	6 152E 02 +	7 758 0 0 +	5 542E 02 <sup>+</sup>	6048E04
	0	1.270E-03	1.100E.00	1.465E-02	0.155E-02	1.138E-02	5.545E-02	0.9481-04
		2.870E-03	1.128E-02	2.572E-02	6.600E-02	8.210E-02	5.736E-02	8.574E-04
		3.058E-03	9.941E-03	1.334E-02	5.562E-01	2.922E-01	1.589E-01	2.198E-03
	5	4.481E-03 <sup>+</sup>	1.308E-02 <sup>+</sup>	1.606E-02 <sup>+</sup>	6.324E-01 <sup>+</sup>	3.624E-01 <sup>+</sup>	$1.675E-01^{+}$	2.493E-03
		1.128E-02	2.120E-02	2.064E-02	6.777E-01	4.056E-01	1.891E-01	2.964E-03
Z2		1 152E-02	2 307E-02	2.830E-02	8 489E-01	6.857E-01	3 167E-01	6 210E-03
Ę	0	1.0020 02	2.0010 02	2.000E 02	0.1000 01 +	0.001 ± 01	0.101E 01	0.4500 00
ΤC	0	1.293E-02	2.849E-02	3.524E-02	9.295E-01	8.782E-01	3.352E-01	8.456E-03
Ц		1.691E-02	3.342E-02	4.904E-02	9.814E-01	1.074E + 00	3.547E-01	1.213E-02
		1.142E-02	2.455E-02	2.270E-02	9.557E-01	8.171E-01	3.652E-01	7.532E-03
	10	1.279E-02 <sup>+</sup>	2.893E-02 <sup>+</sup>	3.838E-02 +	$1.011E \pm 00^{+}$	$1.157E \pm 00^{+}$	3.833E-01 <sup>+</sup>	8.563E-03
		$1.486E_{-}02$	3.689E_02	$4.143E_{-}02$	$1.073E \pm 0.0$	$1.342E \pm 0.0$	3.945E-01	$1.256E_{-}02$
		1.4601-02	4.607E.02	2.602E 02	1.075E   00	1.042E + 00	4.947E-01	6 508E 02
	15	1.052E-02	4.007E-02	3.092E-02	1.1085+00	1.474L+00	4.247E-01	0.5961-05
		1.428E-02	5.477E-02	6.588E-02	1.268E+00	1.635E+00	4.592E-01	8.586E-03
		1.758E-02	7.102E-02	1.485E-01	1.309E + 00	2.134E + 00	4.797E-01	8.236E-02
		8.723E-04	6.758E-03	1.955E-01	5.232E-02	7.106E-02	4.860E-02	3.125E-04
	3	3.991E-03 <sup>+</sup>	$3.334E-02^+$	$1.052E \pm 00^{+}$	5 428E-02 <sup>+</sup>	7.516E-02 <sup>+</sup>	$5.646E-02^+$	4.300E-04
	-	9.847E-03	$2.413E_{-01}$	$4.125E \pm 00$	6.004E-02	8 325E-02	$2.002E \pm 00$	4.667E-03
		9.047E-03	2.415E-01	4.120E+00	0.004E=02	0.525E-02	2.002E+00	4.00712-03
	_	2.174E-03	7.925E-02	2.226E-02	$3.504E \pm 02$	2.716E-01	1./18E-01	0.027E-04
	ъ	3.675E-03 -	2.060E-01 +	1.936E-01 +	$4.927E+02^{+}$	3.844E-01 -	$2.153E-01^{+}$	8.090E-04
~		1.014E-02	3.801E-01	5.687E-01	5.875E + 02	4.890E-01	3.813E-01	5.444E-03
N		1.256E-02	3.811E-01	8.289E-02	3.818E + 02	3.710E + 00	3.762E-01	8.602E-03
늰	8	$2.444 E_{-}02^{-}$	$2.296E \pm 00^{+}$	8 487E-01 +	$5.636E \pm 0.02^{+}$	$6.459E \pm 01^{+}$	$4.392E_{-}01^{+}$	5.039E_02
5	0	5 987E 09	4.402E + 00	$1.145E \pm 0.0$	6 779E   02	1.201E + 0.001	5.171E 01	2.075E 01
-		9.207E-02	4.495E+00	1.145E+00	$0.772E \pm 02$	$1.321E \pm 02$	J.171E-01	3.975E-01
	10	8.230E-03	3.882E-01	5.758E-02	3.513E+02	4.408E+01	4.699E-01	4.480E-03
	10	1.069E-02 -	6.790E-01 +	3.287E-01 +	$4.572E+02^{+}$	$7.938E+01^{+}$	$5.020E-01^{+}$	7.291E-03
		1.929E-02	4.395E + 00	1.169E + 00	6.132E + 02	1.009E + 02	5.985E-01	4.270E-01
		1.121E-02	5.443E + 00	6.600E-02	3.434E + 02	1.533E + 02	5.234E-01	3.936E-03
	15	1.766E-02 <sup>+</sup>	$1.207E \pm 01^{+}$	$1.280E \pm 00^{+}$	$5.223E \pm 02^{+}$	$2.075E \pm 02^{+}$	6.156E-01 <sup>+</sup>	6.160E-03
	-	3 671E-02	$3.338E \pm 01$	$1.301E \pm 00$	$6.283E \pm 02$	$2.247E\pm02$	7 536E-01	2 272E-01
		9.110E-04	3.338E+01	1.3010-00	0.2850702	2.2470702	7.550E-01	2.27215-01
		3.113E-04	4.001E-04	7.698E-03	8.080E-02	6.947E-02	5.124E-02	3.153E-04
	3	3.918E-04 =	1.837E-03 <sup>+</sup>	2.267E-01 <sup>+</sup>	1.108E-01 <sup>+</sup>	7.344E-02 <sup>+</sup>	$5.555E-02^+$	3.721E-04
		5.314E-01	4.983E-03	9.503E-01	1.794E-01	7.985E-02	5.766E-02	9.503E-01
		3.641E-04	2.182E-03	1.641E-02	7.434E-01	1.974E-01	1.463E-01	3.357E-04
	5	4 334E 04 +	$4.001 \pm 0.3 \pm$	$1.030 \pm 0.1 \pm$	$0.713 \pm 0.1 \pm$	2 325E 01 +	$1.533 \pm 0.1^{+}$	3 075F-04
	0	4.004D-04	4.001E-03	2.047E.01	3.713E-01	2.3231-01	1.5551-01	4.99110.04
4		0.072E-04	9.001E-03	3.947E-01	1.1301-00	2.013E-01	1.070E-01	4.001E-04
2		2.541E-03	(.315E-03	3.326E-02	9.863E-01	4.200E-01	2.532E-01	2.469E-03
Ē	8	3.442E-03 <sup>+</sup>	9.148E-03 <sup>+</sup>	2.380E-01 <sup>+</sup>	$1.137E+00^{+}$	5.405E-01 <sup>+</sup>	$2.728E-01^+$	3.073E-03
Ω	1	5.319E-03	1.220E-02	6.228E-01	1.334E + 00	6.252E-01	2.862E-01	4.012E-03
		3.578E-03	6.907E-03	4.088E-02	8.838E-01	5.627E-01	2.813E-01	2.998E-03
	10	4 228E 03 +	8 063E 03 +	$1.843 \pm 01^{+}$	$1.017E \pm 00^{+}$	6 641E 01 +	$2000 \pm 01^+$	3.650E-02
	10	F 174E 00	1 101E 00	1.0401-01	1.145 - 00	5.041E-01	2.3301-01	4.400E-03
		5.174E-03	1.191E-02	3.770E-01	1.145E+00	(.548E-01	3.047E-01	4.490E-03
		5.257E-03	9.225E-03	1.226E-01	1.068E + 00	1.118E + 00	2.512E-01	4.961E-03
	15	$7.298 \text{E-} 03^{=}$	1.115E-02 <sup>+</sup>	2.898E-01 <sup>+</sup>	$1.184E+00^{+}$	$1.268E+00^+$	$2.773E-01^{+}$	7.697E-03
	1	9.578E-03	1.475E-02	9.067E-01	1.303E + 00	1.486E + 00	3.023E-01	1.048E-02
(+	/=/-)	13/4/3	20/0/0	17/2/1	20/0/0	20/0/0	20/0/0	-
	, <u> </u>			+1/4/1				

**Table 3** Best, median and worst IGD values obtained by RMaOPSO and other algorithms on DTLZ instances with differentnumber of objectives. Best performances are highlighted in bold face with gray background.

# **5** Conclusions

RMaOPSO has been developed in this paper for updating the archive of global guides and assigning them to particles using the reference-lines-based framework. The main objective was to select an appropriate global guide for each particle so that many-objective optimization problems can be solved efficiently. Therefore, a set of structured reference lines was used to assign and update guides in every generation for each particle in a swarm. In order to achieve the objective, five modules were developed for improving convergence and diversity of RMaOPSO. These modules included Global\_Guide\_Assignment, Global\_Guide\_Update, Local\_Guide\_Update, Line\_Assignment, and Evolutionary\_Search. The proposed RMaOPSO

	M	NSGA-III	SPEA/R	VaEA	dMOPSO	SMPSO	MaPSO	RMaOPSO
		9.73656E-01	9.73376E-01	9.70545E-01	9.70931E-01	9.68321E-01	9.72251E-01	9.73676E-01
	3	9.73423E-01 <sup>+</sup>	9.70047E-01 <sup>+</sup>	9.57151E-01 <sup>+</sup>	$9.60109 \text{E-}01^+$	$9.66712 \text{E-}01^+$	9.71936E-01 <sup>+</sup>	9.73663E-01
		9.72470E-01	9.44695E-01	4.78116E-01	9.40745E-01	9.65165E-01	9.71078E-01	9.73624E-01
		9.98982E-01	9.97918E-01	9.98560E-01	9.70931E-01	9.94571E-01	9.98277E-01	9.98986E-01
5	5	9.98977E-01 <sup>+</sup>	9.97159E-01 <sup>+</sup>	$9.98216 \text{E-}01^+$	$9.60109 \text{E-}01^+$	9.90411E-01 <sup>+</sup>	$9.97662 \text{E-}01^+$	9.98984E-01
Ľ		9.98963E-01	9.91088E-01	9.97263E-01	9.40745E-01	9.77792E-01	9.94801E-01	9.98981E-01
ΤC		9.99974E-01	9.99786E-01	9.99824E-01	9.70931E-01	9.94571E-01	9.99884E-01	9.99979E-01
_	8	$9.99971 \mathrm{E}{-}01^-$	9.96402E-01 <sup>+</sup>	$9.99570 \text{E-}01^+$	$9.60109 \text{E-}01^+$	$9.90411 \text{E-}01^+$	$9.99807 \text{E-}01^+$	9.99914E-01
		9.99896E-01	4.83954E-01	9.98418E-01	9.40745E-01	9.77792E-01	9.99051E-01	9.99906E-01
		9.99998E-01	9.99974E-01	9.99932E-01	9.70931E-01	9.94571E-01	9.99994E-01	9.99999E-01
	10	9.99997E-01 <sup>=</sup>	9.99923E-01 <sup>+</sup>	$9.99864 \text{E-}01^+$	$9.60109 \text{E-}01^+$	$9.90411 \text{E-}01^+$	$9.99972 \text{E-}01^+$	9.99999E-01
		9.99988E-01	9.74683E-01	9.99656E-01	9.40745E-01	9.77792E-01	9.99870E-01	9.99994E-01
		9.26692E-01	9.26671E-01	9.25552E-01	9.23564E-01	9.19128E-01	9.26472E-01	9.26729E-01
	3	9.26640E-01 <sup>+</sup>	9.26565E-01 <sup>+</sup>	$9.24474 \text{E-}01^+$	$9.22346E-01^+$	$9.17490 \text{E-}01^+$	$9.26058E-01^+$	9.26704 E-01
		9.26584E-01	9.26319E-01	9.22430E-01	9.21754E-01	9.14333E-01	9.25503E-01	9.26684 E-01
		9.90505E-01	9.86881E-01	9.90383E-01	7.69201E-01	9.58619E-01	9.89463E-01	9.90529E-01
$Z_2$	5	9.90474E-01 <sup>+</sup>	9.86822E-01 <sup>+</sup>	$9.90274 \text{E-}01^+$	$7.49667 \text{E-}01^+$	$9.32828E-01^+$	$9.89135 \text{E-}01^+$	9.90511E-01
E		9.90418E-01	9.86721E-01	9.90117E-01	7.09305E-01	9.06122E-01	9.87376E-01	9.90491E-01
5		9.99337E-01	9.98713E-01	9.99325E-01	7.48924E-01	8.46623E-01	9.99055E-01	9.99347E-01
	8	9.99328E-01 <sup>+</sup>	9.98658E-01 <sup>+</sup>	$9.99312 \text{E-}01^+$	$7.08707 \text{E-}01^+$	$7.11107 \text{E-}01^+$	$9.98856E-01^+$	9.99340E-01
		9.99315E-01	9.98475E-01	9.99286E-01	6.75727E-01	4.29473E-01	9.98726E-01	9.99325E-01
		9.99919E-01	9.99764E-01	9.99919E-01	7.71284E-01	8.21622E-01	9.99825E-01	9.99920E-01
	10	9.99917E-01 <sup>+</sup>	9.99744E-01 <sup>+</sup>	$9.99876E-01^{+}$	$7.49630E-01^+$	$6.08050 \text{E}{-}01^+$	$9.99801E-01^+$	9.99919E-01
		9.99916E-01	9.99721E-01	9.99872E-01	7.17320E-01	4.17720E-01	9.99783E-01	9.99917E-01
		9.26593E-01	9.26316E-01	3.29451E-03	9.26429E-01	9.20859E-01	9.26684E-01	9.26775E-01
	3	9.25882E-01 <sup>+</sup>	9.24816E-01 <sup>+</sup>	$6.83835E-03^+$	$9.25997 \text{E-}01^+$	$9.19780 \text{E-}01^+$	$9.26131E-01^+$	9.26695E-01
		9.24558E-01	8.99569E-01	1.11064E-01	9.17906E-01	9.17765E-01	4.40325E-03	9.25775E-01
	-	9.90525E-01	9.86510E-01	9.90161E-01	9.26429E-01	9.59236E-01	9.88524E-01	9.90584E-01
$Z_3$	Э	9.90469E-01	9.82919E-01	9.80306E-01	9.25997E-01	9.21241E-01	9.86276E-01	9.90563E-01
님		9.90135E-01	9.72970E-01	8.19713E-01	9.17906E-01	7.24203E-01	9.78306E-01	9.90330E-01
Ď	0	9.99334E-01	9.86510E-01	9.99072E-01	9.26429E-01	9.59236E-01	9.98633E-01	9.99349E-01
	8	9.99264E-01	9.82919E-01 -	6.58526E-01	9.25997E-01	9.21241E-01	9.98135E-01 '	9.99278E-01
		9.99100E-01	9.72970E-01	5.03707E-01	9.17906E-01	7.24203E-01	9.97371E-01	9.95700E-01
	10	9.99922E-01	9.80510E-01	9.99856E-01	9.26429E-01	9.59236E-01	9.99661E-01	9.99922E-01
	10	9.99918E-01	9.82919E-01 0.72070E-01	9.96896E-01	9.25997E-01	9.21241E-01 7.24202E-01	9.99590E-01	9.99920E-01
		9.99909E-01	9.72970E-01	0.06508E.01	9.17900E-01	7.24203E-01	9.99505E-01	9.99259E-01
	2	9.26777E-01 =	9.20883E-01	9.20598E-01	9.21032E-01	$9.21013 \pm -01$	9.20525E-01	9.20782E-01
	3	9.20733E-01	9.20823E-01	9.14404E-01	9.18204E-01	9.20304E-01	9.20103E-01	9.20731E-01
		0.00503F 01	9.20724E-01 0.87003E-01	0.00000E-01	9.15141E-01 7.25320F_01	9.18995E-01	9.25549E-01	4.999995E-01
<del></del>	5	9.90593E-01	9.87093E-01	9.90028E-01	7.200E 01 <sup>+</sup>	9.84940E-01	9.90341E-01	9.90392E-01
Ň	0	9.90578E-01	9.87007E-01	9.00903E-01	3.23790E-01 2.76585E-01	9.85090E-01	9.90211E-01	9.90580E-01
Ē		9.90371E-01	9.87043E-01	9.71855E-01	6.60632F.01	9.80800E-01 0.85841E-01	9.90000E-01	9.90370E-01
О	8	$0.00364F_{-01}=$	0.08828F 01 +	$0.08877 \pm 01^{+}$	5.80330F 01 <sup>+</sup>	$0.73631E - 01^+$	$0.00330E 01^+$	0.00364F 01
	0	9.99304E-01 0.00363E-01	9.98828E-01 0.08811E-01	9.98877E-01 9.87270E-01	4 15375E 01	9.73031E-01	9.99339E-01	9.99304E-01 0.00363F_01
		9 99924E-01	9.99793E-01	9.99925E_01	8.36730E-01	9.87990E-01	9 99924E-01	9.99903E-01
	10	0.000241-01	$9.99792E_{-01} +$	$9.99918E_{-01}^{+}$	7 06959E-01+	9.64856E-01 <sup>+</sup>	9.00024E-01	0.00023E_01
	10	9.99923E-01	9.99790E-01	9.99454E-01	5.60297E-01	9.52353E-01	9.99913E-01	9.99923E-01
(+	/=/-)	8/7/1	$\frac{13/2}{1}$	16/0/0	16/0/0	16/0/0	16/0/0	0.0001011 01

**Table 4** Best, median and worst HV values obtained by RMaOPSO and other algorithms on DTLZ instances with different number of objectives. Best performances are highlighted in bold face with gray background.

was tested on many-objective instances of DTLZ and WFG problems and the outcome was compared with six existing multi-objective evolutionary and MOPSO algorithms. Based on the obtained results using the IGD and HV indicators, and Wilcoxon test, it can be concluded that RMaOPSO emerges as the best among the chosen set of algorithms. Especially, RMaOPSO outperformed all three MOPSO algorithms.

An observation can be made that RMaOPSO is still unable to perform well in many instances for WFG problems. The primary reason is the frequent jumping of the particles out of the bound which are again brought back to the bound. Therefore, RMaOPSO still needs an efficient velocity update for better performance. Moreover, the concepts like diversity over dominance approaches [52], line prioritized environmental selection [49], etc. can be brought into the parlance of MOPSO to further improve the convergence and diversity among the particles and guides. Furthermore, RMaOPSO can be hybridized with other heuristic algorithms [1, 2, 3, 4] for better performance.

# **Conflict of interest**

The authors declare that they have no conflict of interest.

# References

1. Abualigah L, Yousri D (2021) Advances in sine cosine algorithm: A comprehensive survey. Artifi-

	M	NSGA-III	SPEA/R	VaEA	dMOPSO	SMPSO	MaPSO	RMaOPSO
		3.555E-01	4.010E-01	1.544E-01	5.180E-01	5.357E-01	1.815E-01	3.678E-01
	3	$3.692E-01^{-1}$	4.230E-01 <sup>+</sup>	$1.830E-01^{-1}$	5.235E-01 <sup>+</sup>	$5.390E-01^+$	2 441E-01 <sup>-</sup>	3.868E-01
	-	3 803E 01	4 317E 01	2.345E-01	5 206E 01	5 420E 01	3 000E 01	3.076F 01
		2.004E.01	4.317E-01	2.545E-01	$1.112E \pm 00$	5.420E-01	3.000E-01	4.120E-01
	~	5.994E-01	4.504E-01	3.120E-01	1.115E+00	5.720E-01	2.557E-01	4.129E-01
	5	4.042E-01	4.582E-01	3.803E-01	$1.184E + 00^{+}$	5.782E-01	3.263E-01	4.207 E-01
_		4.108E-01	4.662E-01	4.301E-01	1.210E + 00	5.876E-01	3.981E-01	4.291E-01
Ċ,		3.646E-01	3.464E-01	3.214E-01	1.134E + 00	6.061E-01	2.464E-01	3.452E-01
Ē	8	4.198E-01 <sup>-</sup>	4.010E-01 <sup>-</sup>	3.332E-01 <sup>-</sup>	$1.168E + 00^+$	$6.101E-01^+$	$3.254 \mathrm{E}{ ext{-}01}^{- ext{-}}$	4.755E-01
$\leq$		4.492E-01	6.962E-01	3.507E-01	$1.207E \pm 00$	6.183E-01	4.288E-01	6.149E-01
		3.151E-01	2.934E-01	2.806E-01	1.084E+00	6.024E-01	1.998E-01	2.237E-01
	10	2 GANE 01 -	$2.100 \pm 01 =$	2.000E 01 -	$1.122E + 00^{\pm}$	6 005E 01+	$2.257E_{01}^{-1}$	4 661E 01
	10	3.046E-01	5.192E-01	2.924E-01	$1.152E \pm 00^{\circ}$	0.095E-01	2.207E-01	4.001E-01
		4.425E-01	5.884E-01	3.066E-01	1.165E+00	6.121E-01	3.988E-01	5.610E-01
		4.319E-01	3.326E-01	4.091E-01	1.091E+00	6.081E-01	3.260E-01	3.347E-01
	15	4.435E-01 <sup>+</sup>	6.362E-01 <sup>+</sup>	4.141E-01 <sup>+</sup>	$1.110E + 00^+$	$6.104E-01^+$	$3.443\mathrm{E} extsf{-}01^-$	3.689E-01
		4.899E-01	6.421E-01	4.187E-01	1.142E + 00	6.170E-01	3.629E-01	4.390E-01
		1.769E-02	1.745E-02	4.304E-02	7.598E-02	6.709E-02	4.398E-02	1.815E-02
	3	2.082E-02 =	$2.050E-02^{=}$	$4.989E-02^{+}$	$8.019E_{-}02^{+}$	$7.376E-02^+$	4 785E-02 <sup>+</sup>	2 187E-02
	~	0.766F 02	0.022E.02	1.000E 02	8 788E 02	8.275E 02	5.373E 02	2.1011 02
		9.700E-02	9.922E-02	7 106E 02	2.427E 01	0.275E-02	7 156E 02	2.082E-02
	~	5.840E-02	4.740E-02	7.100E-02	3.437E-01	1.362E-01	7.130E-02	5.813E-02
	Э	$5.990 \text{E}{-}02$ -	4.972E-02	7.732E-02	3.800E-01	1.560E-01	7.499E-02	6.089E-02
$\sim$		1.629E-01	5.139E-02	1.736E-01	4.485E-01	1.673E-01	7.919E-02	6.406E-02
3		8.938E-02	6.683E-02	1.110E-01	4.258E-01	1.676E-01	1.155E-01	1.511E-01
F	8	1.452E-01 <sup>-</sup>	$7.197\mathrm{E}\text{-}02^-$	1.203E-01 <sup>-</sup>	4.595E-01 <sup>+</sup>	$1.988E-01^{=}$	1.216E-01 <sup>-</sup>	1.876E-01
$\leq$		2.313E-01	2.049E-01	2.143E-01	5.131E-01	2.449E-01	1.312E-01	2.694E-01
		1.221E-01	6.505E-02	1.896E-01	4.590E-01	1.484E-01	1.875E-01	1.944E-01
	10	2.017E 01 =	7 482 02	2.042E 01 -	4 052E 01 +	1.052E 01	2.066F 01 -	2.115E 01
	10	2.017E-01 2.100E-01	0.403E-04	2.042E-01	4.955E-01	1.952E-01	2.000E-01	2.115E-01
		3.199E-01	2.403E-01	2.211E-01	5.230E-01	2.262E-01	2.227E-01	3.205E-01
		3.069E-01	3.381E-01	4.713E-01	8.832E-01	1.830E-01	1.187E-02	6.990E-01
	15	6.278E-01 <sup>-</sup>	$1.094E+00^{+}$	5.550E-01 <sup>-</sup>	9.337E-01 <sup>+</sup>	$2.091E-01^{-1}$	$2.191\mathrm{E} extsf{-}02^-$	8.137E-01
		7.115E-01	1.128E + 00	7.147E-01	9.740E-01	2.424E-01	4.289E-02	1.035E+00
		1.788E-02	3.485E-02	3.387E-02	2.770E-02	4.503E-02	2.465E-02	2.300E-02
	3	$2.271E_{-}02^{-}$	4 155E-02 <sup>+</sup>	$4.451E_{-}02^{+}$	3 802E-02 +	$8.472E_{-}02^{+}$	$2.923E_{-02} =$	3.077E-02
	Ŭ	3.068E-02	6.476E 02	5.633E 02	5.003E 02	$1.037E_{01}$	2.525E 02 3 721E 02	4.050E.02
		4 575 02	0.410E-02	6.074E.02	0.000E-02	1.057E-01	4.220E.02	4.0001-02
	F	4.575E-02	9.751E-02	0.074E-02	2.224E-01	1.274E-01	4.559E-02	3.234E-02
	э	5.855E-02 -	1.149E-01 '	8.556E-02	2.515E-01	1.616E-01	$5.463 \pm 02^{-1}$	6.123E-02
m		8.149E-02	1.386E-01	1.585E-01	2.738E-01	1.980E-01	6.321E-02	1.175E-01
Ü		5.078E-02	2.677E-01	7.622E-02	2.208E-01	1.164E-01	1.035E-01	7.925E-02
F	8	$6.922 \mathrm{E}\text{-}02^-$	4.197E-01 <sup>+</sup>	1.108E-01 =	2.761E-01 <sup>+</sup>	$2.069E-01^+$	1.645E-01 <sup>+</sup>	9.846E-02
5		1.342E-01	6.170E-01	1.882E-01	2.984E-01	2.527E-01	2.385E-01	2.635E-01
		5.661E-02	1.056E-01	7.716E-02	2.241E-01	6.873E-02	1.206E-01	5.262E-02
	10	7 /3/E-02-	$2.262 E_{-}01^{+}$	$1.723E_{-}01^{+}$	$2.634E_{-01}^{+}$	$1.893E_{-}01^{+}$	$1.762E_{-}01^{+}$	9 190E-02
		1 176E 01	5.060E 01	2 722E 01	2.001E 01	2.287E 01	2 182E 01	1 202E 01
		2 691E 02	2.005E-01	2.755E-01	2.934E=01	2.387E-01	2.100E-01	1.202E-01
	15	2.031E-02	3.813E-01	3.208E-02	2.445E-01	1.540E-01	1.365E-01	5.066E-02
	15	9.104E-02	4.350E-01	2.071E-01	2.881E-01	2.066E-01 <sup>-</sup>	2.069E-01	1.356E-01
		2.671E-01	5.666E-01	2.794E-01	3.233E-01	2.500E-01	2.956E-01	4.494E-01
		4.735E-03	7.735E-03	5.244E-02	7.515E-02	9.717E-02	5.588E-02	4.478E-03
1	3	$6.065 \mathrm{E}\text{-}03^{=}$	9.383E-03 <sup>+</sup>	$5.576E-02$ $^+$	7.708E-02 <sup>+</sup>	$1.008E-01^+$	6.121E-02 <sup>+</sup>	6.328E-03
1		7.093E-03	1.134E-02	6.114E-02	8.219E-02	1.082E-01	6.711E-02	8.813E-03
		1.629E-02	1.994E-02	1.601E-01	4.639E-01	1.948E-01	1.702E-01	1.741E-02
	5	$2.110E_{-}02 =$	$2.158 E_{-}02^{+}$	$1.681E_{-}01^{+}$	$5.097E_{-}01^{+}$	$2.117E_{-0.1}^{+}$	$1.765E_{-}01^{+}$	1 983E-02
	Ŭ	2.1150-02	2.100E-02	1.001E-01 1.774E 01	5 491E 01	2.117E-01 2.262E 01	1.700E-01	2.256E 02
4		2.966E-02	2.302E-02	1.774E-01	5.421E-01	2.203E-01	1.640E-01	2.330E-02
Q	0	3.175E-02	3.100E-02	2.400E-01	7.204E-01	3.287E-01	2.983E-01	2.837E-02
VF	8	3.562E-02 -	$3.783E-02$ $^+$	$2.759E-01$ $^+$	7.757E-01 +	$3.721E-01^{+}$	3.163E-01 <sup>+</sup>	3.166E-02
$\geq$		4.319E-02	8.833E-02	2.961E-01	8.225E-01	4.031E-01	3.293E-01	4.467E-02
		3.537E-02	3.083E-02	3.191E-01	8.163E-01	3.310E-01	3.301E-01	2.829E-02
	10	4.334E-02 <sup>+</sup>	3.722E-02 <sup>+</sup>	3.355E-01 <sup>+</sup>	8.559E-01 <sup>+</sup>	$3.758E-01^+$	3.533E-01 <sup>+</sup>	3.115E-02
1		4.730E-02	4.268E-02	3.522E-01	8.849E-01	4.024E-01	3.655E-01	3.879E-02
		4.962E-01	3.081E-02	4.893E-01	$1.024E \pm 00$	5.075E-01	3.686E-01	3.937E-01
	15	6 020E 01 +	2 180E 01	5 1515 01 -	1.0525100+	5 272E 01=	4.0255.01 -	5 717E 01
1	10	6 601E 01	6.001E.01	5.101E-01 5.979E-01	1.076E + 00	5.572E-01	4.000E-01	5.111E-01 6.840E-01
L		0.091E-01	0.991E-01	J.2/0E-UI	1.07012+00	0.002E-01	4.3301-01	0.040E-01
		2.996E-02	3.330E-02	5.927E-02	7.405E-02	8.800E-02	6.614E-02	3.096E-02
ŝ	3	3.475E-02 =	$3.457 \text{E-}02^{=}$	6.271E-02 <sup>+</sup>	7.721E-02 <sup>+</sup>	$9.903 \text{E-}02^+$	7.025E-02 <sup>+</sup>	3.536E-02
Ö		4.383E-02	3.851E-02	6.667E-02	8.603E-02	1.191E-01	7.468E-02	4.077E-02
ΥF		3.666E-02	4.140E-02	1.592E-01	4.353E-01	2.756E-01	1.879E-01	3.453E-02
· ·	5	4.005E-02 +	4.335E-02 +	1.638E-01 <sup>+</sup>	4.615E-01 <sup>+</sup>	$2.996E-01^{+}$	1.946E-01 <sup>+</sup>	3.968E-02
	-	4 432E-02	4 474E-02	1 707E-01	4 991E-01	3.220E-01	2.081E-01	4.181E-02

 ${\bf Table \ 5} \ {\rm Best, \ median \ and \ worst \ IGD \ values \ obtained \ by \ RMaOPSO \ and \ other \ algorithms \ on \ WFG \ instances \ with \ different \ number \ of \ objectives. \ Best \ performances \ are \ highlighted \ in \ bold \ face \ with \ gray \ background. }$ 

	M	NSGA-III	SPEA/R	VaEA	dMOPSO	SMPSO	MaPSO	RMaOPSO
		4.727E-02	4.904E-02	2.549E-01	6.436E-01	4.073E-01	3.410E-01	4.595E-02
	8	5.208E-02 <sup>=</sup>	5.219E-02 =	$2.823E-01^+$	$6.827 \text{E}\text{-}01^+$	4.293E-01 <sup>+</sup>	$3.560E-01^+$	5.035E-02
		7.502E-02	5.425E-02	2.953E-01	7.112E-01	4.518E-01	3.628E-01	2.228E-01
		4.529E-02	4.961E-02	3.197E-01	7.083E-01	4.408E-01	3.941E-01	4.570E-02
	10	5.011E-02 =	5.238E-02 =	3.323E-01 <sup>+</sup>	7.390E-01 <sup>+</sup>	4.564E-01 +	$4.037E-01^+$	4.939E-02
		6.825E-02	5.565E-02	3.480E-01	7.867E-01	4.748E-01	4.128E-01	2.130E-01
	15	3.739E-02	6.776E-02	5.023E-01	9.562E-01	5.524E-01	4.691E-01	3.793E-02
	15	4.339E-02 -	2.125E-01	5.228E-01	9.652E-01	5.716E-01 T	4.930E-01	4.238E-02
		1.529E-01	9.339E-01	5.380E-01	9.800E-01	5.905E-01	5.144E-01	1.776E-01
		2.447E-02	1.904E-02	6.184E-02	6.988E-02	7.806E-02	5.568E-02	1.371E-02
	3	2.831E-02	2.820E-02	6.474E-02	7.579E-02	8.240E-02	7.527E-02	1.732E-02
9		3.511E-02	3.417E-02	6.728E-02	8.748E-02	8.858E-02	8.048E-02	2.215E-02
Ċ,	Б	2.903E-02	2.600E-02	1.518E-01	4.344E-01	2.025E-01	1.007E-01	1.901E-02
I.N.	5	3.479E-02	3.485E-02	1.598E-01	4.764E-01	2.149E-01	1.720E-01	2.307E-02
-		4.201E-02 3.350E-02	3.874E-02	2.217F 01	5.205E-01 6.502E-01	2.313E-01 2.025E-01	1.708E-01 3.032F_01	2.520E-02
	8	2.827E 02 +	4.278E 02 +	2.2171-01 $2.472E 01^{+}$	6 909E 01 <sup>+</sup>	2.925E-01	2.052E-01	2.203E-02
	0	1.294E-02	4.578E=02	2.472E-01 2.730E-01	7.088E-01	3.031E-01	3.204E-01	3.048E-01
		2.793E=02	3.624E=02	2.957E-01	7.000E-01 7.208E-01	2.893E-01	3.523E=01	2.029E-02
	10	3 728E-02 +	4 392E-02 +	$3.189E_{-}01^{+}$	7.314E-01 <sup>+</sup>	3.072E-01 +	$3.641E_{-}01^{+}$	2.020E 02
		4.548E-02	5.207E-02	3.290E-01	7.663E-01	3.303E-01	3.742E-01	2.962E-02
		2.911E-02	5.071E-02	5.190E-01	9.254E-01	3.386E-01	4.146E-01	1.597E-02
	15	3.599E-02 +	4.863E-01 +	$5.275 \text{E}-01^+$	$9.467 \text{E} - 01^+$	3.528E-01 <sup>+</sup>	$4.442 \text{E-}01^+$	1.984E-02
		4.709E-02	1.109E + 00	5.425E-01	9.698E-01	3.711E-01	4.742E-01	2.384E-02
		2.136E-03	3.927E-03	5.002E-02	8.934E-02	9.725E-02	5.180E-02	2.739E-03
	3	$2.572 \text{E-} 03^{-}$	4.800E-03 <sup>+</sup>	$5.353E-02^+$	$9.496 \text{E}{-}02^+$	1.077E-01 <sup>+</sup>	$5.561 \text{E} - 02^+$	3.575E-03
		3.344E-03	6.481E-03	5.731E-02	9.885E-02	1.205E-01	5.824E-02	4.250E-03
		6.704E-03	1.002E-02	1.407E-01	4.085E-01	2.129E-01	1.586E-01	1.184E-02
	5	$8.688 \text{E-}03^{-}$	1.162E-02 <sup>-</sup>	$1.487E-01^+$	$4.516E-01^+$	2.340E-01 <sup>+</sup>	$1.638E-01^+$	1.385E-02
		1.727E-02	1.381E-02	1.540E-01	4.860E-01	2.436E-01	1.715E-01	2.369E-02
5		1.720E-02	3.053E-02	2.347E-01	6.595E-01	3.255E-01	3.037E-01	2.693E-02
ΕL	8	$\mathbf{2.039E}\text{-}02^{-}$	3.868E-02 <sup>+</sup>	$2.623E-01^+$	$7.024 \text{E-}01^+$	3.384E-01 <sup>+</sup>	$3.108 \text{E-}01^+$	3.424E-02
$\geq$		2.553E-02	7.388E-02	2.899E-01	7.434E-01	3.674E-01	3.255E-01	4.047E-02
		2.167E-02	3.458E-02	3.089E-01	7.288E-01	3.138E-01	3.275E-01	2.264E-02
	10	$\mathbf{2.292E}\text{-}02^{-}$	4.152E-02 <sup>+</sup>	$3.158E-01^+$	$7.656E-01^+$	3.463E-01 <sup>+</sup>	$3.424\text{E-}01^+$	2.466E-02
		2.441E-02	4.932E-02	3.350E-01	7.961E-01	3.629E-01	3.562E-01	2.634E-02
		7.278E-02	3.375E-01	4.973E-01	9.715E-01	3.953E-01	3.683E-01	1.052E-02
	15	1.312E-01 T	6.146E-01	5.163E-01	9.905E-01	4.254E-01 T	4.085E-01	1.333E-02
		4.640E-01	1.104E+00	5.233E-01	1.017E+00	4.440E-01	4.599E-01	8.189E-02
	2	7.309E-02	4.154E-02	9.408E-02	1.402E-01	1.495E-01	8.379E-02	6.507E-02
	3	7.659E-02 '	4.488E-02	9.869E-02	1.443E-01	1.613E-01	8.751E-02	7.534E-02
	-	1.818E-02	5.137E-02 5.621E-02	1.030E-01	1.547E-01 4.470E-01	1.094E-01	9.144E-02	7.977E-02
	5	1.222E-01 1.207E 01 +	5.021E-02	2.044E-01 $2.105E-01^+$	4.470E-01 5.026E.01 <sup>+</sup>	2.805E-01	2.092E-01 2.170E 01 <sup>+</sup>	0.400E-02
	0	1.307E-01	7.042E-02	2.195E-01 2.201E-01	5.020E-01	2.985E-01 3.156E-01	2.170E-01 2.227E 01	1.129E-01 1.244E 01
20		2.483E-01	1 205E-01	3 931E-01	6.844E=01	3.100E-01	3 715E-01	7 524E-02
F	8	2.577E-01 +	$1.2001 01^{-1}$	$4.070E-01^+$	7 101E-01 <sup>+</sup>	4.036E-01 +	$3.925E-01^+$	$1.62 \pm 01$ 1.767E-01
Μ	-	2.642E-01	1.409E-01	4.259E-01	7.445E-01	4.218E-01	4.047E-01	4.293E-01
	-	2.813E-01	1.361E-01	3.785E-01	7.578E-01	3.851E-01	4.332E-01	5.194E-02
	10	3.062E-01 <sup>+</sup>	1.549E-01 <sup>+</sup>	$4.452E-01^+$	7.831E-01 <sup>+</sup>	4.055E-01 <sup>+</sup>	$4.442\text{E-}01^+$	6.690E-02
		3.191E-01	1.618E-01	4.767E-01	8.191E-01	4.210E-01	4.511E-01	3.980E-01
		5.435E-01	6.018E-01	5.788E-01	9.827E-01	4.629E-01	5.401E-01	5.593E-01
	15	5.902E-01 <sup>=</sup>	9.638E-01 <sup>+</sup>	$5.949E-01^{=}$	$9.946E-01^{+}$	$4.827\mathrm{E}\text{-}01^-$	$5.563 \text{E-}01^{-}$	5.912E-01
		6.306E-01	1.113E + 00	6.115E-01	1.020E + 00	4.913E-01	5.715E-01	6.100E-01
		3.281E-02	2.943E-02	6.125E-02	7.135E-02	7.693E-02	6.145E-02	3.069E-02
	3	5.194E-02 =	5.358E-02 =	$7.244E-02^+$	$7.735E-02^+$	8.423E-02 <sup>+</sup>	$8.471E-02^+$	4.163E-02
		6.727E-02	5.840E-02	8.152E-02	8.645E-02	1.088E-01	8.889E-02	6.557E-02
		5.806E-02	5.311E-02	1.683E-01	4.213E-01	2.118E-01	1.940E-01	8.684E-02
	5	9.513E-02 =	$6.368 \text{E-}02^-$	$1.867 \text{E-}01^+$	$4.586E-01^+$	2.597E-01 <sup>+</sup>	$2.052 \text{E-}01^+$	8.806E-02
6		1.036E-01	7.271E-02	1.953E-01	4.720E-01	2.794E-01	2.095E-01	8.986E-02
Ğ		1.182E-01	8.827E-02	2.596E-01	6.317E-01	4.075E-01	3.504E-01	9.126E-02
VF	8	1.340E-01 =	$1.188E-01^{=}$	2.944E-01 <sup>+</sup>	6.853E-01 <sup>+</sup>	4.280E-01 +	3.625E-01 <sup>+</sup>	1.245E-01
-		2.165E-01	1.980E-01	3.239E-01	7.153E-01	4.538E-01	3.760E-01	2.342E-01
1	10	1.071E-01	9.076E-02	3.271E-01	7.213E-01	4.388E-01	3.983E-01	1.396E-01
1	10	1.030E-01	1.233E-01	3.489E-01 2.620E-01	7.420E-01	4.595E-01 '	4.003E-01	1.902E-01
1		1.994E-01	1.075E-01	4 975F 01	9 396F 01	5 585F 01	4.105E-01 5.051F-01	2.407E-01 2.120F 01
1	15	2 322F 01 -	1.6885-01-	5 230F 01+	9.557F 01+	6.046F.01 +	5.001E-01	4 356F 01
1	10	4.239E-01	2.898E-01	5.425E-01	9.995E-01	6.397E-01	5.607E-01	5.835E-01
(+	/=/-)	15/14/16	26/7/12	35/2/8	45/0/0	39/3/3	33/2/10	5.0001 01

	M	NSGA-III	SPEA/R	VaEA	dMOPSO	SMPSO	MaPSO	RMaOPSO
		7.12840E-01	6.82790E-01	8.74760E-01	6.01700E-01	6.06790E-01	8.45320E-01	7.05130E-01
	3	7.03900E-01 <sup>-</sup>	6.70940E-01 <sup>+</sup>	$8.32610 \text{E-}01^{-}$	$5.91580 \text{E-}01^+$	$6.05430 \text{E-}01^+$	7.94780E-01 <sup>-</sup>	6.92700E-01
		6.95820E-01	6.65730E-01	7.94030E-01	5.86330E-01	6.03010E-01	7.54300E-01	6.83840E-01
		6.50050E-01	6.40660E-01	7.67260E-01	3.00280E-01	5.59280E-01	7.64530E-01	6.37340E-01
	5	6 44320E-01 -	6 23950E-01 +	6 95360E-01	2 74170E-01 <sup>+</sup>	5 54510E-01 <sup>+</sup>	7 00990E-01	6.33590E-01
WFG		6.40330E-01	6 19950E-01	6 51580E-01	2.64420E-01	5.52630E=01	6.47850E-01	6.26480E=01
		6.61610E-01	6 74480E-01	8 75640E-01	2.01120E 01 2.87930E-01	5.01750E-01	8.05640E-01	6.99510E-01
	8	$6.00240 \pm 01 =$	6 24840E 01 -	8 50200E 01 -	2.07500E-01 2.75020E-01+	4.00000E 01+	6.05770E.01 -	5.71700E.01
	0	5.86240E-01	4.66500E.01	8.39300E-01	2.75920E-01 2.62100E-01	4.99990E-01	6.00520E.01	4.05100E-01
		5.80340E-01 6.02100E-01	4.00390E-01	0.27990E-01	2.03190E-01	4.96560E-01	0.00520E-01	4.95100E-01
	10	0.93100E-01	0.93930E-01	9.32010E-01	2.98090E-01	4.85500E-01	9.01430L-01	5.31340E-01
		0.51950E-01	0.78220E-01	9.20530E-01	2.82990E-01	4.76400E-01	9.17990E-01	5.07250E-01
		5.66840E-01	4.51850E-01	9.08160E-01	2.72020E-01	4.74000E-01	6.20230E-01	5.04820E-01
		9.87120E-01	9.80730E-01	9.81860E-01	9.43810E-01	9.08100E-01	9.82720E-01	9.85280E-01
	3	9.84290E-01 -	9.84940E-01	9.78080E-01	9.39520E-01	9.62460E-01	9.80360E-01	9.83090E-01
		8.93220E-01	8.92270E-01	8.88500E-01	9.31490E-01	9.52570E-01	9.70600E-01	9.77640E-01
	5	9.96560E-01	9.96080E-01	9.94770E-01	7.44550E-01	9.74820E-01	9.98280E-01	9.93210E-01
52		9.95630E-01	9.95120E-01	9.90850E-01 -	6.88980E-01	9.65900E-01	9.97770E-01	9.89420E-01
Ĕ		8.97790E-01	9.93820E-01	8.94370E-01	6.57400E-01	9.56030E-01	9.95190E-01	9.81090E-01
A		9.97490E-01	9.97090E-01	9.95660E-01	6.96120E-01	9.57910E-01	9.99280E-01	9.84450E-01
	8	9.93110E-01 =	9.95430E-01 <sup>-</sup>	9.91880E-01 <sup>-</sup>	$6.65430 \text{E-}01^+$	$9.39680E-01^{=}$	$9.98750 \mathrm{E-01}^{-1}$	9.64060E-01
		8.94710E-01	8.97440E-01	8.92850E-01	6.42620E-01	9.18920E-01	9.97110E-01	8.55900E-01
		9.98030E-01	9.98120E-01	9.97080E-01	7.18580E-01	9.65180E-01	9.99730E-01	9.93650E-01
	10	9.94850E-01 =	9.97130E-01 <sup>-</sup>	9.95500E-01 <sup>-</sup>	$6.66150 \text{E}-01^+$	$9.49230 \text{E-}01^{=}$	$9.99500 \mathrm{E}{-}01^{-}$	9.85120E-01
		8.95970E-01	8.97380E-01	9.92410E-01	6.52070E-01	9.25840E-01	9.99040E-01	8.87610E-01
		8.75020E-01	8.74280E-01	8.71150E-01	8.62320E-01	8.63000E-01	8.74740E-01	8.71650E-01
	3	$8.71570 \mathrm{E-01}^-$	8.67970E-01 =	8.61310E-01 <sup>+</sup>	$8.53680 \text{E-}01^+$	$8.47220 \text{E-}01^+$	8.65220E-01 =	8.65570E-01
		8.66020E-01	8.53310E-01	8.52490E-01	8.42350E-01	8.36440E-01	8.59630E-01	8.52050E-01
		8.75090E-01	8.60600E-01	8.65350E-01	6.92590E-01	8.48550E-01	8.86780E-01	8.78340E-01
3	5	8.66150E-01 =	8.38480E-01 <sup>+</sup>	8.43920E-01 <sup>+</sup>	6.71660E-01 <sup>+</sup>	8.35830E-01 <sup>+</sup>	$8.72820  ext{E-01}^-$	8.66090E-01
Ū.		8.60270E-01	8.20580E-01	8.28910E-01	6.47770E-01	8.25210E-01	8.63440E-01	8.49740E-01
ΥE		8 73700E-01	7 13170E-01	8 64960E-01	6 76230F 01	8 45170E 01	8 73460E-01	8 39750E-01
~			1.101101-01	0.040001-01	0.1023012-01	0.401701-01	0.101000-01	0.001001-01
M	8	8.55450E-01 -	6.62100E-01 +	8.48120E-01 -	6.49880E-01 <sup>+</sup>	$8.27250E-01^{-1}$	8.62380E-01	8.07590E-01
Μ	8	8.55450E-01 7.91750E-01	6.62100E-01 + 5.89310E-01	8.48120E-01 - 8.29240E-01	6.49880E-01 <sup>+</sup> 6.40190E-01	8.27250E-01 8.18250E-01	8.62380E-01 <sup>-</sup> 8.39310E-01	8.07590E-01 7.12320E-01
M	8	8.55450E-01 - 7.91750E-01 8.67930E-01	6.62100E-01 + 5.89310E-01 7.70670E-01	8.48120E-01 - 8.29240E-01 8.68470E-01	6.49880E-01 <sup>+</sup> 6.40190E-01 6.70530E-01	8.45170E-01 8.27250E-01 8.18250E-01 8.51050E-01	8.62380E-01 <sup>-</sup> 8.39310E-01 8.75170E-01	8.07590E-01 7.12320E-01 8.52380E-01
M	8	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 -	6.62100E-01 + 5.89310E-01 7.70670E-01 7.33000E-01 +	8.48120E-01 - 8.29240E-01 8.68470E-01 8.38090E-01 -	$\begin{array}{c} 6.70250\pm01\\ 6.49880\pm01^+\\ 6.40190\pm01\\ \hline 6.70530\pm01\\ 6.60290\pm01^+\\ \end{array}$	8.43170E-01 8.27250E-01 8.18250E-01 8.51050E-01 8.42760E-01	8.62380E-01 8.39310E-01 8.75170E-01 8.63960E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01
M	8 10	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01	$\begin{array}{c} \text{6.62100E-01} \\ \text{5.89310E-01} \\ \hline \text{7.70670E-01} \\ \text{7.33000E-01} \\ \text{6.32980E-01} \end{array}$	8.04300E-01 8.29240E-01 8.68470E-01 8.38090E-01 8.27910E-01	$\begin{array}{c} 6.70250\pm01\\ 6.49880\pm01^+\\ 6.40190\pm01\\ \hline 6.70530\pm01\\ 6.60290\pm01^+\\ 6.37920\pm01\\ \end{array}$	8.43170E-01 8.27250E-01 8.18250E-01 8.51050E-01 8.42760E-01 8.22140E-01	8.62380E-01 8.39310E-01 8.75170E-01 8.63960E-01 8.48880E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01
M	8 10	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01 9.23800E-01	6.62100E-01 + 5.89310E-01 7.70670E-01 7.33000E-01 + 6.32980E-01 9.22330E-01	8.48120E-01 8.29240E-01 8.68470E-01 8.38090E-01 8.27910E-01 9.20650E-01	$\begin{array}{c} 6.49880 \pm 01^{+} \\ 6.49880 \pm 01^{+} \\ 6.40190 \pm 01 \\ \hline 6.70530 \pm 01 \\ 6.60290 \pm 01^{+} \\ 6.37920 \pm 01 \\ \hline 9.06790 \pm 01 \end{array}$	8.43170E-01 8.27250E-01 8.18250E-01 8.42760E-01 8.42760E-01 8.22140E-01 8.82340E-01	8.62380E-01 8.39310E-01 8.75170E-01 8.63960E-01 8.48880E-01 9.18590E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01 9.23970E-01
M	8 10 3	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.23670E-01 =	6.62100E-01 + 5.89310E-01 7.70670E-01 7.33000E-01 + 6.32980E-01 9.22330E-01 9.2690E-01 +	8.48120E-01 - 8.29240E-01 8.68470E-01 8.38090E-01 - 8.27910E-01 9.20650E-01 9.18680E-01 +	$\begin{array}{c} 6.49880E{-}01^+\\ 6.40190E{-}01\\ \hline 6.70530E{-}01\\ \hline 6.60290E{-}01^+\\ \hline 6.37920E{-}01\\ \hline 9.06790E{-}01\\ \hline 8.97430E{-}01^+\\ \end{array}$	8.45170E-01 8.27250E-01 8.18250E-01 8.51050E-01 8.42760E-01 8.22140E-01 8.82340E-01 8.79280E-01 <sup>+</sup>	8.62380E-01 8.39310E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.16450E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01 9.23970E-01 9.2310E-01
M	8 10 3	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.22670E-01 - 9.21520E-01	$\begin{array}{r} 1.101100E-01 \\ 6.62100E-01 \\ \hline \\ 5.89310E-01 \\ \hline \\ 7.70670E-01 \\ \hline \\ 7.3000E-01 \\ + \\ 6.32980E-01 \\ \hline \\ 9.2030E-01 \\ \hline \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ \end{array}$	8.48120E-01 - 8.29240E-01 8.68470E-01 8.38090E-01 - 8.27910E-01 9.20650E-01 9.18680E-01 + 9.14610E-01	6.49880E-01 <sup>+</sup> 6.40190E-01 6.70530E-01 6.60290E-01 <sup>+</sup> 6.37920E-01 9.06790E-01 8.97430E-01 <sup>+</sup> 8.89830E-01	8.27250E-01 <sup>-</sup> 8.28250E-01 <sup>-</sup> 8.18250E-01 8.51050E-01 8.22140E-01 8.22140E-01 8.79280E-01 <sup>+</sup> 8.74120E-01	8.62380E-01 8.39310E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.16450E-01 + 9.11490E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01 9.22310E-01 9.2120E-01
M	8 10 3	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01 9.23800E-01 9.22670E-01= 9.82040E-01	$\begin{array}{r} 1.101101-011 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline 7.70670E-01 \\ + \\ 6.32980E-01 \\ 9.22330E-01 \\ 9.22330E-01 \\ + \\ 9.17950E-01 \\ + \\ 9.80220E-01 \\ \end{array}$	8.48120E-01 - 8.29240E-01 8.68470E-01 8.38090E-01 - 8.27910E-01 9.20650E-01 9.18680E-01 + 9.14610E-01 9 73930E-01	$\begin{array}{c} 6.49880\text{E-}01^+\\ 6.40190\text{E-}01\\ 6.70530\text{E-}01\\ 6.70530\text{E-}01\\ 6.60290\text{E-}01^+\\ 6.37920\text{E-}01\\ 9.06790\text{E-}01\\ 8.9930\text{E-}01\\ 8.89830\text{E-}01\\ 6.55620\text{E-}01\\ \end{array}$	8.27250E-01 <sup>-</sup> 8.18250E-01 8.18250E-01 8.51050E-01 8.22140E-01 8.82340E-01 8.79280E-01 <sup>+</sup> 8.74120E-01 9.34800E-01	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.16450E-01 + 9.11490E-01 9.82000E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01 9.23970E-01 9.21120E-01 9.81170E-01
4 W	8 10 3 5	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.21520E-01 - 9.21520E-01 - 9.78010E-01 - 9.78010E-01 -	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{4.52980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.17950E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.78940E-01} \\ 9.78940E-0$	8.48120E-01 - 8.29240E-01 - 8.68470E-01 - 8.38090E-01 - 8.27910E-01 - 9.20650E-01 - 9.14610E-01 + 9.14610E-01 + 9.60580E-01 +	6.49880E-01 6.49880E-01 6.40190E-01 6.70530E-01 6.60290E-01 9.06790E-01 8.97430E-01 8.89830E-01 6.55620E-01 6.36480E-01 4.36480E-01 6.36480E-01 4.36480E-01 6.36480E-01 4.364	8.27250E-01 8.27250E-01 8.18250E-01 8.51050E-01 8.42760E-01 8.22140E-01 8.82340E-01 8.79280E-01 9.34800E-01 9.34800E-01 9.25850E-01 <sup>+</sup>	8.62380E-01 8.6380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.1490E-01 9.82000E-01 9.78300E-01 9.78300E-01	8.0759DE-01 7.12320E-01 8.52380E-01 8.52380E-01 8.33230E-01 9.23970E-01 9.2310E-01 9.21120E-01 9.81170E-01 9.75520E-01
G4 W	8 10 3 5	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.21520E-01 - 9.82040E-01 - 9.74300E-01 - 9.74300E-01 -	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{7.33000E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.8920E-01} \\ \textbf{9.78940E-01} \\ \textbf{9.76700E-01} \end{array}$	$\begin{array}{r} 8.48120\text{E-}01 \\ \hline 8.48120\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.68470\text{E-}01 \\ \hline 8.38090\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.18680\text{E-}01 \\ \hline 9.73930\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 4.6310\text{E-}01 \\ \hline 9.64310\text{E-}01 \\ \hline \end{array}$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^+\\ 6.37920\text{E-01}^+\\ 9.06790\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.9830\text{E-01}^+\\ 6.55620\text{E-01}^+\\ 6.35620\text{E-01}^+\\ 6.35620\text{E-01}^+\\ \end{array}$	8.27250E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.2340E-01 8.79280E-01+ 8.74120E-01 9.34800E-01 9.2850E-01+ 9.18370E-01	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.16450E-01 9.1490E-01 9.82000E-01 9.7390E-01 9.7390E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 7.78990E-01 9.2970E-01 9.2970E-01 9.21120E-01 9.81170E-01 9.79520E-01 9.79520E-01
VFG4 W	8 10 3 5	$\begin{array}{r} 8.55450E-01 \\ \hline 7.91750E-01 \\ \hline 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 9.40580E-01 \\ \hline 9.23800E-01 \\ \hline 9.22670E-01 \\ \hline 9.21520E-01 \\ \hline 9.78910E-01 \\ \hline 9.74300E-01 \\ \hline 9.74300E-01 \\ \hline 9.7440E-01 \\ \hline \end{array}$	$\begin{array}{l} \textbf{1.0110E-01} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.78940E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.92110E-01} \end{array}$	8.48120E-01 - 8.29240E-01 - 8.29240E-01 - 8.38090E-01 - 8.27910E-01 - 9.20650E-01 - 9.18680E-01 + 9.14610E-01 - 9.69580E-01 + 9.69580E-01 + 9.69580E-01 - 9.88010E-01 - 9.8801	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^+\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}^-\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}^-\\ 6.55620\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}^-\\ 6.49310\text{E-01}^-\\ \end{array}$	8.27250E-01 8.27250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.2240E-01 8.79280E-01 8.79280E-01 9.34800E-01 9.25850E-01 9.25850E-01 9.2750E-01	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.16450E-01 9.1490E-01 9.78390E-01 9.73290E-01 9.82010E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 7.78990E-01 9.2310E-01 9.21120E-01 9.81170E-01 9.79520E-01 9.76980E-01 9.76980E-01
WFG4 W	8 10 3 5 8	$\begin{array}{l} 8.55450E-01 \\ \hline 8.55450E-01 \\ \hline 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 8.62790E-01 \\ \hline 9.23800E-01 \\ \hline 9.22670E-01 \\ \hline 9.21520E-01 \\ \hline 9.82040E-01 \\ \hline 9.74300E-01 \\ \hline 9.87140E-01 \\ \hline 9.87120E-01 \\ \hline 9.87120E-01 \\ \hline \end{array}$	6.62100E-01 + 5.89310E-01 7.70670E-01 7.33000E-01 + 6.32980E-01 + 9.20690E-01 + 9.17950E-01 9.80220E-01 = 9.76700E-01 = 9.76700E-01 = 9.82240E-01 =	$\begin{array}{l} 8.48120\text{E-}01 \\ \hline 8.48120\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.38090\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.18680\text{E-}01 \\ \hline 9.14610\text{E-}01 \\ \hline 9.73930\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.64310\text{E-}01 \\ \hline 9.88010\text{E-}01 \\ \hline 9.80010\text{E-}01 \\ \hline 9.80010\text{E-}01 \\ \hline \end{array}$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^+\\ 6.37920\text{E-01}^+\\ 9.06790\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}^-\\ 6.55620\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 6.14980\text{E-01}^+\\ \end{array}$	8.27250E-01 8.27250E-01 8.18250E-01 8.51050E-01 8.42760E-01 8.22140E-01 8.79280E-01 8.79280E-01 9.34800E-01 9.25850E-01 9.25850E-01 9.27150E-01 9.10920E-01 +	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.16450E-01 9.16450E-01 9.82000E-01 9.73290E-01 9.73290E-01 9.87910E-01 9.87910E-01 9.8790	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 9.23970E-01 9.22310E-01 9.21120E-01 9.81170E-01 9.76980E-01 9.86530E-01 9.85520E-01 9.85520E-01
WFG4 W	8 10 3 5 8	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.23800E-01 - 9.21520E-01 - 9.74300E-01 - 9.87140E-01 - 9.82120E-01 - 9.7580E 01 - 9.7580E	$\begin{array}{l} 1.101101-011 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ 7.70670E-01 \\ + \\ 6.32980E-01 \\ + \\ 9.22330E-01 \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ 9.80220E-01 \\ - \\ 9.78940E-01 \\ - \\ 9.89240E-01 \\ - \\ 9.$	$\begin{array}{l} 8.48120E-01 \\ 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.68470E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ 9.18680E-01 \\ \hline 9.14610E-01 \\ 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.64310E-01 \\ \hline 9.88010E-01 \\ \hline 9.80910E-01 \\ \hline 9.74200E-01 \\$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40980\text{E-01}^+\\ 6.40190\text{E-01}\\ \hline 6.70530\text{E-01}\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}\\ \hline 6.55620\text{E-01}\\ \hline 6.36480\text{E-01}^+\\ 6.05550\text{E-01}\\ \hline 6.49310\text{E-01}\\ 6.14980\text{E-01}^+\\ 5.85030\text{E-01}\\ \hline 6.3030\text{E-01}\\ \hline \end{array}$	8.42750E-01 8.27250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.79280E-01+ 8.74120E-01 9.34800E-01+ 9.34800E-01 9.25850E-01+ 9.18370E-01 9.27150E-01 9.0920E-01+ 8.85470E-01	$\begin{array}{l} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.63960E-01^{-}\\ 8.48880E-01\\ 9.18590E-01\\ 9.1490E-01\\ 9.82000E-01\\ 9.78390E-01\\ 9.73290E-01\\ 9.87910E-01\\ 9.82390E-01\\ = 0.7370E-01\\ 9.73270E-01\\ \end{array}$	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.3230E-01 9.23970E-01 9.2310E-01 9.21120E-01 9.79520E-01 9.79520E-01 9.76580E-01 9.85530E-01 9.85520E-01 9.85520E-01
WFG4 W	8 10 3 5 8	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 9.23800E-01 9.22670E-01 = 9.74300E-01 = 9.74300E-01 = 9.87140E-01 = 9.82120E-01 = 9.77580E-01 = 9.77580E-01 = 9.8710E-01 = 9.8710E-	$\begin{array}{r} 1.10110E-01 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline 7.70670E-01 \\ + \\ 6.32980E-01 \\ + \\ 9.22330E-01 \\ 9.20330E-01 \\ + \\ 9.17950E-01 \\ - \\ 9.80220E-01 \\ - \\ 9.767700E-01 \\ \hline 9.89240E-01 \\ - \\ 9.85780E-01 \\ - $	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.68470E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.14610E-01 \\ \hline 9.73930E-01 \\ \hline 9.64310E-01 \\ \hline 9.88010E-01 \\ \hline 9.80910E-01 \\ \hline 9.74290E-01 \\ \hline 9.8410E-01 \\ \hline 9.8010E-01 \\ \hline $	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.49880\text{E-01}^+\\ 6.40190\text{E-01}\\ 6.70530\text{E-01}\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}\\ 9.06790\text{E-01}\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}\\ 6.49310\text{E-01}\\ 6.14980\text{E-01}^+\\ 5.85030\text{E-01}\\ 6.5720\text{E-01}\\ \end{array}$	8.37170E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.79280E-01 9.34800E-01 9.34800E-01 9.2850E-01 9.27150E-01 9.27150E-01 9.10920E-01 8.85470E-01 9.40020E 01	8.62380E-01 8.6380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.1450E-01 9.78390E-01 9.73290E-01 9.87910E-01 9.82390E-01 9.73770E-01 9.8000F 01 9.8000F 01	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.3230E-01 9.23970E-01 9.2310E-01 9.21120E-01 9.76980E-01 9.76980E-01 9.8530E-01 9.8520E-01 9.77480E-01 9.7940E-01
WFG4 W	8 10 3 5 8	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.62790E-01 - 8.62790E-01 - 9.23800E-01 9.22670E-01 = 9.21520E-01 = 9.74300E-01 - 9.87140E-01 - 9.87140E-01 - 9.86710E-01 - 9.86710E-01 + 9.86710E-01 + 9.86710E-0	1.10110E-01         6.62100E-01         5.89310E-01         7.70670E-01         7.33000E-01         9.22330E-01         9.22330E-01         9.20690E-01         9.80220E-01         9.76700E-01         9.76700E-01         9.89240E-01         9.85780E-01         9.95840E-01	$\begin{array}{r} 8.48120\text{E-}01 \\ \hline 8.48120\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.68470\text{E-}01 \\ \hline 8.38090\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.16680\text{E-}01 \\ \hline 9.16680\text{E-}01 \\ \hline 9.73930\text{E-}01 \\ \hline 9.64310\text{E-}01 \\ \hline 9.88010\text{E-}01 \\ \hline 9.88010\text{E-}01 \\ \hline 9.88010\text{E-}01 \\ \hline 9.85140\text{E-}01 \\ \hline 9.85140\text{E-}01 \\ \hline 9.85120\text{E-}01 \\ \hline 9.851200\text{E-}01 \\ \hline 9$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.9830\text{E-01}^-\\ 6.55620\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 6.49310\text{E-01}^+\\ 5.85030\text{E-01}^+\\ 5.85030\text{E-01}^+\\ 6.21970\text{E-01}^+\\ 6.21970\text{E-01}^+\\ 6.21970\text{E-01}^+\\ \end{array}$	8.37170E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.2920E-01+ 8.79280E-01+ 9.34800E-01 9.2850E-01+ 9.27150E-01 9.10920E-01+ 8.85470E-01 9.40030E-01 9.27620E 01+	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.16450E-01 9.78390E-01 9.73290E-01 9.87910E-01 9.82390E-01 9.83900E-01 9.839	8.07590E-01 8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 9.23970E-01 9.22310E-01 9.21120E-01 9.21120E-01 9.79520E-01 9.86530E-01 9.86530E-01 9.86530E-01 9.89340E-01 9.87202E 01
WFG4 W	8 10 3 5 8 10	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.40580E-01 - 8.40580E-01 - 9.23800E-01 - 9.21520E-01 - 9.78910E-01 - 9.74300E-01 - 9.87140E-01 - 9.87140E-01 - 9.83350E-01 + 0.7770E 01 - 9.770E 01 - 9.7140E-01 - 9.8350E-01 - 9.7140E-01 - 9.8350E-01 - 9.7140E-01 - 9.8350E-01 - 9.7140E-01 - 9.8350E-01 - 9.7720E 01 - 7.770E 01 -	$\begin{array}{r} 1.101100E-01 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline \\ 7.70670E-01 \\ + \\ 6.32980E-01 \\ + \\ 9.22330E-01 \\ + \\ 9.22330E-01 \\ + \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ \hline \\ 9.89220E-01 \\ - \\ 9.76700E-01 \\ \hline \\ 9.89240E-01 \\ - \\ 9.85780E-01 \\ \hline \\ 9.95840E-01 \\ - \\ 9.95740E-01 \\ - \\ 9.9270E-01 \\ - \\ 9.92$	$\begin{array}{r} 8.48120\text{E-}01 \\ \hline 8.48120\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.18680\text{E-}01 \\ \hline 9.16680\text{E-}01 \\ \hline 9.73930\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.89010\text{E-}01 \\ \hline 9.89010\text{E-}01 \\ \hline 9.81830\text{E-}01 \\ \hline 9.81830\text{E-}01 \\ \hline 9.81830\text{E-}01 \\ \hline 9.72700\text{E-}01 \\ \hline 9.7270$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^+\\ 6.70530\text{E-01}^+\\ 6.7920\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.9830\text{E-01}^+\\ 6.55620\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 5.85030\text{E-01}^+\\ 5.85030\text{E-01}^+\\ 6.57320\text{E-01}^+\\ 6.31970\text{E-01}^+\\ 6.02320\text{E-01}^+\\ 6.02320\text{E-01}^+\\ \end{array}$	8.37170E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.22140E-01 8.79280E-01 9.34800E-01 9.25850E-01 9.27150E-01 9.27150E-01 9.10920E-01 9.40030E-01 9.27630E-01 9.27630E-01 9.11570E 01	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.16450E-01 9.78390E-01 9.73290E-01 9.87910E-01 9.83900E-01 9.83050E-01 9.83050E-01 9.83050E-01 4.72910E-01 9.83050E-01 9.7370E-01 9.83050E-01 9.7370E-01 9.7370E-01 9.83050E-01 9.7370E-01 9.7370E-01 9.83050E-01 9.7370E-01 9.7570E-01	8.07590E-01 8.07590E-01 7.12320E-01 8.3230E-01 9.33970E-01 9.22310E-01 9.21120E-01 9.7170E-01 9.70520E-01 9.8530E-01 9.8530E-01 9.85320E-01 9.83520E-01 9.89340E-01 9.87020E-01 9.87020E-01 9.87020E-01 9.87020E-01
WFG4 W	8 10 3 5 8 10	$\begin{array}{r} 8.55450E-01 \\ \hline 8.55450E-01 \\ \hline 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 8.62790E-01 \\ \hline 9.23800E-01 \\ \hline 9.22670E-01 \\ \hline 9.21520E-01 \\ \hline 9.21520E-01 \\ \hline 9.74300E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.8710E-01 \\ \hline 9.8350E-01 \\ \hline 9.83350E-01 \\ \hline 9.77770E-01 \\ \hline 9.2727E-01 \\ \hline$	6.62100E-01 + 5.89310E-01 7.70670E-01 7.33000E-01 + 6.32980E-01 + 9.22330E-01 + 9.20690E-01 + 9.20690E-01 + 9.80220E-01 = 9.76700E-01 = 9.76700E-01 = 9.89240E-01 - 9.89240E-01 - 9.95840E-01 - 9.93070E-01 - 9.93070E-01 -	$\begin{array}{l} 8.48120\text{E-}01 \\ \hline 8.48120\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.29240\text{E-}01 \\ \hline 8.38090\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.20650\text{E-}01 \\ \hline 9.18680\text{E-}01 \\ \hline 9.14610\text{E-}01 \\ \hline 9.73930\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.69580\text{E-}01 \\ \hline 9.88010\text{E-}01 \\ \hline 9.80910\text{E-}01 \\ \hline 9.8140\text{E-}01 \\ \hline 9.81830\text{E-}01 \\ \hline 9.81830\text{E-}01 \\ \hline 9.78790\text{E-}01 \\ \hline 9.78790\text{E-}01 \\ \hline 0.0000\text{E-}01 \\ \hline 0.00000\text{E-}01 \\ \hline 0.000000\text{E-}01 \\ \hline 0.0000000\text{E-}01 \\ \hline 0.000000\text{E-}01 \\ \hline 0.000000\text{E-}01 \\ \hline 0.000000000\text{E-}01 \\ \hline 0.000000000000\text{E-}01 \\ \hline 0.000000000000000000000000000000000$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^-\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}^-\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}^-\\ 6.55620\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 6.49310\text{E-01}^+\\ 6.57320\text{E-01}^-\\ 6.31970\text{E-01}^+\\ 6.3330\text{E-01}^-\\ 6.3330\text{E-01}^-\\ 6.93300\text{E-01}^-\\ 6.93300$	8.27250E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.79280E-01 8.79280E-01 9.34800E-01 9.25850E-01 9.1920E-01 9.10920E-01 9.40030E-01 9.40030E-01 9.27650E-01 9.27650E-01 9.27650E-01 9.27650E-01 9.2765	$\begin{array}{l} 8.62380E-01 \\ \hline 8.62380E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 8.63960E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.1490E-01 \\ \hline 9.82000E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.83900E-01 \\ \hline 9.83900E-01 \\ \hline 9.83050E-01 \\ \hline 9.83050E-01 \\ \hline 9.73810E-01 \\ \hline 9.73810E$	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 9.23970E-01 9.22310E-01 9.21120E-01 9.81170E-01 9.7520E-01 9.8530E-01 9.8520E-01 9.8520E-01 9.77480E-01 9.87020E-01 9.80330E-01 9.80330E-01
WFG4 W	8 10 3 5 8 10	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 9.23800E-01 9.23800E-01 9.21520E-01 9.74300E-01 9.87140E-01 9.87140E-01 9.8350E-01 - 9.83350E-01 9.03370E-01 9.03370E-01	$\begin{array}{l} 1.01100E-01 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline 7.70670E-01 \\ - \\ 7.33000E-01 \\ + \\ 6.32980E-01 \\ - \\ 9.22330E-01 \\ - \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ - \\ 9.89240E-01 \\ - \\ 9.89240E-01 \\ - \\ 9.85780E-01 \\ - \\ 9.95840E-01 \\ - \\ 9.95840E-01 \\ - \\ 9.93070E-01 \\ - \\ 8.98040E-01 \\ - \\ 9.93070E-01 \\ - \\ 8.98040E-01 \\ - \\ 9.93070E-01 \\ - \\ 8.98040E-01 \\ - \\ 9.93070E-01 \\ - \\ 9.930E-01 \\ + \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.68470E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.14610E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88140E-01 \\ \hline 9.8140E-01 \\ \hline 9.81830E-01 \\ \hline 9.8790E-01 \\ \hline 9.78790E-01 \\ \hline 9.02990E-01 \\ \hline 9.0290E-01 \\ \hline$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^-\\ 6.0290\text{E-01}^+\\ 6.37920\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.9830\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.3550\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 6.49310\text{E-01}^+\\ 6.57320\text{E-01}^-\\ 6.31970\text{E-01}^+\\ 6.0330\text{E-01}^+\\ 8.82540\text{E-01}^+\\ 8.82540$	8.32750E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.79280E-01 8.79280E-01 9.25850E-01 9.25850E-01 9.25850E-01 9.27150E-01 9.27050E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 9.27630E-01 8.72420E-01	$\begin{array}{l} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.63960E-01^{-}\\ 8.48880E-01\\ 9.18590E-01\\ 9.16450E-01^{+}\\ 9.11490E-01\\ 9.82000E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.8390E-01\\ 9.83900E-01\\ 9.83050E-01\\ 9.83050E-01\\ +\\ 9.73810E-01\\ 8.92250E-01\\ 4.570E-01\\ +\\ 9.73810E-01\\ 8.92250E-01\\ 4.570E-01\\ +\\ 9.73810E-01\\ 8.92250E-01\\ +\\ 9.73810E-01\\ 4.570E-01\\ +\\ 9.73810E-01\\ +\\ 9.75810E-01\\ +\\ 9.75$	8.0759DE-01 7.12320E-01 8.52380E-01 8.52380E-01 8.3230E-01 9.2310E-01 9.2310E-01 9.21120E-01 9.79800E-01 9.79800E-01 9.83520E-01 9.83520E-01 9.8930E-01 9.8930E-01 9.8030E-01 9.8030E-01 9.02500E-01
WFG4 W	8 10 3 5 8 10 3	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 9.23800E-01 9.22670E-01 = 9.21520E-01 = 9.74300E-01 = 9.74300E-01 = 9.87140E-01 = 9.87140E-01 = 9.86710E-01 = 9.8350E-01 + 9.77770E-01 = 9.03370E-01 = 8.99610E-01 = 9.01 =	$\begin{array}{l} 1.101100E-01 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline \\ 7.70670E-01 \\ + \\ 6.32980E-01 \\ + \\ 9.22330E-01 \\ 9.20330E-01 \\ + \\ 9.17950E-01 \\ 9.80220E-01 \\ - \\ 9.80220E-01 \\ \hline \\ 9.76700E-01 \\ \hline \\ 9.92110E-01 \\ - \\ 9.85780E-01 \\ - \\ 9.94740E-01 \\ - \\ 9.93070E-01 \\ \hline \\ 8.98040E-01 \\ - \\ 8.98180E-01 \\ + \\ 8.90120E-01 \\ - \\ \end{array}$	$\begin{array}{l} 8.48120E-01 \\ 8.48120E-01 \\ 8.29240E-01 \\ 8.68470E-01 \\ 8.38090E-01 \\ - \\ 8.27910E-01 \\ 9.20650E-01 \\ 9.20650E-01 \\ 9.18680E-01 \\ + \\ 9.14610E-01 \\ 9.64310E-01 \\ 9.64310E-01 \\ 9.80910E-01 \\ - \\ 9.80910E-01 \\ - \\ 9.8100E-01 \\ - \\ 9.8100E-01 \\ + \\ 9.78790E-01 \\ 9.02990E-01 \\ 8.98100E-01 \\ = \\ 8.02700E-01 \\ - \\ 8.0270E-01 \\ - \\ 8.028E-01 \\ - \\ 8.018E-01 \\ - \\ 8.0$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.49880\text{E-01}^+\\ 6.40190\text{E-01}\\ 6.70530\text{E-01}\\ 6.60290\text{E-01}^+\\ 6.37920\text{E-01}\\ 9.06790\text{E-01}\\ 8.97430\text{E-01}^+\\ 8.89830\text{E-01}^+\\ 6.35502\text{E-01}\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}\\ 6.49310\text{E-01}\\ 6.14980\text{E-01}^+\\ 5.85030\text{E-01}\\ 6.31970\text{E-01}^+\\ 6.03330\text{E-01}\\ 8.82540\text{E-01}\\ 8.80560\text{E-01}^+\\ 8.70580\text{E-01} \\ \end{array}$	8.37170E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.82340E-01 8.79280E-01+ 8.74120E-01 9.34800E-01+ 9.27150E-01 9.27150E-01 9.40030E-01+ 9.27630E-01+ 9.27420E-01 8.72420E-01 8.5590E-01+ 8	8.62380E-01 8.63960E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.18590E-01 9.18450E-01 9.73290E-01 9.73290E-01 9.87910E-01 9.83900E-01 9.83900E-01 9.83000E-01 9.83000E-01 9.83050E-01 8.92250E-01 8.92250E-01 8.87070E-01 + 8.87270E-01 + 8.87270E-01	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.52380E-01 9.23970E-01 9.22310E-01 9.21120E-01 9.21120E-01 9.79520E-01 9.76980E-01 9.8530E-01 9.8720E-01 9.80330E-01 9.80330E-01 9.02860E-01 8.97510E-01
WFG4 W	8 10 3 5 8 10 3	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01 9.23800E-01 9.22670E-01= 9.21520E-01 9.78910E-01 = 9.74300E-01 9.87140E-01 9.87140E-01 9.86710E-01 9.8350E-01 + 9.7770E-01 8.99610E-01= 8.995120E-01 8.95120E-01	1.10110E-01         6.62100E-01         7.70670E-01         7.33000E-01         7.3300E-01         9.22330E-01         9.22330E-01         9.20690E-01         9.80220E-01         9.76700E-01         9.76700E-01         9.89240E-01         9.95840E-01         9.93070E-01         8.98040E-01         8.98130E-01         4.88130E-01	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.27910E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.16680E-01 \\ \hline 9.73930E-01 \\ \hline 9.64310E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88100E-01 \\ \hline 9.8830E-01 \\ \hline 9.74290E-01 \\ \hline 9.8830E-01 \\ \hline 9.74290E-01 \\ \hline 9.8790E-01 \\ \hline 9.02990E-01 \\ \hline 8.98100E-01 \\ \hline 8.98100E-01 \\ \hline 8.98790E-01 \\ \hline 8.93790E-01 \\ \hline 8.93790E-01 \\ \hline 8.93790E-01 \\ \hline 8.940E-01 \\ \hline 9.56740E-01 \\ \hline 9.55740E-01 $	$\begin{array}{c} 6.49880E{-}01^{+}\\ 6.49880E{-}01^{+}\\ 6.40190E{-}01^{-}\\ 6.60290E{-}01^{+}\\ 6.37920E{-}01^{-}\\ 9.06790E{-}01^{-}\\ 8.97430E{-}01^{+}\\ 8.9830E{-}01^{-}\\ 6.55620E{-}01^{-}\\ 6.36480E{-}01^{+}\\ 6.05550E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 5.85030E{-}01^{-}\\ 6.31970E{-}01^{+}\\ 6.03330E{-}01^{-}\\ 8.82540E{-}01^{+}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 8.70580$	8.37170E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.82340E-01 8.79280E-01+ 8.74120E-01 9.34800E-01 9.28550E-01+ 9.27150E-01 9.27150E-01 9.27630E-01+ 8.5470E-01 9.40030E-01+ 8.5470E-01 8.72420E-01 8.72420E-01 8.5590E-01+ 8.54300E-01	$\begin{array}{l} 8.62380E-01 \\ \hline 8.62380E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.1490E-01 \\ \hline 9.82000E-01 \\ \hline 9.73290E-01 \\ \hline 9.87910E-01 \\ \hline 9.83900E-01 \\ \hline 9.83900E-01 \\ \hline 9.83900E-01 \\ \hline 9.83050E-01 \\ \hline 9.73770E-01 \\ \hline 9.73810E-01 \\ \hline 8.92250E-01 \\ \hline 8.87070E-01 \\ \hline 8.82730E-01 \\ \hline 8.82750E-01 \\ \hline 8.82750E-01 \\ \hline 8.82750E$	8.07590E-01 8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 9.23970E-01 9.22310E-01 9.2310E-01 9.21120E-01 9.79520E-01 9.86530E-01 9.86530E-01 9.86530E-01 9.86530E-01 9.8720E-01 9.8030E-01 9.8030E-01 9.02860E-01 8.97510E-01 8.91570E-01 8.91570E-01
WFG4 W	8 10 3 5 8 10 3 5	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.62790E-01 - 8.62790E-01 - 9.23800E-01 9.22670E-01 = 9.21520E-01 = 9.74300E-01 - 9.82140E-01 - 9.82120E-01 = 9.77580E-01 - 9.8350E-01 + 9.77770E-01 - 8.99610E-01 = 8.99610E-01 = 8.95120E-01 - 9.59720E-01	1.01100E-01         6.62100E-01         7.70670E-01         7.33000E-01         7.3300E-01         9.22330E-01         9.22330E-01         9.20690E-01         9.20690E-01         9.80220E-01         9.78940E-01         9.76700E-01         9.89240E-01         9.89240E-01         9.95840E-01         9.95840E-01         9.94740E-01         9.93070E-01         8.98040E-01         8.93180E-01         9.50670E-01	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.27910E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.16680E-01 \\ \hline 9.73930E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.88010E-01 \\ \hline 9.88910E-01 \\ \hline 9.88130E-01 \\ \hline 9.74290E-01 \\ \hline 9.8790E-01 \\ \hline 9.02990E-01 \\ \hline 8.98100E-01 \\ \hline 8.93790E-01 \\ \hline 9.56040E-01 \\ \hline 9.56040E$	$\begin{array}{c} 6.49880E{-}01^{+}\\ 6.40190E{-}01^{-}\\ 6.40190E{-}01^{-}\\ 6.70530E{-}01^{-}\\ 6.60290E{-}01^{+}\\ 6.37920E{-}01^{-}\\ 8.97430E{-}01^{+}\\ 8.9830E{-}01^{-}\\ 8.9830E{-}01^{-}\\ 6.55620E{-}01^{-}\\ 6.36480E{-}01^{+}\\ 6.05550E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 6.49310E{-}01^{+}\\ 6.14980E{-}01^{+}\\ 5.85030E{-}01^{-}\\ 6.3330E{-}01^{-}\\ 6.3330E{-}01^{-}\\ 8.82540E{-}01^{+}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 6.2020E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 6.2020E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 8.70580E{-}01^{-}\\ 8.70580E{-}0$	$\begin{array}{c} 8.3770\text{E}{-}01^{-}\\ 8.27250\text{E}{-}01^{-}\\ 8.18250\text{E}{-}01\\ 8.18250\text{E}{-}01\\ 8.51050\text{E}{-}01\\ 8.22140\text{E}{-}01\\ 8.22140\text{E}{-}01\\ 8.22140\text{E}{-}01\\ 8.22140\text{E}{-}01\\ 9.2980\text{E}{-}01^{+}\\ 8.74120\text{E}{-}01\\ 9.34800\text{E}{-}01\\ 9.25850\text{E}{-}01^{+}\\ 9.18370\text{E}{-}01\\ 9.27150\text{E}{-}01\\ 9.27630\text{E}{-}01^{+}\\ 9.10920\text{E}{-}01^{+}\\ 8.5470\text{E}{-}01\\ 9.27630\text{E}{-}01^{+}\\ 9.11570\text{E}{-}01\\ 8.65590\text{E}{-}01^{+}\\ 8.54300\text{E}{-}01\\ 8.857640\text{E}{-}01\\ 8.87640\text{E}{-}01\\ 8.87640\text{E}{-}01\\ \end{array}$	8.62380E-01 8.62380E-01 8.75170E-01 8.63960E-01 9.18590E-01 9.18590E-01 9.16450E-01 9.78390E-01 9.73290E-01 9.87910E-01 9.83050E-01 9.83050E-01 9.83050E-01 4.82730E-01 9.51630E-01 9.51630E-01 9.404075.c1 +	8.07590E-01 7.12320E-01 8.52380E-01 8.33230E-01 9.23970E-01 9.22310E-01 9.21120E-01 9.21120E-01 9.79520E-01 9.76980E-01 9.86530E-01 9.86530E-01 9.83520E-01 9.83520E-01 9.8030E-01 9.8030E-01 9.02860E-01 8.97510E-01 8.97510E-01 8.91570E-01 9.61260E-01
G5 WFG4 W	8 10 3 5 8 10 3 5	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.67930E-01 - 8.40580E-01 - 9.23800E-01 - 9.23800E-01 - 9.23800E-01 - 9.21520E-01 - 9.74300E-01 - 9.74300E-01 - 9.87140E-01 - 9.87140E-01 - 9.8350E-01 - 9.8350E-01 - 9.77770E-01 - 9.03370E-01 - 8.99610E-01 - 8.995120E-01 - 9.58590E-01 - 9.58590E-	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.3000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.95780E-01} \\ \textbf{9.95840E-01} \\ \textbf{9.95840E-01} \\ \textbf{9.93070E-01} \\ \textbf{8.93180E-01} \\ \textbf{8.93180E-01} \\ \textbf{9.50670E-01} \\ \textbf{9.47760E-01} \\ \textbf{+} \\ \textbf{4.89130E-01} \\ \textbf{9.50670E-01} \\ \textbf{9.47760E-01} \\ \textbf{1.5760E-01} \\ \textbf{9.47760E-01} \\ \textbf{1.5760E-01} \\ $	$\begin{array}{l} 8.48120E-01 \\ 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.68470E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ 9.20650E-01 \\ 9.18680E-01 \\ + \\ 9.14610E-01 \\ \hline 9.73930E-01 \\ 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.63500E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88140E-01 \\ \hline 9.81830E-01 \\ \hline 9.81830E-01 \\ \hline 9.78790E-01 \\ \hline 9.78790E-01 \\ \hline 9.78790E-01 \\ \hline 9.78790E-01 \\ \hline 9.58010E-01 \\ \hline 9.56040E-01 \\ \hline 9.53650E-01 \\ \hline 9.56040E-01 \\ \hline 9.53650E-01 \\ \hline 9.56040E-01 \\ \hline 9.56040E-01 \\ \hline 9.53650E-01 \\ \hline 9.56040E-01 \\ \hline 9.56040E-01 \\ \hline 9.53650E-01 \\ \hline 9.56040E-01 \\$	$\begin{array}{c} 6.49880\text{E-01}^+\\ 6.49880\text{E-01}^+\\ 6.40190\text{E-01}^-\\ 6.70530\text{E-01}^-\\ 6.0290\text{E-01}^+\\ 9.06790\text{E-01}^+\\ 8.97430\text{E-01}^+\\ 8.9830\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.35502\text{E-01}^-\\ 6.36480\text{E-01}^+\\ 6.05550\text{E-01}^-\\ 6.49310\text{E-01}^+\\ 6.57320\text{E-01}^-\\ 6.57320\text{E-01}^+\\ 6.03330\text{E-01}^+\\ 8.80560\text{E-01}^+\\ 8.80560\text{E-01}^+\\ 8.70580\text{E-01}^-\\ 6.24710\text{E-01}^-\\ 6.09680\text{E-01}^+\\ 5.005\text{E-01}^+\\ 6.09680\text{E-01}^+\\ \end{array}$	8.27250E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.22140E-01 8.79280E-01+ 8.74120E-01 9.34800E-01 9.25850E-01+ 9.10920E-01+ 8.85470E-01 9.40030E-01 9.27630E-01+ 9.10920E-01+ 8.75420E-01 8.752420E-01 8.75400E-01 8.7640E-01 8.7640E-01 8.70720E-01+ 8.7570E-01+	$\begin{array}{l} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.63960E-01^{-}\\ 8.48880E-01\\ 9.18590E-01\\ 9.18590E-01\\ 9.1490E-01\\ 9.82000E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 8.82730E-01\\ 8.82730E-01\\ 9.51630E-01\\ 9.40420E-01\\ +\\ 9.70E-01\\ 9.600E-01\\ 9.60$	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.52380E-01 9.23970E-01 9.2310E-01 9.21120E-01 9.79520E-01 9.79520E-01 9.76530E-01 9.85320E-01 9.87202E-01 9.87202E-01 9.89340E-01 9.89340E-01 9.89340E-01 9.89510E-01 9.961260E-01 9.603
PG5 WFG4 W	8 10 3 5 8 10 3 5	8.55450E-01 - 7.91750E-01 8.67930E-01 - 8.62790E-01 - 8.40580E-01 - 9.23800E-01 - 9.23800E-01 - 9.23800E-01 - 9.23800E-01 - 9.21520E-01 - 9.74300E-01 - 9.87140E-01 - 9.87140E-01 - 9.871580E-01 - 9.8350E-01 + 9.77770E-01 - 8.99610E-01 - 8.995120E-01 - 9.59720E-01 - 9.57080E-01 - 9.57080	$\begin{array}{l} 1.1011010-01 \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline 7.70670E-01 \\ 7.33000E-01 \\ + \\ 6.32980E-01 \\ 9.22330E-01 \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ 9.80220E-01 \\ \hline 9.80220E-01 \\ 9.76700E-01 \\ \hline 9.89240E-01 \\ - \\ 9.85780E-01 \\ 9.95840E-01 \\ \hline 9.93070E-01 \\ 8.98040E-01 \\ \hline 8.98040E-01 \\ 8.93180E-01 \\ + \\ 8.89130E-01 \\ 9.50670E-01 \\ 9.46240E-01 \\ - \\ 9.50670E-01 \\ - \\ 9.50670E-01 \\ - \\ 9.50670E-01 \\ - \\ 9.46240E-01 \\ - \\ 9.50670E-01 \\ - \\ 9.5070E-01 \\ - \\ 9.5070E-01 \\ - \\ 9.5070$	$\begin{array}{l} 8.48120E-01 \\ 8.48120E-01 \\ 8.29240E-01 \\ 8.68470E-01 \\ 8.38090E-01 \\ - \\ 8.27910E-01 \\ 9.20650E-01 \\ 9.20650E-01 \\ 9.18680E-01 \\ + \\ 9.14610E-01 \\ 9.64310E-01 \\ 9.64310E-01 \\ 9.80910E-01 \\ = \\ 9.74290E-01 \\ 9.85140E-01 \\ 9.8100E-01 \\ 9.8100E-01 \\ 9.898100E-01 \\ 9.3790E-01 \\ 9.5650E-01 \\ 9.566040E-01 \\ 9.56650E-01 \\ + \\ 9.49460E-01 \\ - \\ 9.640E-01 \\ - \\ 9.660E-01 \\ - \\ 9.6$	$\begin{array}{c} 6.49880E{-}01^{+}\\ 6.40190E{-}01^{-}\\ 6.40190E{-}01^{-}\\ 6.60290E{-}01^{+}\\ 6.37920E{-}01^{-}\\ 9.06790E{-}01^{-}\\ 8.97430E{-}01^{+}\\ 8.9830E{-}01^{-}\\ 6.36480E{-}01^{+}\\ 6.3550E{-}01^{-}\\ 6.36480E{-}01^{+}\\ 6.35502E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 6.35030E{-}01^{-}\\ 6.37320E{-}01^{-}\\ 6.3330E{-}01^{+}\\ 8.82540E{-}01^{+}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 6.09680E{-}01^{+}\\ 5.96880E{-}01^{-}\\ 5.96880E{-}01^{-}\\ \end{array}$	8.32750E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.82340E-01 8.79280E-01+ 8.74120E-01 9.25850E-01+ 9.27550E-01 9.27150E-01 9.27630E-01+ 9.11570E-01 8.72420E-01 8.5590E-01+ 8.5550E-01+ 8.5720E-01 8.7720E-01+ 8.57520E-01	$\begin{array}{l} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.75170E-01^{-}\\ 8.4880E-01^{-}\\ 9.18590E-01^{-}\\ 9.18590E-01\\ 9.1490E-01\\ 9.78390E-01^{-}\\ 9.73290E-01\\ 9.73290E-01\\ 9.82390E-01 =\\ 9.73290E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 8.92250E-01\\ 8.92250E-01\\ 8.87070E-01\\ 9.51630E-01\\ 9.51630E-01\\ 9.32700E-01\\ 9.3270E-01\\ 9.3$	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.3230E-01 9.2310E-01 9.2310E-01 9.21120E-01 9.78980E-01 9.79520E-01 9.76980E-01 9.8520E-01 9.8720E-01 9.8030E-01 9.87510E-01 8.91570E-01 9.61260E-01 9.6360E-01 9.63500E-01
WFG5 WFG4 W	8 10 3 5 8 10 3 5 5	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01 9.23800E-01 9.23800E-01 9.23800E-01 9.24500E-01 9.74300E-01 9.87140E-01 9.87140E-01 9.87140E-01 9.86710E-01 9.8350E-01 9.77770E-01 9.03370E-01 8.99610E-01= 8.995120E-01 9.58590E-01 9.58590E-01 9.562480E-01 9.62480E-01	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.20330E-01} \\ \textbf{9.20330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.2030E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.93580E-01} \\ \textbf{9.94740E-01} \\ \textbf{9.93670E-01} \\ \textbf{8.93180E-01} \\ \textbf{8.93180E-01} \\ \textbf{8.93180E-01} \\ \textbf{9.50670E-01} \\ \textbf{9.47760E-01} \\ \textbf{9.46240E-01} \\ \textbf{9.58040E-01} \\ \textbf{9.580E-01} \\$	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.18680E-01 \\ \hline 9.14610E-01 \\ \hline 9.73930E-01 \\ \hline 9.64310E-01 \\ \hline 9.64310E-01 \\ \hline 9.80910E-01 \\ \hline 9.80910E-01 \\ \hline 9.85140E-01 \\ \hline 9.81800E-01 \\ \hline 9.81800E-01 \\ \hline 9.81800E-01 \\ \hline 9.89100E-01 \\ \hline 9.89100E-01 \\ \hline 9.83600E-01 \\ \hline 9.53650E-01 \\ \hline 9.53650E-01 \\ \hline 9.49460E-01 \\ \hline 9.62240E-01 \\ \hline 9.6240E-01 \\ \hline 9.6240E-$	$\begin{array}{c} 6.49880E{-}01^{+}\\ 6.49880E{-}01^{+}\\ 6.40190E{-}01^{-}\\ 6.60290E{-}01^{+}\\ 6.37920E{-}01^{-}\\ 9.66790E{-}01^{-}\\ 8.97430E{-}01^{+}\\ 8.9830E{-}01^{-}\\ 6.55620E{-}01^{-}\\ 6.49310E{-}01^{-}\\ 6.49310E{-}01^{-}\\ 6.49310E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 6.31970E{-}01^{+}\\ 6.03330E{-}01^{-}\\ 8.82540E{-}01^{+}\\ 8.80560E{-}01^{+}\\ 8.80560E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 6.24710E{-}01^{-}\\ 6.09680E{-}01^{+}\\ 5.96880E{-}01^{-}\\ 5.96880E{-}01^{-}\\ 6.01020E{-}01^{+}\\ 5.96880E{-}01^{-}\\ \end{array}$	$\begin{array}{c} 8.3770 \text{E}{-}01^{-}\\ 8.27250 \text{E}{-}01^{-}\\ 8.18250 \text{E}{-}01^{-}\\ 8.18250 \text{E}{-}01^{-}\\ 8.2140 \text{E}{-}01^{-}\\ 8.22140 \text{E}{-}01^{-}\\ 8.22140 \text{E}{-}01^{-}\\ 8.22140 \text{E}{-}01^{-}\\ 8.72280 \text{E}{-}01^{+}\\ 8.74120 \text{E}{-}01^{-}\\ 9.2850 \text{E}{-}01^{+}\\ 9.2850 \text{E}{-}01^{+}\\ 9.27150 \text{E}{-}01^{-}\\ 9.27150 \text{E}{-}01^{-}\\ 9.27630 \text{E}{-}01^{+}\\ 9.27630 \text{E}{-}01^{+}\\ 9.11570 \text{E}{-}01\\ 8.72420 \text{E}{-}01^{+}\\ 8.5590 \text{E}{-}01^{+}\\ 8.57640 \text{E}{-}01\\ 8.77750 \text{E}{-}01\\ 8.77750 \text{E}{-}01\\ 8.77750 \text{E}{-}01 \\ 8.77750 \text{E}{-}01 \\ \end{array}$	$\begin{array}{l} 8.62380E-01 \\ \hline 8.62380E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 8.63960E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.182000E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.83900E-01 \\ \hline 9.83900E-01 \\ \hline 9.83900E-01 \\ \hline 9.83050E-01 \\ \hline 9.83050E-01 \\ \hline 9.83050E-01 \\ \hline 9.73770E-01 \\ \hline 9.83050E-01 \\ \hline 9.7370E-01 \\ \hline 9.7370E-01 \\ \hline 9.7370E-01 \\ \hline 9.7360E-01 \\ \hline 9.40420E-01 \\ \hline 9.40570E-01 \\ \hline 9.40570E-0$	8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 8.52380E-01 9.2330E-01 9.2310E-01 9.2310E-01 9.21120E-01 9.79520E-01 9.76980E-01 9.86530E-01 9.87020E-01 9.80330E-01 9.02860E-01 9.63900E-01 9.63900E-01 9.63990E
WFG5 WFG4 W	8 10 3 5 8 10 3 5 8 8	8.55450E-01 - 7.91750E-01 8.67930E-01 8.62790E-01 - 8.40580E-01 9.23800E-01 9.22670E-01= 9.21520E-01 9.78910E-01 = 9.74300E-01 9.87140E-01 9.87140E-01 9.87140E-01 9.8350E-01 + 9.77580E-01 8.99610E-01= 8.95120E-01 9.59720E-01 9.59720E-01 9.5590E-01 + 9.57080E-01 9.60390E-01 + 9.60390E-01 + 9.60390E	$\begin{array}{l} \textbf{1.51101-01} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.95840E-01} \\ \textbf{9.935780E-01} \\ \textbf{9.935780E-01} \\ \textbf{8.98040E-01} \\ \textbf{8.93180E-01} \\ \textbf{8.89130E-01} \\ \textbf{8.89130E-01} \\ \textbf{9.56670E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{+} \\ \textbf{9.55180E-01} \\ \textbf{-} \\ \textbf{9.55180E-01} \\ 9$	$\begin{array}{l} 8.48120E-01 \\ = \\ 8.48120E-01 \\ = \\ 8.29240E-01 \\ \hline \\ 8.29240E-01 \\ = \\ 8.27910E-01 \\ = \\ 9.20650E-01 \\ = \\ 9.73930E-01 \\ = \\ 9.64310E-01 \\ = \\ 9.64310E-01 \\ = \\ 9.88010E-01 \\ = \\ 9.88100E-01 \\ = \\ 9.74290E-01 \\ = \\ 9.88100E-01 \\ = \\ 8.93790E-01 \\ = \\ 9.660370E-01 \\ = \\ 9.60370E-01 \\ = \\ 9.60$	$\begin{array}{l} 6.49880E{-}01^{+}\\ 6.49880E{-}01^{+}\\ 6.40190E{-}01^{-}\\ 6.60290E{-}01^{+}\\ 6.37920E{-}01^{-}\\ 9.06790E{-}01^{-}\\ 8.97430E{-}01^{+}\\ 8.9830E{-}01^{+}\\ 8.9830E{-}01^{+}\\ 6.55620E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 6.05550E{-}01^{-}\\ 6.49310E{-}01^{+}\\ 5.85030E{-}01^{-}\\ 6.37320E{-}01^{-}\\ 6.37320E{-}01^{-}\\ 6.37320E{-}01^{-}\\ 8.82540E{-}01^{+}\\ 8.70580E{-}01^{-}\\ 8.70580E{-}01^{-}\\ 6.09680E{-}01^{+}\\ 5.96880E{-}01^{-}\\ 6.01020E{-}01^{+}\\ 5.67660E{-}01^{+}\\ \end{array}$	8.37750E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.22140E-01 8.29280E-01+ 8.74120E-01 9.34800E-01 9.27550E-01+ 9.27550E-01 9.27630E-01 9.27630E-01 8.72420E-01 8.72420E-01 8.7640E-01 8.7640E-01 8.77750E-01 8.57750E-01 8.56950E-01+ 8.56950E	$\begin{array}{l} 8.62380E-01 \\ \hline 8.62380E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 8.63960E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.1490E-01 \\ \hline 9.82000E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.83900E-01 \\ \hline 9.87910E-01 \\ \hline 9.83050E-01 \\ \hline 9.73770E-01 \\ \hline 9.83050E-01 \\ \hline 9.73770E-01 \\ \hline 9.73810E-01 \\ \hline 8.92250E-01 \\ \hline 8.82730E-01 \\ \hline 8.82730E-01 \\ \hline 9.51630E-01 \\ \hline 9.32700E-01 \\ \hline 9.45370E-01 \\ \hline 9.38590E-01 \\ \hline 9.38590E-01 \\ \hline 9.38590E-01 \\ \hline 9.3650E-01 \\ \hline 9.45370E-01 \\ \hline 9.45370E-01 \\ \hline 9.45370E-01 \\ \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline 9.38590E-01 \\ \hline \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline \hline \hline 9.38590E-01 \\ \hline \hline \hline 9.38590E-01 \\ \hline \hline \hline \hline 9.38590E-01 \\ \hline $	8.07590E-01 8.07590E-01 7.12320E-01 8.52380E-01 8.52380E-01 9.23970E-01 9.22310E-01 9.22310E-01 9.22310E-01 9.22310E-01 9.79520E-01 9.76980E-01 9.86530E-01 9.86530E-01 9.86330E-01 9.80330E-01 9.80330E-01 9.02860E-01 8.97510E-01 9.60360E-01 9.60360E-01 9.63990E-01 9.626
WFG5 WFG4 W	8 10 3 5 8 10 3 5 5 8	$\begin{array}{l} 8.55450E-01 \\ \hline 8.55450E-01 \\ \hline 7.91750E-01 \\ \hline 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 9.23800E-01 \\ \hline 9.23800E-01 \\ \hline 9.22670E-01 \\ \hline 9.21520E-01 \\ \hline 9.82040E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87150E-01 \\ \hline 9.8750E-01 \\ \hline 9.8350E-01 \\ \hline 9.8350E-01 \\ \hline 9.87770E-01 \\ \hline 9.03370E-01 \\ \hline 8.99610E-01 \\ \hline 8.995120E-01 \\ \hline 9.58590E-01 \\ \hline 9.5720E-01 \\ \hline 9.5720E-01 \\ \hline 9.57700E-01 \\ \hline 9.5720E-01 \\ \hline 9.5640E-01 \\ \hline 9.60430E-01 \\ \hline 9.60440E-01 \\ \hline 9.6040E-01 \\ \hline 9.6040$	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.20690E-01} \\ \textbf{9.2020E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80220E-01} \\ \textbf{9.80240E-01} \\ \textbf{9.80240E-01} \\ \textbf{9.89240E-01} \\ \textbf{9.85780E-01} \\ \textbf{9.85780E-01} \\ \textbf{9.95840E-01} \\ \textbf{9.93070E-01} \\ \textbf{8.98130E-01} \\ \textbf{8.93180E-01} \\ \textbf{9.50670E-01} \\ \textbf{9.47760E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.51790E-01} \\ \textbf{4.501} \\ \textbf{9.51790E-01} \\ \textbf{4.501} \\ \textbf{5.5180E-01} \\ \textbf{4.501} \\ \textbf{5.5180E-01} \\ \textbf{4.501} \\ \textbf{5.5180E-01} \\ 5.5180E-01$	$\begin{array}{r} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.27910E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.16680E-01 \\ \hline 9.73930E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.69580E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88010E-01 \\ \hline 9.88130E-01 \\ \hline 9.8130E-01 \\ \hline 9.6290E-01 \\ \hline 9.56040E-01 \\ \hline 9.56040E-01 \\ \hline 9.53650E-01 \\ \hline 9.62240E-01 \\ \hline 9.60370E-01 \\ \hline 9.62340E-01 \\ \hline 9.6240E-01 \\ \hline 9.640E-01 \\ \hline 9.64$	$\begin{array}{c} 6.49880E{-}01^+\\ 6.40190E{-}01\\ 6.40190E{-}01\\ 6.70530E{-}01\\ 6.60290E{-}01^+\\ 6.37920E{-}01\\ 9.06790E{-}01\\ 8.97430E{-}01^+\\ 8.9830E{-}01\\ 6.55620E{-}01\\ 6.36480E{-}01^+\\ 6.05550E{-}01\\ 6.49310E{-}01\\ 6.49310E{-}01\\ 6.14980E{-}01^+\\ 5.85030E{-}01\\ 6.3330E{-}01\\ 8.82540E{-}01\\ 8.80560E{-}01^+\\ 8.70580E{-}01\\ 6.24710E{-}01\\ 6.09680E{-}01^+\\ 5.96880E{-}01\\ 5.67660E{-}01^+\\ 5.40930E{-}01\\ 5.40930E{-}01\\ \end{array}$	$\begin{array}{c} 8.3770 \text{E-01}^-\\ 8.27250 \text{E-01}^-\\ 8.18250 \text{E-01}^-\\ 8.18250 \text{E-01}^-\\ 8.18250 \text{E-01}^-\\ 8.22140 \text{E-01}^-\\ 8.22140 \text{E-01}^-\\ 8.22140 \text{E-01}^-\\ 8.22140 \text{E-01}^-\\ 9.2980 \text{E-01}^+\\ 8.74120 \text{E-01}^-\\ 9.34800 \text{E-01}^-\\ 9.27550 \text{E-01}^+\\ 9.18370 \text{E-01}^-\\ 9.27150 \text{E-01}^-\\ 9.27630 \text{E-01}^+\\ 8.5470 \text{E-01}^-\\ 9.27630 \text{E-01}^+\\ 8.5520 \text{E-01}^+\\ 8.5520 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.5550 \text{E-01}^+\\ 8.56950 \text{E-01}^+\\ 8.56950 \text{E-01}^+\\ 8.42830 \text{E-01}^-\\ 8.42830 \text{E-01}^-$	$\begin{array}{l} 8.62380E-01 \\ \hline 8.62380E-01 \\ \hline 8.75170E-01 \\ \hline 8.75170E-01 \\ \hline 8.63960E-01 \\ \hline 9.18590E-01 \\ \hline 9.18590E-01 \\ \hline 9.1490E-01 \\ \hline 9.1490E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.73290E-01 \\ \hline 9.87910E-01 \\ \hline 9.83050E-01 \\ \hline 9.83050E-01 \\ \hline 9.83050E-01 \\ \hline 9.7370E-01 \\ \hline 9.83050E-01 \\ \hline 9.7370E-01 \\ \hline 9.83050E-01 \\ \hline 9.7370E-01 \\ \hline 9.7370E-01 \\ \hline 9.83050E-01 \\ \hline 9.51630E-01 \\ \hline 9.40420E-01 \\ \hline 9.45370E-01 \\ \hline 9.45470E-01 \\$	8.07590E-01 7.12320E-01 8.07590E-01 7.12320E-01 8.33230E-01 9.23970E-01 9.22310E-01 9.22310E-01 9.21120E-01 9.79520E-01 9.76980E-01 9.86530E-01 9.86530E-01 9.83520E-01 9.87020E-01 9.80330E-01 9.02860E-01 8.97510E-01 8.97510E-01 9.6360E-01 9.63890E-01 9.63890E-01 9.63890E-01 9.63890E-01 9.63890E-01 9.6390
WFG5 WFG4 W	8 10 3 5 8 10 3 5 8 8	$\begin{array}{c} 8.55450E-01 \\ 8.55450E-01 \\ \hline 7.91750E-01 \\ 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 8.40580E-01 \\ \hline 9.23800E-01 \\ \hline 9.74300E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.8350E-01 \\ \hline 9.8350E-01 \\ \hline 9.83350E-01 \\ \hline 9.83350E-01 \\ \hline 9.6330E-01 \\ \hline 9.59720E-01 \\ \hline 9.59720E-01 \\ \hline 9.57780E-01 \\ \hline 9.57780E-01 \\ \hline 9.57780E-01 \\ \hline 9.6180E-01 \\ \hline 9.61040E-01 \\ \hline 9.60020E-01 \\ \hline$	$\begin{array}{c} 1.50100E-01 \\ + \\ 6.62100E-01 \\ + \\ 5.89310E-01 \\ \hline \\ 7.70670E-01 \\ + \\ 3.2980E-01 \\ + \\ 9.22330E-01 \\ - \\ 9.20690E-01 \\ + \\ 9.17950E-01 \\ - \\ 9.80220E-01 \\ - \\ 9.76700E-01 \\ \hline \\ 9.89240E-01 \\ - \\ 9.8780E-01 \\ - \\ 9.85780E-01 \\ - \\ 9.95840E-01 \\ - \\ 9.93070E-01 \\ - \\ 9.93070E-01 \\ - \\ 9.59180E-01 \\ - \\ 9.50670E-01 \\ - \\ 9.55180E-01 \\ - \\ 9.551790E-01 \\ - \\ 9.58640E-01 \\ - \\ 9.5864$	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.27910E-01 \\ \hline 9.20650E-01 \\ \hline 9.20650E-01 \\ \hline 9.18680E-01 \\ \hline 9.14610E-01 \\ \hline 9.73930E-01 \\ \hline 9.6930E-01 \\ \hline 9.6930E-01 \\ \hline 9.6930E-01 \\ \hline 9.80910E-01 \\ \hline 9.80910E-01 \\ \hline 9.88100E-01 \\ \hline 9.8140E-01 \\ \hline 9.8140E-01 \\ \hline 9.8140E-01 \\ \hline 9.81800E-01 \\ \hline 9.8100E-01 \\ \hline 9.8100E-01 \\ \hline 9.5650E-01 \\ \hline 9.56040E-01 \\ \hline 9.602240E-01 \\ \hline 9.60370E-01 \\ \hline 9.60640E-01 \\ \hline 9.58730E-01 \\ \hline 9.60640E-01 \\ \hline 9.6080E-01 \\ \hline 9.$	$\begin{array}{c} 6.49880E{-}01^+\\ 6.49880E{-}01^+\\ 6.40190E{-}01\\ 6.60290E{-}01^+\\ 6.37920E{-}01^+\\ 8.97430E{-}01^+\\ 8.9830E{-}01\\ 6.36480E{-}01^+\\ 6.35502E{-}01\\ 6.36480E{-}01^+\\ 6.35502E{-}01\\ 6.49310E{-}01\\ 6.49310E{-}01^+\\ 6.57320E{-}01\\ 6.31970E{-}01^+\\ 6.3330E{-}01\\ 8.82540E{-}01\\ 8.82540E{-}01\\ 8.80560E{-}01^+\\ 8.70580E{-}01\\ 6.24710E{-}01\\ 6.09680E{-}01^+\\ 5.96880E{-}01\\ 6.01020E{-}01\\ 5.67660E{-}01^+\\ 5.40930E{-}01\\ 6.10130E{-}01\\ 6.01020E{-}01\\ 5.40930E{-}01\\ 6.01030E{-}01\\ \end{array}$	8.32750E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.18250E-01 8.22140E-01 8.22140E-01 8.79280E-01 9.27850E-01 9.25850E-01 9.25850E-01 9.27150E-01 9.27630E-01 9.27630E-01 9.27630E-01 8.72420E-01 8.55470E-01 8.55400E-01 8.57640E-01 8.77750E-01 8.57750E-01 8.5650E-0	$\begin{array}{c} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.75170E-01\\ 9.18590E-01^{-}\\ 9.18590E-01\\ 9.18590E-01\\ 9.1490E-01\\ 9.82000E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.83050E-01\\ 9.4370E-01\\ 9.51630E-01\\ 9.46370E-01\\ 9.38590E-01\\ 9$	8.07590E-01 7.12320E-01 8.07590E-01 8.52380E-01 8.52380E-01 9.23370E-01 9.2310E-01 9.2310E-01 9.21120E-01 9.76980E-01 9.76980E-01 9.85530E-01 9.8530E-01 9.87020E-01 9.80330E-01 9.89340E-01 9.6360E-01 9.6360E-01 9.6390E-01 9.6390E-01 9.62420E-01
WFG5 WFG4 W	8 10 3 5 8 10 3 5 8 8 10	$\begin{array}{l} 8.55450E-01 \\ \hline 8.55450E-01 \\ \hline 7.91750E-01 \\ \hline 8.67930E-01 \\ \hline 8.62790E-01 \\ \hline 9.23800E-01 \\ \hline 9.74300E-01 \\ \hline 9.74300E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87140E-01 \\ \hline 9.87150E-01 \\ \hline 9.8750E-01 \\ \hline 9.8700E-01 \\ \hline 9.83550E-01 \\ \hline 9.59520E-01 \\ \hline 9.57080E-01 \\ \hline 9.57080E-01 \\ \hline 9.57080E-01 \\ \hline 9.60390E-01 \\ \hline 9.56140E-01 \\ \hline 9.60030E-01 \\ \hline 9.60030E-$	$\begin{array}{l} \textbf{1.501}, \textbf{0.501} \\ \textbf{6.62100E-01} \\ \textbf{+} \\ \textbf{5.89310E-01} \\ \textbf{7.70670E-01} \\ \textbf{7.33000E-01} \\ \textbf{+} \\ \textbf{6.32980E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.22330E-01} \\ \textbf{9.2330E-01} \\ \textbf{9.2330E-01} \\ \textbf{9.2330E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.76700E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.92110E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.9240E-01} \\ \textbf{9.94740E-01} \\ \textbf{9.94740E-01} \\ \textbf{9.94740E-01} \\ \textbf{9.94740E-01} \\ \textbf{9.93070E-01} \\ \textbf{8.99130E-01} \\ \textbf{8.99130E-01} \\ \textbf{9.5670E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.55180E-01} \\ \textbf{9.56310E-01} \\ \textbf{9.56540E-01} \\ 9.$	$\begin{array}{l} 8.48120E-01 \\ \hline 8.48120E-01 \\ \hline 8.29240E-01 \\ \hline 8.29240E-01 \\ \hline 8.38090E-01 \\ \hline 9.20650E-01 \\ \hline 9.208010E-01 \\ \hline 9.80910E-01 \\ \hline 9.80910E-01 \\ \hline 9.80910E-01 \\ \hline 9.80910E-01 \\ \hline 9.8140E-01 \\ \hline 9.8140E-01 \\ \hline 9.8140E-01 \\ \hline 9.8100E-01 \\ \hline 9.8100E-01 \\ \hline 9.89100E-01 \\ \hline 9.5670E-01 \\ \hline 9.5670E-01 \\ \hline 9.5870E-01 \\ \hline 9.58770E-01 \\ \hline 5.58770E-01 \\ \hline 5.$	$\begin{array}{l} 6.49880E{-}01^+\\ 6.49880E{-}01^+\\ 6.40190E{-}01\\ 6.60290E{-}01^+\\ 6.37920E{-}01\\ 9.06790E{-}01\\ 8.97430E{-}01^+\\ 8.89830E{-}01\\ 6.55620E{-}01\\ 6.3550E{-}01\\ 6.49310E{-}01\\ 6.49310E{-}01\\ 6.49310E{-}01\\ 6.31970E{-}01^+\\ 6.3330E{-}01\\ 8.82540E{-}01\\ 8.80560E{-}01^+\\ 8.80560E{-}01^+\\ 8.80560E{-}01^+\\ 8.70580E{-}01\\ 6.24710E{-}01\\ 6.09680E{-}01^+\\ 5.96880E{-}01\\ 6.01020E{-}01\\ 5.6760E{-}01^+\\ 5.40930E{-}01\\ 6.10130E{-}01\\ 5.86790E{-}01^+\\ 5.86790E{-}01^+\\ \end{array}$	8.32750E-01 8.27250E-01 8.18250E-01 8.18250E-01 8.42760E-01 8.22140E-01 8.22140E-01 8.79280E-01+ 8.74120E-01 9.2850E-01+ 9.27150E-01 9.27150E-01 9.27030E-01+ 9.40030E-01+ 9.27630E-01+ 8.72420E-01 8.75590E-01+ 8.75520E-01 8.77750E-01	$\begin{array}{l} 8.62380E-01^{-}\\ 8.62380E-01^{-}\\ 8.39310E-01\\ 8.75170E-01\\ 8.75170E-01\\ 8.63960E-01^{-}\\ 9.18590E-01\\ 9.18590E-01\\ 9.18590E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.73290E-01\\ 9.83900E-01\\ 9.83900E-01\\ 9.83000E-01\\ 9.83000E-01\\ 9.83000E-01\\ 9.83000E-01\\ 9.3810E-01\\ 8.92250E-01\\ 8.87070E-01\\ 9.3810E-01\\ 8.87070E-01\\ 9.3630E-01\\ 9.36370E-01\\ 9.40420E-01\\ 9.40820E-01\\ 9.$	8.07590E-01 7.12320E-01 8.07590E-01 7.12320E-01 8.52380E-01 9.2330E-01 9.2310E-01 9.2310E-01 9.21120E-01 9.774980E-01 9.76980E-01 9.85530E-01 9.85530E-01 9.87510E-01 9.80330E-01 9.6260E-01 9.61260E-01 9.63990E-01 9.62420E-01 9.62420E-01 9.61760E-01

**Table 6** Best, median and worst HV values obtained by RMaOPSO and other algorithms on WFG instances with differentnumber of objectives. Best performances are highlighted in bold face with gray background.

cial Intelligence Review 54:2567–2608, DOI https://doi.org/10.1007/s10462-020-09909-3

- Abualigah L, Diabat A, Mirjalili S, Abd Elaziz M, Gandomi AH (2021) The arithmetic optimization algorithm. Computer Methods in Applied Mechanics and Engineering 376:113609, DOI https: //doi.org/10.1016/j.cma.2020.113609
- Abualigah L, Yousri D, Abd Elaziz M, Ewees AA, Al-qaness MA, Gandomi AH (2021) Aquila

optimizer: A novel meta-heuristic optimization algorithm. Computers & Industrial Engineering 157:107250, DOI https://doi.org/10.1016/j.cie. 2021.107250

 Abualigah LMQ (2019) Feature Selection and Enhanced Krill Herd Algorithm for Text Document Clustering, vol 816, 1st edn. Springer International Publishing

Deepak Sharma et al.

<b></b>	M	NSGA-III	SPEA/B	VaEA	dMOPSO	SMPSO	MaPSO	BMaOPSO
WFG6	3	9.07810E-01	9.12380E-01	9.06840E-01	9.15370E-01	9.10770E-01	9.16270E-01	9.16150E-01
		9.04990E-01 +	9.04200E-01 +	9.01570E-01+	9.08540E-01 <sup>+</sup>	9.07230E-01 <sup>+</sup>	8 82970E-01 +	9 13290E-01
		8.99480E-01	9.00880E-01	8.97230E-01	8.81980E-01	8.97030E-01	8.82230E-01	9.09570E-01
		9.65910E-01	9.68320E-01	9.62430E-01	6.03800E-01	9.38640E-01	9.36850E-01	9.74700E-01
	5	9.61300E-01 +	9.58200E-01 <sup>+</sup>	$9.56510 \text{E-}01^+$	5.85100E-01 <sup>+</sup>	9.31730E-01 <sup>+</sup>	9.36550E-01 <sup>+</sup>	9.71390E-01
	-	9.54490E-01	9.54280E-01	9.51670E-01	5.55760E-01	9.28400E-01	9.36340E-01	9.69520E-01
	-	9.71930E-01	9.76720E-01	9.74290E-01	5.60780E-01	9.45080E-01	9.36130E-01	9.80850E-01
	8	9.65630E-01 <sup>+</sup>	9.65940E-01 <sup>+</sup>	9.65950E-01 <sup>+</sup>	$5.44850 \text{E-}01^+$	$9.41560 \text{E-}01^+$	9.36070E-01 <sup>+</sup>	9.77300E-01
		9.60550E-01	9.58560E-01	9.59030E-01	5.33000E-01	9.40570E-01	9.36000E-01	9.58550E-01
		9.76850E-01	9.80160E-01	9.73060E-01	5.79590E-01	9.49290E-01	9.32110E-01	9.83180E-01
	10	9.65770E-01 <sup>+</sup>	9.67310E-01 <sup>+</sup>	9.64340E-01 <sup>+</sup>	5.55450E-01 <sup>+</sup>	9.44460E-01 <sup>+</sup>	9.32100E-01 <sup>+</sup>	9.78080E-01
		9.55710E-01	9.56200E-01	9.50880E-01	5.40360E-01	9.42270E-01	9.32090E-01	9.71950E-01
-		9.25530E-01	9.24960E-01	9.22930E-01	8.82550E-01	8.83970E-01	9.26440E-01	9.25370E-01
	3	9.25160E-01 -	9.24160E-01 <sup>+</sup>	9.22650E-01 <sup>+</sup>	8.75930E-01 <sup>+</sup>	8.66970E-01 <sup>+</sup>	$9.26070 \mathrm{E}{-}01^{-}$	9.24830E-01
		9.24530E-01	9.23570E-01	9.21630E-01	8.67330E-01	8.53260E-01	9.25590E-01	9.24550E-01
		9.87490E-01	9.84000E-01	9.83410E-01	6.85290E-01	8.84020E-01	9.89750E-01	9.85980E-01
1	5	9.86590E-01 <sup>-</sup>	9.83520E-01 <sup>+</sup>	9.80370E-01 <sup>+</sup>	$6.47060 \text{E-}01^+$	8.75270E-01 <sup>+</sup>	$9.89640 \mathrm{E-01}^{-1}$	9.84320E-01
G		9.85090E-01	9.81920E-01	9.77780E-01	6.17670E-01	8.67030E-01	9.89450E-01	9.82400E-01
M		9.95210E-01	9.95600E-01	9.95010E-01	6.28080E-01	8.97910E-01	9.99130E-01	9.93540E-01
	8	9.93990E-01 <sup>-</sup>	9.94890E-01 <sup>-</sup>	9.94400E-01 <sup>-</sup>	6.13800E-01 <sup>+</sup>	$8.84050E-01^+$	$9.99050 \mathrm{E-01}^{-}$	9.90620E-01
		9.91930E-01	9.93800E-01	9.93570E-01	6.00910E-01	8.68130E-01	9.98940E-01	9.89140E-01
		9.96800E-01	9.97810E-01	9.96620E-01	6.51580E-01	9.17520E-01	9.99840E-01	9.95780E-01
	10	9.96000E-01 -	9.97570E-01 <sup>-</sup>	9.95440E-01 <sup>-</sup>	$6.28300 \text{E-}01^+$	8.99570E-01 <sup>+</sup>	$9.99810 \text{E-}01^-$	9.94840E-01
		9.94820E-01	9.96790E-01	9.93230E-01	6.10660E-01	8.89000E-01	9.99730E-01	9.93570E-01
	3	9.07130E-01	9.12060E-01	8.93340E-01	8.35130E-01	8.45640E-01	9.01710E-01	9.05690E-01
		9.04450E-01 <sup>-</sup>	$9.09470 \mathrm{E}{-}01^{-}$	8.90140E-01 <sup>+</sup>	$8.22450E-01^+$	8.29490E-01 <sup>+</sup>	8.99280E-01 <sup>+</sup>	9.03170E-01
		9.03040E-01	9.05760E-01	8.86740E-01	8.14720E-01	8.13670E-01	8.97750E-01	9.01150E-01
	5	9.68530E-01	9.73780E-01	9.53750E-01	6.33600E-01	8.62840E-01	9.70330E-01	9.66030E-01
20		9.65260E-01 <sup>-</sup>	$9.70780 \text{E-}01^-$	9.45730E-01 <sup>+</sup>	$6.07020 \text{E-}01^+$	8.48690E-01 <sup>+</sup>	9.69380E-01 <sup>-</sup>	9.60450E-01
F		9.60950E-01	9.66910E-01	9.35660E-01	5.94110E-01	8.34860E-01	9.64090E-01	9.52750E-01
$\geq$		9.75980E-01	9.89670E-01	9.62950E-01	6.12310E-01	8.77300E-01	9.87860E-01	9.68900E-01
	8	9.67820E-01 -	$9.88220 \pm 01^{-1}$	$9.52950 \text{E}{-}01^{-}$	$5.89980E-01^{+}$	$8.48820E-01^{+}$	9.83540E-01 -	9.46650E-01
		9.55860E-01	9.85050E-01	9.36220E-01	5.54250E-01	8.29400E-01	9.77240E-01	9.26980E-01
	10	9.78740E-01	9.94820E-01	9.67200E-01	6.27390E-01	8.97600E-01	9.92790E-01	9.78060E-01
		9.73090E-01	9.94030E-01	9.56930E-01	6.01290E-01	8.70360E-01	9.91020E-01	9.67140E-01
		9.04010E-01	9.92960E-01	9.39640E-01	5.81340E-01	8.51410E-01	9.81690E-01	9.33220E-01
	3	8.93710E-01	8.89040E-01	8.93400E-01	8.80610E-01	8.82210E-01	8.92260E-01	8.94030E-01
		8.74290E-01 -	8.62340E-01 -	8.73110E-01	8.68350E-01	8.73650E-01	8.53540E-01 '	8.82850E-01
		8.59390E-01	8.59100E-01	8.53690E-01	8.57600E-01	8.45330E-01	8.49270E-01	8.60660E-01
	F	9.45010E-01	9.21170E-01	9.55750E-01	0.01050E-01	8.90100E-01	9.39710E-01	9.14570E-01
69	э	9.07190E-01	9.01670E-01	9.01900E-01	0.23030E-01	8.72930E-01	8.98630E-01	9.09710E-01
/F		9.03020E-01 0.03250F-01	0.90010E-01	0.97920E-01	0.00940E-01 6.38670E-01	0.04/20E-01 8 78800F 01	0.93420E-01 8 08110F 01	9.07220E-01
	8	8 08530E 01 +	8 01700E 01 +	8.07570F 01=	5 85210E 01+	8.66720E 01+	8 01610E 01 +	8 00050F 01
	0	8.85810F 01	8 80880F 01	8 00300E 01	5.43030F 01	8.46450F 01	8.87440F 01	8.05370E-01
		9.43600E-01	9.22390E-01	9 44250E-01	6.38010E-01	8 94820E-01	8.96880E-01	9 14540E-01
	10	$9.01710E_{01}^{=}$	$8.94760E_{-01} =$	$8.98/90E_{-01}=$	5.97190E-01+	8 82230E-01+	8 91780E-01 +	9.00330E_01
		8.91960E-01	8.87560E-01	8.91280E-01	5.46390E-01	8.64140E-01	8.85640E-01	8.95410E-01
(+	/_/_)	9/12/15	18/5/13	18/8/10	36/0/0	31/3/2	16/3/17	0.001101-01



Fig. 6 Average performance score based on the median IGD values over all objectives for different DTLZ and WFG problem instances. The solid line represents the performance of RMaOPSO.



**Fig. 7** Average performance score based on the median IGD values over all DTLZ (Dx) and WFG (Wx) problem instances. The solid line represents the performance of RMaOPSO.



Fig. 8 Ranking of algorithms over all DTLZ and WFG test instances. The smaller rank represents better performance.

- Al Moubayed N, Petrovski A, McCall J (2012) D<sup>2</sup>mopso: Multi-objective particle swarm optimizer based on decomposition and dominance. In: Hao JK, Middendorf M (eds) Evolutionary Computation in Combinatorial Optimization, Springer Berlin Heidelberg, Berlin, Heidelberg, pp 75–86
- Barakat N, Sharma D (2019) Evolutionary multiobjective optimization for bulldozer and its blade in soil cutting. International Journal of Management Science and Engineering Management 14(2):102– 112, DOI 10.1080/17509653.2018.1500953
- Britto A, Pozo A (2012) I-mopso: A suitable pso algorithm for many-objective optimization. In: 2012 Brazilian Symposium on Neural Networks, pp 166– 171, DOI 10.1109/SBRN.2012.20
- Britto A, Pozo A (2012) Using archiving methods to control convergence and diversity for manyobjective problems in particle swarm optimization. In: 2012 IEEE Congress on Evolutionary Computation, pp 1–8, DOI 10.1109/CEC.2012.6256149
- 9. Britto A, Pozo A (2014) Using reference points to update the archive of mopso algorithms in manyobjective optimization. Neurocomputing 127:78 - 87, DOI https://doi.org/10.1016/j.neucom.2013. 05.049, advances in Intelligent Systems
- de Carvalho AB, Pozo A (2012) Measuring the convergence and diversity of cdas multiobjective particle swarm optimization algorithms: A study of many-objective problems. Neurocomputing 75(1):43 – 51, DOI https://doi.org/10. 1016/j.neucom.2011.03.053, brazilian Symposium on Neural Networks (SBRN 2010) International Conference on Hybrid Artificial Intelligence Systems (HAIS 2010)
- 11. Castro OR, Santana R, Pozo A (2016) Cmulti: A competent multi-swarm approach for

many-objective problems. Neurocomputing 180:68 - 78, DOI doi.org/10.1016/j.neucom.2015.06.097, progress in Intelligent Systems Design

- Cheng T, Chen M, Fleming PJ, Yang Z, Gan S (2017) A novel hybrid teaching learning based multi-objective particle swarm optimization. Neurocomputing 222:11 – 25, DOI https://doi.org/10. 1016/j.neucom.2016.10.001
- Coello CAC, Pulido GT, Lechuga MS (2004) Handling multiple objectives with particle swarm optimization. IEEE Transactions on Evolutionary Computation 8(3):256–279, DOI 10.1109/TEVC. 2004.826067
- Coello Coello CA, Lechuga MS (2002) MOPSO: a proposal for multiple objective particle swarm optimization. In: Proceedings of the 2002 Congress on Evolutionary Computation. CEC'02 (Cat. No.02TH8600), vol 2, pp 1051–1056 vol.2, DOI 10.1109/CEC.2002.1004388
- Dai C, Wang Y, Ye M (2015) A new multi-objective particle swarm optimization algorithm based on decomposition. Information Sciences 325:541 – 557, DOI https://doi.org/10.1016/j.ins.2015.07.018
- Das I, Dennis JE (1998) Normal-boundary intersection: A new method for generating the pareto surface in nonlinear multicriteria optimization problems. SIAM Journal on Optimization 8(3):631–657, DOI 10.1137/S1052623496307510
- Deb K, Agrawal RB (1995) Simulated binary crossover for continuous search space. Complex Systems 9(2):115–148
- Deb K, Jain H (2014) An evolutionary manyobjective optimization algorithm using referencepoint-based nondominated sorting approach, part i: Solving problems with box constraints. IEEE Transactions on Evolutionary Computation 18(4):577-601, DOI 10.1109/TEVC.2013.2281535
- Deb K, Pratap A, Agarwal S, Meyarivan T (2002) A fast and elitist multiobjective genetic algorithm: NSGA-II. Evolutionary Computation, IEEE Transactions on 6(2):182 –197
- Deb K, Thiele L, Laumanns M, Zitzler E (2005) Scalable test problems for evolutionary multiobjective optimization. In: Abraham A, Jain L, Goldberg R (eds) Evolutionary multiobjective optimization: theoritical advances and applications, Springer-Verlag, London, pp 105–145
- Deb K, Gupta S, Daum D, Branke J, Mall A, Padmanabhan D (2009) Reliability-based optimization using evolutionary algorithms. IEEE Transaction on Evolutionary Computation 13(5):1054–1074
- 22. Durillo JJ, Nebro AJ (2011) jmetal: A java framework for multi-objective optimization. Advances

in Engineering Software 42:760–771, DOI DOI:10. 1016/j.advengsoft.2011.05.014

- Figueiredo E, Ludermir T, Bastos-Filho C (2016) Many objective particle swarm optimization. Information Sciences 374:115 – 134, DOI https://doi. org/10.1016/j.ins.2016.09.026
- 24. Han H, Lu W, Zhang L, Qiao J (2018) Adaptive gradient multiobjective particle swarm optimization. IEEE Transactions on Cybernetics 48(11):3067–3079, DOI 10.1109/TCYB.2017. 2756874
- Hirano H, Yoshikawa T (2013) A study on two-step search based on pso to improve convergence and diversity for many-objective optimization problems. In: 2013 IEEE Congress on Evolutionary Computation, pp 1854–1859, DOI 10.1109/CEC.2013. 6557785
- 26. Hu W, Yen GG (2015) Adaptive multiobjective particle swarm optimization based on parallel cell coordinate system. IEEE Transactions on Evolutionary Computation 19(1):1–18, DOI 10.1109/ TEVC.2013.2296151
- 27. Hu W, Yen GG, Luo G (2017) Many-objective particle swarm optimization using two-stage strategy and parallel cell coordinate system. IEEE Transactions on Cybernetics 47(6):1446–1459, DOI 10. 1109/TCYB.2016.2548239
- 28. Huband S, Hingston P, Barone L, While L (2006) A review of multiobjective test problems and a scalable test problem toolkit. IEEE Transactions on Evolutionary Computation 10(5):477–506, DOI 10.1109/TEVC.2005.861417
- 29. Jiang S, Yang S (2017) A strength pareto evolutionary algorithm based on reference direction for multiobjective and many-objective optimization. IEEE Transactions on Evolutionary Computation 21(3):329–346, DOI 10.1109/TEVC.2016.2592479
- 30. Junior O, Britto A, Pozo A (2012) A comparison of methods for leader selection in many-objective problems. In: 2012 IEEE Congress on Evolutionary Computation, pp 1–8, DOI 10.1109/CEC.2012. 6256415
- 31. Köppen M, Yoshida K (2007) Many-objective particle swarm optimization by gradual leader selection. In: Beliczynski B, Dzielinski A, Iwanowski M, Ribeiro B (eds) Adaptive and Natural Computing Algorithms, Springer Berlin Heidelberg, Berlin, Heidelberg, pp 323–331
- 32. Li L, Wang W, Xu X (2017) Multi-objective particle swarm optimization based on global margin ranking. Information Sciences 375:30 – 47, DOI https://doi.org/10.1016/j.ins.2016.08.043

- 33. Li L, Chang L, Gu T, Sheng W, Wang W (2020) On the norm of dominant difference for many-objective particle swarm optimization. IEEE Transactions on Cybernetics (in press) pp 1–13
- 34. Lin Q, Li J, Du Z, Chen J, Ming Z (2015) A novel multi-objective particle swarm optimization with multiple search strategies. European Journal of Operational Research 247(3):732 – 744, DOI https://doi.org/10.1016/j.ejor.2015.06.071
- 35. Lin Q, Liu S, Zhu Q, Tang C, Song R, Chen J, Coello CAC, Wong K, Zhang J (2018) Particle swarm optimization with a balanceable fitness estimation for many-objective optimization problems. IEEE Transactions on Evolutionary Computation 22(1):32–46, DOI 10.1109/TEVC.2016.2631279
- 36. Liu X, Zhan Z, Gao Y, Zhang J, Kwong S, Zhang J (2019) Coevolutionary particle swarm optimization with bottleneck objective learning strategy for many-objective optimization. IEEE Transactions on Evolutionary Computation 23(4):587–602
- 37. Luo J, Huang X, Yang Y, Li X, Wang Z, Feng J (2020) A many-objective particle swarm optimizer based on indicator and direction vectors for many-objective optimization. Information Sciences 514:166 - 202, DOI https://doi.org/10.1016/j.ins. 2019.11.047
- 38. Mostaghim S, Schmeck H (2008) Distance based ranking in many-objective particle swarm optimization. In: Rudolph G, Jansen T, Beume N, Lucas S, Poloni C (eds) Parallel Problem Solving from Nature – PPSN X, Springer Berlin Heidelberg, Berlin, Heidelberg, pp 753–762
- 39. Mostaghim S, Schmeck H (2008) Distance based ranking in many-objective particle swarm optimization. In: Rudolph G, Jansen T, Beume N, Lucas S, Poloni C (eds) Parallel Problem Solving from Nature – PPSN X, Springer Berlin Heidelberg, Berlin, Heidelberg, pp 753–762
- 40. Nebro AJ, Durillo JJ, Garcia-Nieto J, Coello Coello CA, Luna F, Alba E (2009) Smpso: A new pso-based metaheuristic for multi-objective optimization. In: 2009 IEEE Symposium on Computational Intelligence in Multi-Criteria Decision-Making(MCDM), pp 66–73, DOI 10.1109/MCDM. 2009.4938830
- Padhye N, Branke J, Mostaghim S (2009) Empirical comparison of mopso methods - guide selection and diversity preservation -. In: 2009 IEEE Congress on Evolutionary Computation, pp 2516–2523, DOI 10.1109/CEC.2009.4983257
- Pan A, Wang L, Guo W, Wu Q (2018) A diversity enhanced multiobjective particle swarm optimization. Information Sciences 436-437:441 465,

DOI https://doi.org/10.1016/j.ins.2018.01.038

- Peng W, Zhang Q (2008) A decomposition-based multi-objective particle swarm optimization algorithm for continuous optimization problems. In: 2008 IEEE International Conference on Granular Computing, pp 534–537, DOI 10.1109/GRC.2008. 4664724
- 44. Purshouse RC, Fleming PJ (2007) On the evolutionary optimization of many conflicting objectives. IEEE Transactions on Evolutionary Computation 11(6):770–784, DOI 10.1109/TEVC.2007.910138
- 45. Qin S, Sun C, Zhang G, He X, Tan Y (2020) A modified particle swarm optimization based on decomposition with different ideal points for manyobjective optimization problems. Complex & Intelligent Systems (in press) pp 1 – 12, DOI https: //doi.org/10.1007/s40747-020-00134-7
- 46. Ram L, Sharma D (2017) Evolutionary and gpu computing for topology optimization of structures. Swarm and Evolutionary Computation 35:1 – 13, DOI https://doi.org/10.1016/j.swevo.2016.08.004
- 47. Ray T, Tai K, Seow KC (2001) Multiobejctive design optimization by an evolutionary algorithm. Engineering Optimization 33(4):399–424
- 48. Ser JD, Osaba E, Molina D, Yang XS, Salcedo-Sanz S, Camacho D, Das S, Suganthan PN, Coello CAC, Herrera F (2019) Bio-inspired computation: Where we stand and what's next. Swarm and Evolutionary Computation 48:220 – 250, DOI doi.org/10.1016/j. swevo.2019.04.008
- 49. Sharma D, Shukla PK (2019) Line-prioritized environmental selection and normalization scheme for many-objective optimization using reference-linesbased framework. Swarm and Evolutionary Computation 51:100592, DOI https://doi.org/10.1016/ j.swevo.2019.100592
- 50. Sharma D, Deb K, Kishore NN (2011) Domainspecific initial population strategy for compliant mechanisms using customized genetic algorithm. Structural and Multidisciplinary Optimization 43(4):541–554
- 51. Sharma D, Deb K, Kishore NN (2014) Customized evolutionary optimization procedure for generating minimum weight compliant mechanisms. Engineering Optimization 46(1):39–60
- 52. Sharma D, Basha SZ, Kumar SA (2019) Diversity over dominance approach for many-objective optimization on reference-points-based framework. In: Deb K, Goodman E, Coello Coello CA, Klamroth K, Miettinen K, Mostaghim S, Reed P (eds) Evolutionary Multi-Criterion Optimization, Springer International Publishing, Cham, pp 278–290

- 53. Sharma D, Vats S, Saurabh S (2021) Diversity preference-based many-objective particle swarm optimization using reference-lines-based framework. Swarm and Evolutionary Computation 65:100910, DOI https://doi.org/10.1016/j.swevo. 2021.100910
- 54. Sierra MR, Coello Coello CA (2005) Improving psobased multi-objective optimization using crowding, mutation and epsilon-dominance. In: Coello Coello CA, Hernández Aguirre A, Zitzler E (eds) Evolutionary Multi-Criterion Optimization, Springer Berlin Heidelberg, Berlin, Heidelberg, pp 505–519
- 55. Wickramasinghe UK, Li X (2009) Using a distance metric to guide pso algorithms for many-objective optimization. In: Proceedings of the 11th Annual Conference on Genetic and Evolutionary Computation, ACM, New York, NY, USA, GECCO '09, pp 667–674, DOI 10.1145/1569901.1569993
- 56. Woolard MM, Fieldsend JE (2013) On the effect of selection and archiving operators in manyobjective particle swarm optimisation. In: Proceedings of the 15th Annual Conference on Genetic and Evolutionary Computation, ACM, New York, NY, USA, GECCO '13, pp 129–136, URL http://doi.acm.org/10.1145/2463372.2463380
- 57. Wu B, Hu W, Hu J, Yen GG (2020) Adaptive multiobjective particle swarm optimization based on evolutionary state estimation. IEEE Transactions on Cybernetics (in press) pp 1–14
- Xiang Y, Zhou Y, Li M, Chen Z (2017) A vector angle-based evolutionary algorithm for unconstrained many-objective optimization. IEEE Transactions on Evolutionary Computation 21(1):131– 152, DOI 10.1109/TEVC.2016.2587808
- 59. Xiang Y, Zhou Y, Chen Z, Zhang J (2020) A many-objective particle swarm optimizer with leaders selected from historical solutions by using scalar projections. IEEE Transactions on Cybernetics 50(5):2209–2222
- 60. Yang W, Chen L, Wang Y, Zhang M (2020) reference points and intuitionistic fuzzy Α dominance based particle swarm algorithm multi/many-objective for optimization. Applied Intelligence 50:11331154.DOI \_ https://doi.org/10.1007/s10489-019-01569-3
- Yu H, Wang Y, Xiao S (2020) Multi-objective particle swarm optimization based on cooperative hybrid strategy. Applied Intelligence 50:256 – 269, DOI https://doi.org/10.1007/s10489-019-01496-3
- 62. Zapotecas Martínez S, Coello Coello CA (2011) A multi-objective particle swarm optimizer based on decomposition. In: Proceedings of the 13th Annual Conference on Genetic and Evolutionary Compu-

tation, ACM, New York, NY, USA, GECCO '11, pp 69–76, DOI 10.1145/2001576.2001587

- 63. Zhang X, Zheng X, Cheng R, Qiu J, Jin Y (2018) A competitive mechanism based multi-objective particle swarm optimizer with fast convergence. Information Sciences 427:63 – 76, DOI https://doi.org/ 10.1016/j.ins.2017.10.037
- 64. Zhu Q, Lin Q, Chen W, Wong K, Coello Coello CA, Li J, Chen J, Zhang J (2017) An external archive-guided multiobjective particle swarm optimization algorithm. IEEE Transactions on Cybernetics 47(9):2794–2808, DOI 10.1109/TCYB.2017. 2710133